

# BIODEGRADATION AND MECHANICAL BEHAVIOUR OF SINTERED COMPAKTS OF Co-Cr ALLOY POWDER DOPED WITH ZrO<sub>2</sub> USED IN DENTISTRY

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Original scientific paper

Direct Metal Laser Sintering process is modern technology and is used in different industries, inclusive in medicine industry. The purpose of this study was to obtain sintered compacts of Co-Cr powder doped with ZrO<sub>2</sub> in order to improve the bioactivity of the implants and the behavior in vitro after immersion in simulated biological fluid (SBF) for 21 days. Co-Cr powders (ST2724G) were used to realize one reference sample of Co-Cr and 4 compacts of Co-Cr doped with ZrO<sub>2</sub> in the following percents: a) 5 % ZrO<sub>2</sub>, b) 10 % ZrO<sub>2</sub>, c) 15 % ZrO<sub>2</sub>, d) 20 % ZrO<sub>2</sub>. The morphology and structure of all compacts were determined using scanning electron microscope (SEM), EDS (quantitative and qualitative) and X-ray diffraction analysis (XRD). The microstructures differ in function of concentrations. XRD presents qualitative analysis of Co-Cr probes doped with zirconia and EDS analysis presents qualitative and quantitative analysis of composites compacts, before and after immersion in SBF for 21 days. After immersion in SBF, it can be noticed that the probes of Co-Cr doped with zirconia demonstrate good corrosion resistance and that for the probe Co-Cr doped with 20 % zirconia mechanical resistance is low. In this study the mechanical behavior of Co-Cr powder manufacturing by Direct Metal Laser Sintering (DMLS) process was determined. The sintering machine Phenix Systems type PXS & PXM Dental uses the Co-Cr powder (ST2724G) and for 3D printing use "stl" file. The mechanical tests (traction and compression) was realized with an INSTRON 8810 machine.

**Keywords:** biodegradation; Co-Cr sintered compact; dental implant; in vitro test; mechanical behaviour; SEM analysis; ZrO<sub>2</sub>; XRD analysis

## Biološka razgradnja i mehaničko ponašanje sinteriranih kompakata od Co-Cr legure u prahu dopiranih sa ZrO<sub>2</sub> rabljenih u stomatologiji

Izvorni znanstveni članak

Direct Metal Laser Sintering je postupak moderne tehnologije s primjenom u različitim industrijama, uključujući medicinsku industriju. Namjena ovog istraživanja bila je dobiti sinterirane kompakte Co-Cr praha dopiranog sa ZrO<sub>2</sub> u cilju poboljšanja biološke aktivnosti implantata te ponašanja in vitro nakon uranjanja u simuliranu biološku tekućinu (SBF) tijekom 21 dana. Co-Cr prašak (ST2724G) rabljen je za izradu jednog referentnog uzorka Co-Cr i 4 kompakta Co-Cr dopirana sa ZrO<sub>2</sub> u sljedećim postocima: a) 5 % ZrO<sub>2</sub>, b) 10 % ZrO<sub>2</sub>, c) 15 % ZrO<sub>2</sub>, d) 20 % ZrO<sub>2</sub>. Morfološija i struktura svih kompaktova određena je skeniranjem elektronskim mikroskopom (SEM), EDS (kvantitativno i kvalitativno) i rendgenskom analizom difracije (XRD). Mikrostrukture se razlikuju u ovisnosti o koncentraciji. XRD predstavlja kvalitativnu analizu sondi Co-Cr dopiranih cirkonij-dioksidom i EDS analiza predstavlja kvalitativnu i kvantitativnu analizu kompozita kompakta, prije i nakon uranjanja u SBF tijekom 21 dana. Nakon uranjanja u SBF, može se primjetiti da su sonde Co-Cr dopirane s cirkonijem imale dobru otpornost na koroziju, a sonde Co-Cr dopirane s 20 % cirkonija nizak mehanički otpor. U ovoj analizi je utvrđeno mehaničko ponašanje Co-Cr praha proizvedenog procesom izravnog laserskog sinteriranja metala (DMLS). Stroj za sinteriranje Phenix System tipa PXS & PXM Dental koristio je Co-Cr prah (ST2724G) a za 3D ispis datoteku "stl". Ispitivanje mehaničkih svojstava (vlaka i kompresije) ostvareno je na INSTRON 8810 stroju.

