VISCOSITY AND ELECTRIC CONDUCTIVITY OF MELT SYSTEM OF CaO - Al₂O₃ - B₂O₃

Received – Primljeno: 2015-06-12 Accepted – Prihvaćeno: 2015-12-12 Original Scientific Paper – Izvorni znanstveni rad

It was studied the viscosity and electric conductivity of the melt system CaO - Al_2O_3 - B_2O_3 . On the base of experimental data it was created the mathematical model of studied features dependence on chemical structure of melt and temperature. There were created the computer programs which allow to calculate the temperature range at 1 823 – 1 973 K. There were constructed the triaxial diagrams based on models. It was found the reduction of viscosity and extension of electric conductivity of melt CaO - Al_2O_3 by adding B_2O_3 .

Key words: metallurgy, CaO - Al₂O₃ - B₂O₃ system, viscosity, electric conductivity, axial diagram

INTRODUCTION

Melts of binary group CaO - Al₂O₃ have got wide circulation in the metallurgy by high purifying qualities. They are mostly used for deletion of sulfur from cast iron and different types of steel [1]. By adding oxidizers they successfully purify metal from phosphorous. Research of its physical characteristics have shown that the most optimum melts are which crystallized in a binary system CaO - Al₂O₃ at twelve-calcium seven aluminate (12 CaO·7 Al₂O₃) where it is easy to get fusible slags. However it should be noticed that they still have high temperature of crystallization and for better use of them it is required its overheating related to some expenses. That is why such fluxes as CaF2, CaCl2 and others are added [2]. It was noticed the expressed pass of fluorine and chlorine toxic compounds at the temperature of metallurgic redistribution [3].

They have decided to try boric anhydrite (B_2O_3) which has low temperature of melt (723 K) and which forms low temperature compounds with many oxides as an add to the melt CaO - Al_2O_3 [4]. It was planned to research viscosity and electric conductivity of triple system CaO - Al_2O_3 - B_2O_3

WAYS OF RESEARCH

For measuring the viscosity it was used electrovibrator viscosimeter [5, 6]. It was graduated by heavy liquid ("Clerichy") which has density close to the density of oxide melts. Reactionary crucible and viscosimeter probe were made of molybdenum. The temperature in working area of furnace fixed tungsten rhenium ther-

mocouple BP-5/20 the end of which reinforced by alunite cover got to the bottom of crucible in a special dimple. Thermocouple was checked periodically by the temperature of pure metals melt.

Samples of slag were prepared from chemically pure reagents. At first they were fired then remelt and saved in the hermetic dish. The experiments were controlled at every point on the data of not less than three experiments by calculation of dispersion and root-mean-square error.

The experiments were held by mathematic planning at simplex [7 - 9] Figure 1. For the research it was chosen the local part of triple diagram CaO - Al $_2$ O $_3$ - B $_2$ O $_3$ with coordinate peaks, mass %: y_1 = 62,20 CaO и 37,80 Al $_2$ O $_3$; y_2 = 35,40 CaO и 64,60 Al $_2$ O $_3$; y_3 = 42,00 CaO, 42,00 Al $_2$ O $_3$ и 16,00 B $_2$ O $_3$. (Table 1) According to recommendation [7-9] for description of triple system melt characteristics was chosen polynomial of fourth degree:

$$\begin{split} \lg \eta &= \beta_1 \, x_1 + \beta_2 \, x_2 + \beta_3 \, x_3 + \beta_{12} \, x_1 x_2 + \\ &+ \beta_{13} \, x_1 x_3 + \beta_{23} \, x_2 x_3 + \gamma_{12} \, x_1 x_2 (x_1 - x_2) + \\ &+ \gamma_{13} \, x_1 x_3 (x_1 - x_3) + \gamma_{23} \, x_2 x_3 (x_2 - x_3) + \\ &+ \sigma_{12} \, x_1 x_2 (x_1 - x_2)^2 + \sigma_{13} \, x_1 x_3 (x_1 - x_3)^2 + \\ &+ \sigma_{23} \, x_2 x_3 (x_2 - x_3)^2 + \beta_{1123} \, x_1^2 x_2 x_3 + \\ &+ \beta_{1223} \, x_1 x_2^2 x_3 + \beta_{1233} \, x_1 x_2 x_3^2, \end{split}$$