**Ključne riječi:** biološka razgradnja; Co-Cr sinterirani kompakt; in vitro test; mehaničko ponašanje; SEM analiza; ZrO<sub>2</sub>; zubni implantat; XRD analiza;

## 1 Introduction

The control and adaptation of the implant degradation rate are crucial, since the resorption capacity of the tissue is limited. Moreover, the local physiology of the implant environment determines the maximal degradation rate of a temporary implant.

There are many reasons that contribute to the corrosion of metals when implants are placed inside the human body. The existing in vitro corrosion test system always needs to be adapted to the corresponding in vivo application [1].

Permanent metallic implants can lead to certain biocompatibility problems related to continuous physical/mechanical irritation and long-term release of metallic ions and/or particles through corrosion or wear processes. The cast CoCrMo alloy was considered satisfactory for total hip replacements [2].

Co-Cr alloys are generally known for their excellent wear resistance where they have been in use in dentistry for many decades and in making artificial joints [3].

Co-Cr alloy powder used in DMLS manufacturing presents good sintering properties and grains of powder present spherical form necessary to obtain sintering probes [4]. The Co-Cr powder has grains of around 20 microns size [5-13]. Direct metal laser sintering (DMLS)

is a rapid prototyping technique and uses a laser as the power source and sinters the metallic powder material, aiming the laser automatically at points in space defined by a 3D model, binding the material together to create a solid structure. Co-Cr alloy presents good mechanical strength, good resistance to corrosion and a degree of cleaning identical to that of the glass [14-16]. Powder of Co-Cr alloy is considered tolerable in dentistry domain and is used for the realization of dental crowns, bridges and chapels. In the literature, no research has been made in vitro doping of Co-Cr alloy (ST2724G) with Zirconia in different percentages by mass.

Zirconia is a good ceramic bioactive material with excellent chemical and thermal resistance, toughness and mechanical strength. Deposition of ZrO<sub>2</sub> thin films on stainless steel 316L substrates by DC unbalanced magnetron sputtering leads to obtaining of ZrO<sub>2</sub> with monoclinic phase and bioactivity in SBF [17].

Researches have demonstrated the importance of preparation and phase structure in development of properties as bioactivity of zirconia [18].

Similar research concerning the biodegradation behavior has been realized on Co-Cr alloy using a human cell culture model and showed a higher corrosion rate in the presence of osteoblasts in the range of 25-30 % [19].

Research concerning biodegradation in SBF was realized on magnesium by chromium and oxygen dual ion implantation showing that Cr is a passive element that can be optimized to control the degradation of pure magnesium [20].

DMLS process permits manufacturing different personalized medical implants, microsurgical medical instruments with complex geometry. This technique realized personalized pieces with a great precision and faster. Medical microsurgery instruments must present good mechanical resistance and good corrosion resistance. Co-Cr alloy powder is a superalloy powder and is a tolerable material in medicine domain.

The Co-Cr powder presents good properties for sintering process, the grain size is very fine, 20 µm and the grain form is spherical.

In this paper experimental researches concerning mechanical resistance (traction and compression) and corrosion resistance in artificial saliva Fusayama Meyer of Co-Cr alloy samples have been carried out. The mechanical test realized on Co-Cr superalloy samples, shows a very good mechanical and corrosion resistance.

Some authors have conducted studies concerning mechanical and corrosion resistance of metals used in medical domain, like titanium alloy Ti6Al4V, Ti-Ni alloys, stainless steel 304 or 316L and Co-Cr alloys. In literature are reported Rockwell hardness of dental alloys, Co-Cr and Ni-Cr [21, 22].

## 2 Materials and methods

The compacts for dental implants with bioactive behavior in bone tissue were prepared starting from Co-Cr powders (ST2724G) used for direct metal laser sintering (DMLS) process. Commercial powder of ZrO<sub>2</sub> from Merck with a purity greater than 99 % was used for doping.