where

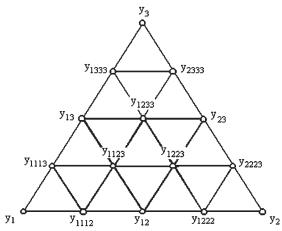
 η – viscosity / Pa·sec,

 β_1 , β_2 , β_3 , γ_{12} , σ_{12} , and others – polynomial coefficients, x_1 , x_2 , x_3 – fractions of unit according to the content of pseudocomponents CaO, Al₂O₃ and B₂O₃ at the peaks of simplex (Table 1).

Analogous equations were chosen for description pf electric conductivity of melts. In the matrix of plans recalculation of slag content from the coordinates of pseudocomponents into massive percentage were made by formulas:

A. Akberdin, U. Konurov, A. Kim, R. Saitov Chemical-Metallurgical Institute, Karaganda, Kazakhstan

R. Sultangaziyev, A. Issagulov, Karaganda State Technical University, Karaganda, Kazakhstan



y1, y2, y3, - the vertices of the triangle yi - designation of points plan

Figure 1 Disposition of experimental points at simplex

$$CaO = 62.2 x_1 + 35.4 x_2 + 42 x_3, (2)$$

$$Al_2O_3 = 37.8 x_1 + 64.6 x_2 + 42x_3,$$
 (3)

$$B_2O_3 = 16 x_3$$
 (4)

At the machine method of getting viscosity by the Formula (1) the system of equation (2-4) are solved according to x_1 , x_2 , and x_3 :

$$x_1 = 0.0239 \cdot CaO - 0.0131 \cdot Al_2O_3 - 0.0283 \cdot B_2O_3$$
, (5)

$$x_2 = -0.014 \cdot CaO + 0.0231 \cdot Al_2O_3 - 0.0241 \cdot B_2O_3$$
, (6)

$$x_3 = 0.0625 \cdot B_2 O_3 \tag{7}$$

Further, knowing the content of slag by CaO, Al_2O_3 and B_2O_3 using the formula (5-7) at first we get the value of x_1 , x_2 and x_3 which we put to equation (1) it is get the value of viscosity.

According to chosen polynomial (equation 1) we have to get 15 experiments. Disposition of all the points at the triangle CaO - Al_2O_3 - B_2O_3 is shown in the picture 1 and its content at the weight % and coordinates of pseudocomponents (x_i) – at the matrix of plans (Table 1).

Table 1 Matrix of experiment planning

	Melt content						
Nº	Code scale, fraction of units		weight / %			Index of melt	
	X,	X ₂	X ₃	CaO	Al ₂ O ₃	B_2O_3	
1	1	0	0	62,20	37,80	0	y ₁
2	0	1	0	35,40	64,60	0	y ₂
3	0	0	1	42,00	42,00	16	y ₃
4	1/2	1/2	0	48,80	51,20	0	y ₁₂
5	1/2	0	1/2	52,10	39,90	8	y ₁₃
6	0	1/2	1/2	38,70	53,30	8	y ₂₃
7	3/4	1/4	0	55,50	44,50	0	y ₁₁₁₂
8	3/4	0	1/4	57,15	38,85	4	y ₁₁₁₃
9	0	3/4	1/4	37,05	58,95	4	y ₂₂₂₃
10	1/4	3/4	0	42,10	57,90	0	y ₁₂₂₂
11	1/4	0	3/4	47,05	40,95	12	y ₁₃₃₃
12	0	1/4	3/4	40,35	47,65	12	y ₂₃₃₃
13	1/2	1/4	1/4	50,45	45,55	4	y ₁₁₂₃
14	1/4	1/2	1/4	43,75	52,25	4	y ₁₂₂₃
15	1/4	1/4	1/2	45,40	46,60	8	y ₁₂₃₃