Co-Cr alloy used in this paper is of the following chemical composition: Co 54,31 %, Cr 23,08 %, Mo 11,12 %, W 7,85 %, Si 3,35 % and Mn, Fe < 0,1. The engineering properties of Co-Cr alloys (ST2724G) given by Phenix Systems [4] are:

- elastic limit 0,2 %  $R_{p0,2} = 815$  MPa
- elongation at break = 10 %
- Vickers hardness = 375 HV 5
- Elastic module = 229 GPa
- Volume mass = 8,336 g/cm<sup>3</sup>
- Corrosion resistance < 4 µg/cm<sup>2</sup>
- Thermal expansion coefficient =  $14,5 \times 10^{-6}$  K<sup>-1</sup>.

### 2.1 Co-Cr samples doped with Zirconia powder

Different compositions were obtained starting from powder Co-Cr and 5 %, 10 %, 15 %, 20 % ZrO<sub>2</sub> (percentage by mass). An undoped Co-Cr sample was used as reference. The raw materials powders were homogenized for 30 minutes, in ethanol. The compacts were compacted by pressing into the mold to active section of 1 cm<sup>2</sup>. Compacts were realized using the pressures of 20 kg/cm<sup>2</sup>.

The sinterization was made in an electrical furnace after a complex multistage regime. In the first stage of sintering the compacts were heated at a heating rate of 5

/min to 250 °C where a plateau of 10 minutes was maintained in order to remove water and organic residues, followed by the second stage of sintering at 700 °C for 30 minutes, using a heating rate of 10 °/min. The compacts were cooled naturally up to ambient temperature.

The sintered composite compacts were investigated by SEM, EDS and XRD analysis. The bioactivity was realized by immersion of sintered composite compacts in SBF for 21 days. In this period, the sintered compacts suffer biodegradability in SBF, evidenced by SEM, EDS and XRD analysis.

Investigation of morphology and quantitative analysis of compacts were performed using scanning electron microscope QUANTA INSPECT F (qualitative and quantitative analysis) equipped with electron gun with field emission -FEG (field emission gun) with a resolution of 1,2 nm and x-ray spectrometer for energy dispersive (EDS) with a resolution of 133 eV at MnK. For the chemical composition of the samples studied were used images of secondary electrons and backscatter electron images. The bright areas contain heavy elements (large atomic number) and the dark areas are light elements. The areas of interest were analysed qualitatively by micro compositional X-ray spectrometry.

XRD analysis was performed using an X-ray diffractometer that uses PAnalytical Empyrial characteristic CuKα radiation and wavelength 1,541874. Spectrum acquisition was performed in Bragg-Brentano geometry.

For mineralization assay, three compacts of each material were incubated in synthetic body fluid (SBF1x) at pH=7,4, adjusted with tris (hydroxy-methyl) aminomethane (Tris) and hydrochloric acid (HCl), for 21 days, under sterile conditions, in containers with 45 mL of the incubation medium at 37 °C. The incubation medium was changed every 48 h. After incubation, the specimens were rinsed with distilled water to remove any traces of salts from the surface and dried at 40 °C for 24 h. The composition of SBF1x is presented in Tab. 1.

**Table 1** Chemical composition of synthetic body fluid (SBF1x)

Ionic composition	Concentration (mM)
Na <sup>+</sup>	142,19
Mg <sup>2+</sup>	1,5
Ca <sup>2+</sup>	2,49
HCO <sub>3</sub> <sup>-</sup>	4,2
Cl <sup>-</sup>	141,54
HPO <sub>4</sub> <sup>2-</sup>	0,9
SO <sub>4</sub> <sup>2-</sup>	0,5
K <sup>+</sup>	4,85

The presence of mineral crystals on the surface was evaluated by SEM analysis. The Ca/P molar ratio was investigated by EDS spectroscopy. XRD patterns for mineralized compacts were obtained using a PAnalytical Empyrial diffractometer with CuKα radiation.

## 3 Results

### 3.1 Blind Co-Cr sintered compact

SEM (Fig. 1) and XRD (Fig. 2) analysis was realized for Co-Cr sintered composite as reference. The Co-Cr compact contains spherical grains of around 20 µm.