RESULTS OF RESEARCH

Experimental values of viscosity at all 15 points of plan are in the Table 2. They are base for calculation of coefficients in the equation of polynomial (1). For example, $\beta_1 = Ig\eta_1$; $\beta_2 = lg\eta_2$; $\beta_{12} = 9/4(lg\eta_{112} + lg\eta_{122} - lg\eta_1 \cdot Ig\eta_2)$ [9]. Thus all 15 coefficients of polynomial got by this way are given in the Table 3. Availability of coefficients let us define concretely the equation (1) for getting the value of viscosity at the temperature 1 823, 1 873, 1 923 and 1 973 K.

For example, at the temperature 1 873 K it looks as:

$$\begin{split} &\lg\eta = -0.1871 \ x_1 - 0.167 \ 5x_2 - 1 \ x_3 - 1.2168 \ x_1x_2 - \\ &0.9214 \ x_1x_3 - 0.2182 \ x_2x_3 - 1.1712 \ x_1x_2(x_1 - x_2) + 0.3768 \\ &x_1x_3(x_1 - x_3) - -0.1496 \ x_2x_3(x_2 - x_3) - 2.3232 \ x_1x_2(x_1 - x_2)^2 \\ &- -0.1037 \ x_1x_3(x_1 - x_3)^2 + 1.5800 \ x_2x_3(x_2 - x_3)^2 - -4.9245 \\ &x_1^2 x_2x_3 - 5.5091 \ x_1 x_2^2 x_3 + 10.330 \ x_1 x_2 x_3^2 \end{split}$$

Table 2 Experimental value of viscosity

Nº	Viscosity / Pa-sec				
IN-	1 82 3K	1 873 K	1 923 K	1 973 K	
y ₁	1,60	0,65	0,30	0,17	
y ₂	9,95	0,68	0,39	0,28	
y ₃	0,13	0,10	0,08	0,07	
y ₁₂	0,47	0,33	0,23	0,17	
y ₁₃	0,19	0,15	0,13	0,10	
y ₂₃	0,28	0,23	0,20	0,17	
y ₁₁₁₂	0,30	0,24	0,19	0,16	
y ₁₁₁₃	0,36	0,30	0,25	0,22	
y ₂₂₂₃	2,01	0,44	0,35	0,28	
y ₁₂₂₂	0,59	0,39	0,26	0,18	
y ₁₃₃₃	0,12	0,10	0,07	0,06	
y ₂₃₃₃	0,23	0,18	0,15	0,13	
y ₁₁₂₃	0,24	0,18	0,14	0,10	
y ₁₂₂₃	0,29	0,23	0,18	0,14	
y ₁₂₃₃	0,26	0,19	0,15	0,12	

Table 3 Coefficient of viscosity model

Nō	Coefficient of polynomials	Coefficients of viscosity models at temperatures / K				
		1 823 K	1 873 K	1 923 K	1 973 K	
1	β1	0,2041	- 0,1871	- 0,5229	- 0,7696	
2	β2	0,9978	- 0,1675	- 0,4089	- 0,5528	
3	β3	- 0,8861	- 1	- 1,0969	- 1,1549	
4	β12	- 3,7154	- 1,2168	- 0,6896	- 0,4336	
5	β13	- 1,5208	- 0,9214	- 0,3048	- 0,151	
6	β23	- 2,4346	- 0,2182	0,2156	0,337	
7	γ12	0,5496	- 1,1712	- 0,4224	0,3051	
8	γ13	- 0,3627	0,3768	1,4176	1,9816	
9	γ23	- 0,0024	- 0,1496	0,128	0,172	
10	σ12	- 5,98	- 2,3232	- 1,2352	- 0,5931	
11	σ13	- 1,1968	0,1037	- 0,2443	1,0851	
12	σ23	4,9725	1,5800	1,5483	1,5192	
13	β1123	1,7661	- 4,9245	- 11,115	- 19,034	
14	β1223	- 9,0139	- 5,5091	- 4,9627	- 1,9299	
15	β1233	19,195	10,3301	11,2304	12,9173	

The equations are analogous at other temperatures. Thus the problem of creation the mathematical model can be considered solved. On the base of these models the computer program was created which shows at the screen and prints the value of viscosity at the values of melt and temperature given by desk. The program can

be used at the range of melts and temperatures shown in the Table 1.

The electric conductivity of melt CaO - Al₂O₂ - B₂O₃ was studied. The current-voltage scheme realized on the combined set on viscosity measure by vibration was used for that . It let us measure viscosity on two main parameters during the same experiment. One of the electrode was viscosimeter probe whereas the second was molybdenic glass where the probe of slag was set to. For reduction of polarization at the slag – electrode board the current of high frequency was used [10]. The vacuum tube generator was used as a source of it. The cell was graduated by electrolyte which has electric conductivity close to studied melts: by melt CaCl, at 1 273 K, by melt KCl at 1 123 K and by one normal melt KCl at 293 K [11]. The experiments were planned mathematically and held at the 15 points where viscosity was studied (Table 4).

Table 4 Experimental value of electric conductivity

				,	
Melt	Electric conductivity / χ Om⁻¹ · cm⁻¹				
index	1 723 K	1 773 K	1 823 K	1 873 K	
y ₁	0,28	0,42	0,59	0,83	
y ₂	0,11	0,19	0,30	0,47	
y ₃	0,65	0,91	1,23	1,74	
y ₁₂	0,22	0,32	0,46	0,65	
y ₁₃	0,47	0,68	0,93	1,32	
y ₂₃	0,22	0,33	0,47	0,68	
y ₁₁₁₂	0,21	0,35	0,51	0,76	
y ₁₁₁₃	0,62	0,87	1,17	1,58	
y ₂₂₂₃	0,11	0,19	0,31	0,50	
y ₁₂₂₂	0,13	0,23	0,36	0,59	
y ₁₃₃₃	0,54	0,76	1,05	1,41	
y ₂₃₃₃	0,40	0,58	0,81	1,15	
y ₁₁₂₃	0,43	0,62	0,85	1,20	
y ₁₂₂₃	0,29	0,42	0,58	0,81	
y ₁₂₃₃	0,36	0,51	0,71	0,98	

The coefficients of polynomials were found experimentally by the values of electric conductivity in the above scheme (1). Its values are in the Table 5. They allow to derive mathematical equation for values of electric conductivity (χ) depending on the content at four temperatures : 1 723, 1 773, 1 823 and 1 873 K. For example there is a mathematical model of value $\lg\chi$ at the temperature 1 873 K:

$$\begin{split} & \lg\chi = -\ 0.082\ x_{_1} - 0.3279\ x_{_2} + 0.2405\ x_{_3} + 0.0735\ x_{_1}x_{_2} + \\ & 0.1719\ x_{_1}x_{_3} - 0.4953\ x_{_2}x_{_3} - 0.0634\ x_{_1}x_{_2}(x_{_1} - x_{_2}) + 1.1378 \\ & x_{_1}x_{_3}(x_{_1} - x_{_3}) - 0.4133\ x_{_2}x_{_3}(x_{_2} - x_{_3}) + 0.3799\ x_{_1}x_{_2}(x_{_1} - x_{_2})^2 \\ & + 1.3685\ x_{_1}x_{_3}(x_{_1} - x_{_3})^2 + 0.3493\ x_{_2}x_{_3}(x_{_2} - x_{_3})^2 + 6.2068 \\ & x_{_1}^2x_{_2}x_{_3} + 4.0646x_{_1}x_{_2}^2x_{_3} - 3.8796x_{_1}x_{_2}x_{_3}^2. \end{split} \tag{9}$$