The great particles represent Co grains size and the smaller particles represent Cr grains size. The chemical composition was determinate by XRD and the result

shows the single face of chromium cobalt molybdenum with chemical formula Cr<sub>0,32</sub>Mo<sub>0,04</sub>Co<sub>0,64</sub> according to card 04-016-6870.

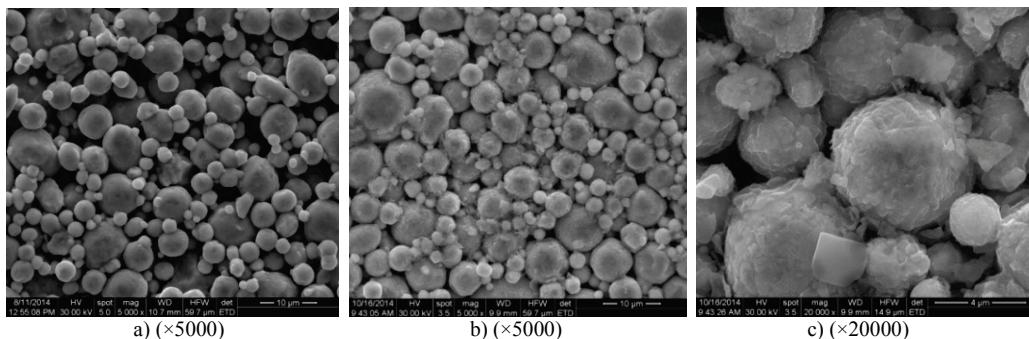


Figure 1 SEM images of the Co-Cr sintered compacts: a) before, b) and c) after immersion in SBF for 21 days

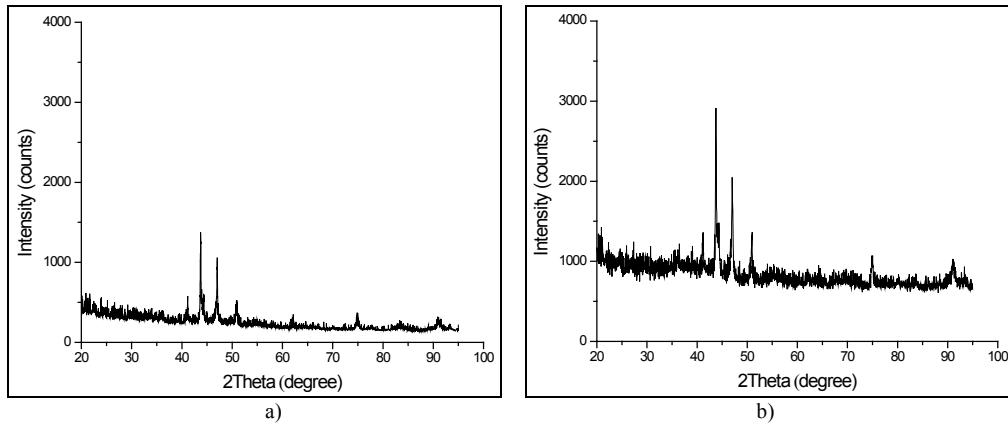


Figure 2 XRD patterns of the Co-Cr sintered compacts: a) before and b) after immersion in SBF for 21 days

In order to increase bioactivity of compacts, they were immersed in simulated biological fluid during 21 days, then were dried and analyzed. Results of SEM and XRD show small corrosion effects on the particles as can be seen in Figs. 1b, 1c and 2b.

### 3.2 Sintered compact of Co-Cr doped with 5 %wt ZrO<sub>2</sub>

In Fig. 3 are presented SEM images of sintered compact of Co-Cr doped with 5 %wt ZrO<sub>2</sub> at different magnifications. The compact sample of Co-Cr doped with 5 %wt ZrO<sub>2</sub> shows a uniform and dense microstructure.

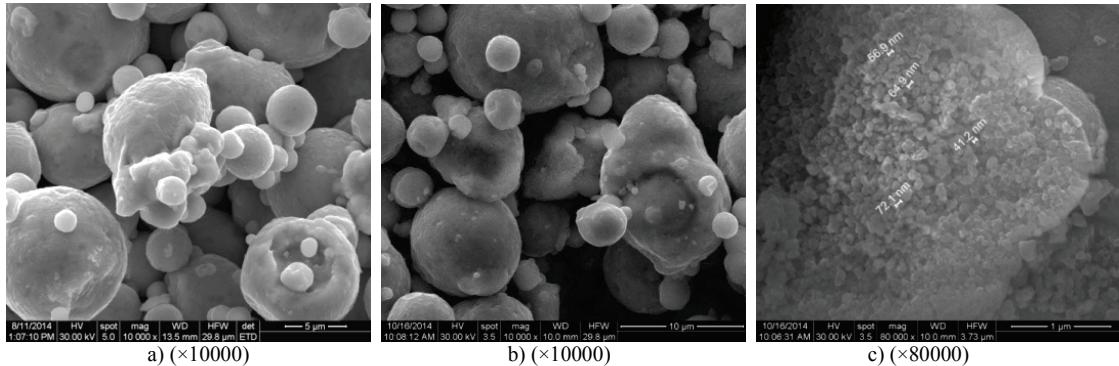


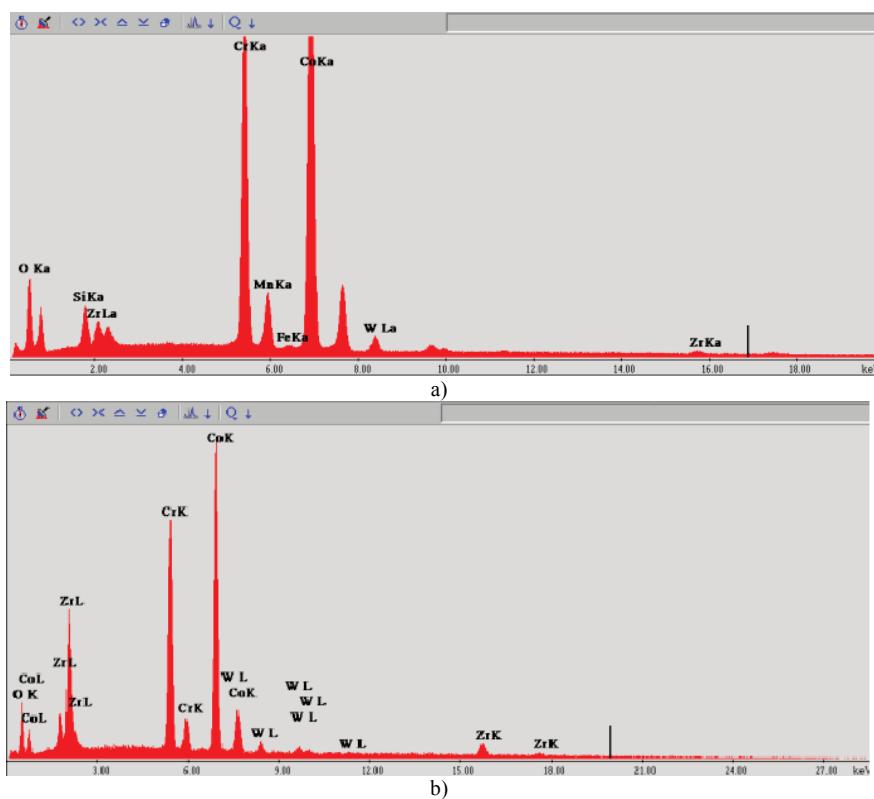
Figure 3 SEM images of sintered Co-Cr compacts doped with 5 %wt ZrO<sub>2</sub>: a) before, b) and c) after immersion in SBF for 21 days

Zirconia grains are of nanometrical scale with spherical grains. The compact shows a good compacting of grains that are not destroyed after immersion in SBF for 21 days (Fig. 3b and 3c). Some transformations of compact particles can be remarked. The compacts morphology shows some changes and damages; the particles are rounded to the existence of peeling particles like foils.