The check of conformity of got dependence was held on the criteria of Student at three extra control points (two experiments for every mix) at the level a=0.05. Calculation has shown that in all cases $t_{\rm exp.}=3.267 < t_{\rm tabl.}=5.841$ that means the hypothesis of conformity is not rejected.

Table 5 Coefficients of electric conductivity models

Nº	Coefficients index	Coefficients of electric conductivity models at temperatures / K				
		1 723	1 773	1 823	1 873	
1	$\beta_{_1}$	- 0,5423	- 0,3729	- 0,2267	- 0,0820	
2	β_2	- 0,9586	- 0,7212	- 0,5229	- 0,3279	
3	$\beta_{_3}$	- 0,1871	- 0,0410	- 0,0899	0,2405	
4	β ₁₂	0,3733	0,2110	0,1525	0,0735	
5	β ₁₃	0,1600	0,1685	0,1559	0,1719	
6	β_{23}	- 0,3389	- 0,4015	- 0,4457	- 0,4953	
7	Υ ₁₂	- 0,0312	0,0316	0,0112	- 0,0634	
8	γ ₁₃	1,3121	1,2284	1,1212	1,1378	
9	γ ₂₃	- 0,9328	- 0,7708	- 0,5906	- 0,4133	
10	$\sigma_{_{12}}$	- 2,1982	- 0,8527	- 0,4654	0,3799	
11	$\sigma_{_{13}}$	2,1772	1,8997	1,8515	1,3685	
12	$\sigma_{_{23}}$	- 0,8934	- 0,4804	- 0,0006	0,3493	
13	β ₁₁₂₃	4,1398	4,6445	5,0029	6,2068	
14	β ₁₂₂₃	11,5500	9,3388	6,7502	4,0646	
15	β ₁₂₃₃	- 6,1681	- 5,6302	- 4,3851	- 3,8796	

RESULTS DISCUSSION

Mathematical models of viscosity (8) and electric conductivity (9) can be used for values of melts features of current and planned industry as well as construction of graphical diagrams. In the Figures 2 and 3 you can see the example of these models use for such purposes.

Its analysis shows that at all the range of temperatures B_2O_3 has considerable positive influence on viscosity. There are wide areas of mobile melts (0,15 - 0,20 Pa·sec) which is important for stable work of industrial sets where there are variations of in-process materials. Reduction of viscosity level by adding boron oxide let us make processes at the low thermal level which saves the heat.

Boron anhydrite (B_2O_3) has influence on electric conductivity of melts CaO - Al_2O_3 . It is necessary to know it while choosing transformer of electric furnaces working on the principle of electric resistance of slag melts.

B₂O₃ does not have such additional charge carriers as Mg²⁺, Ca²⁺, F⁻, O²⁻, for example as manganese oxide and calcium fluoride because it is located as anions of different degree in the melt.

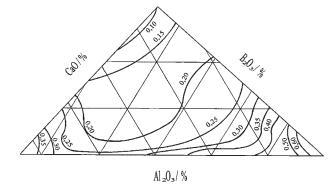
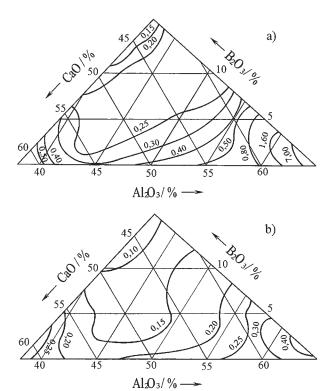


Figure 2 Diagram of melts viscosity of CaO - Al_2O_3 - B_2O_3 at 1 873 K



Figture 3 Diagrams of electric conductivity (values are increased 100 times) of melts CaO - Al₂O₃ - B₂O₃ for: a) 1 723; b) 1 823/K

Its influence is indicated by changing of melt viscosity. Transfer of the boron most part at high temperatures from four to three-coordinated state [12, 13] and occurrence of fusible borates [4] leads to reduction of melt viscosity that contributes to rise of charge carrier mobility.

The effect of its influence reduces in main liquid slags where there are many charge carriers (Ca²+) and there are not any barriers (as in thick slags) for its drift. While reaching minimal values of viscosity the further admix B_2O_3 causes reduction of χ because of progressive reduction of charge carriers.

In metallurgy slags based on calcium aluminate are frequently used in such sets as "furnace-bucket" for deletion of sulfur and other contaminations whereas oxygen is deleted from the steel by admix for example Al and FeSi. We can get metal alloyage with boron by mix of deoxidizers and B_2O_3 while the concentration of boron is minimal (0,002 - 0,.003 %) and exceeds traditional ferroalloys ten times according to its positive influen. Thus we can see one more advantage of flux CaO - Al_2O_3 - B_2O_3 at fluorine and chlorine.

CONCLUSION

It was experimentally researched viscosity and electric conductivity of melts CaO - Al_2O_3 - B_2O_3 . On the base of experimental data it was created the mathematical model of studied features dependence on chemical structure of melt and temperature. These models can be used for estimation of current melts features and planned for industries as well as for making graphical diagrams. It is shown that admix of boron anhydrite (B_2O_3) in the melt CaO - Al_2O_3 leads to reduction of viscosity and extension of electric conductivity. In the metallurgy melts CaO - Al_2O_3 - B_2O_3 can be used for deletion of sulfur from steel and its alloyage with boron.

LITERATURE

- [1] Voinov S., Shalimov A. Steel purifying with synthetic slags. M.: Metallurgija, Russia 1970. 464 p.
- [2] Momokava H., Sano N. Thermodynamics of Phosphideand Phosphatein CaO -Al₂O₃ meltsunder Strongly Reducing Conditions //Trans. Ironand 22(1982)4, 87
- [3] Filova V. Harmful chemical substances. Inorganic elements combinations of I-IV groups. Directory. Leningrad.: Chemistry, 1989. 165 p.
- [4] Slag atlas. Translation from German. Redaction of Kulikov I. M.: Metallurgija, Russia 1985. 308 p.
- [5] Solovyev A., Caplun A. Vibration method of liquid viscosity value. Novosibirsk: Science, 1970. 140 p.
- [6] Voskoboynikov V., Dunayev N., Mikhalevich A. and others. Liquid slags features. M.: Metallurgija, Russia 1975–182 p.
- [7] Scheffe H. Experiments with mixtures //J. Roy. Stat. Soc. 22(1958)B, 344-360
- [8] Gorman J.W., Hinman J.E. Simplex lattice designs for multi-component Systems //Technometrics 4(1962)4, 463-487
- [9] Chemleva T., Adler Y. Experiment planning at diagram "content-characteristics" creation. //Saint Petersburg: «Use of mathematical methods for research of multicomponent systems». – M: Metallurgija, Russia -1974.-p.11-42.
- [10] Linchevskiy B. Technique of metallurgic experiment. M: Metallurgija, Russia 1967. - 344 p.
- [11] Zhmoydin G. Electric conductivity of fluorine melts//Iz-vestiya AS of USSR, Metals . (1970)3, 69-74.
- [12] Belov N. About the atomic structure if glass // Glass structure. Leningrad: Edition of AS USSR, 1955. p. 344.
- [13] Tarasov V. New problems of glass physics. M.: Gosstroyizdat, Russia 1959. 270 p.

Note: he responsible translator for English language is Nataliya. Drag, Karaganda, Kazakhstan