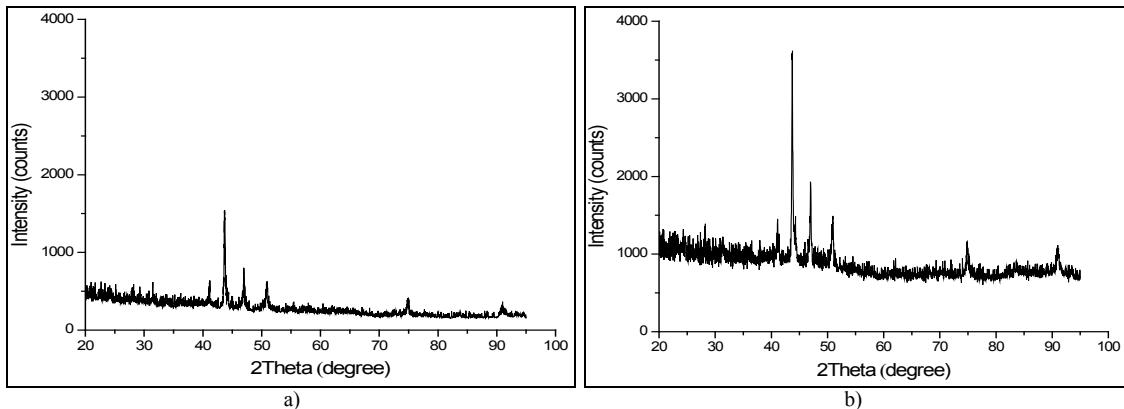
In Fig. 3b and 3c new areas of zirconia crystallites of nanometer sizes formed after immersion in SBF are

distinguished. Some ZrO<sub>2</sub> crystallites with size between 41–71 nm, are formed after immersion in SBF. Peaks of Ca, or P do not stand out; no hydroxyapatite appeared. EDS analysis (Fig. 4) shows that the zirconia is uniformly dispersed in the compacted sample.

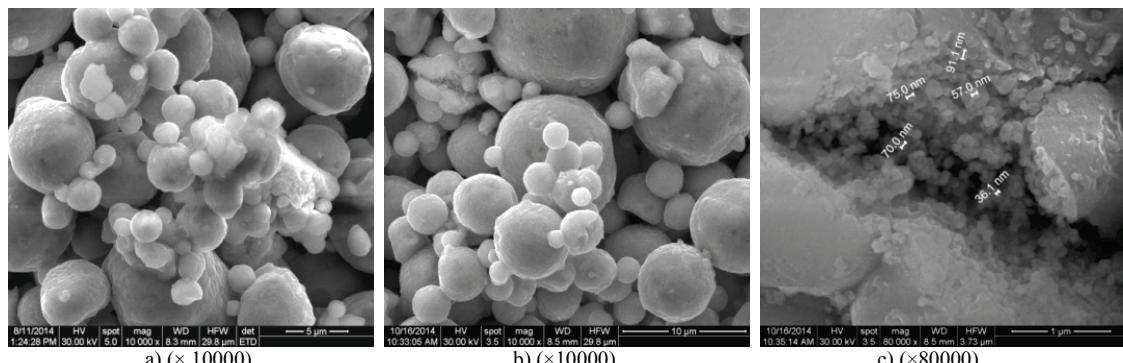
In Fig. 5 can be seen XRD pattern recorded on compact sintered sample of Co-Cr doped with 5 % ZrO<sub>2</sub> and the result presents a body centered cubic crystalline structure.



**Figure 4** EDS (quantitative and qualitative) analyses of sintered Co-Cr compacts doped with 5 % ZrO<sub>2</sub>: a) initially and b) after immersion in SBF for 21 days



**Figure 5** XRD patterns of sintered compacts of Co-Cr doped with 5 % ZrO<sub>2</sub>: a) before and b) after immersion in SBF for 21 days



**Figure 6** SEM images of sintered Co-Cr compacts doped with 10% ZrO<sub>2</sub>: a) before, b) and c) after immersion in SBF for 21 days

### 3.3 Sintered compact of Co-Cr doped with 10 %wt ZrO<sub>2</sub>

SEM images of Co-Cr compacts doped with 10 %wt ZrO<sub>2</sub> are presented in Fig. 6.

In the compact can be observed the uniform repartition of Co-Cr and ZrO<sub>2</sub> grains and the composition.

Zirconia is present as spherical grains with crystalline structure.

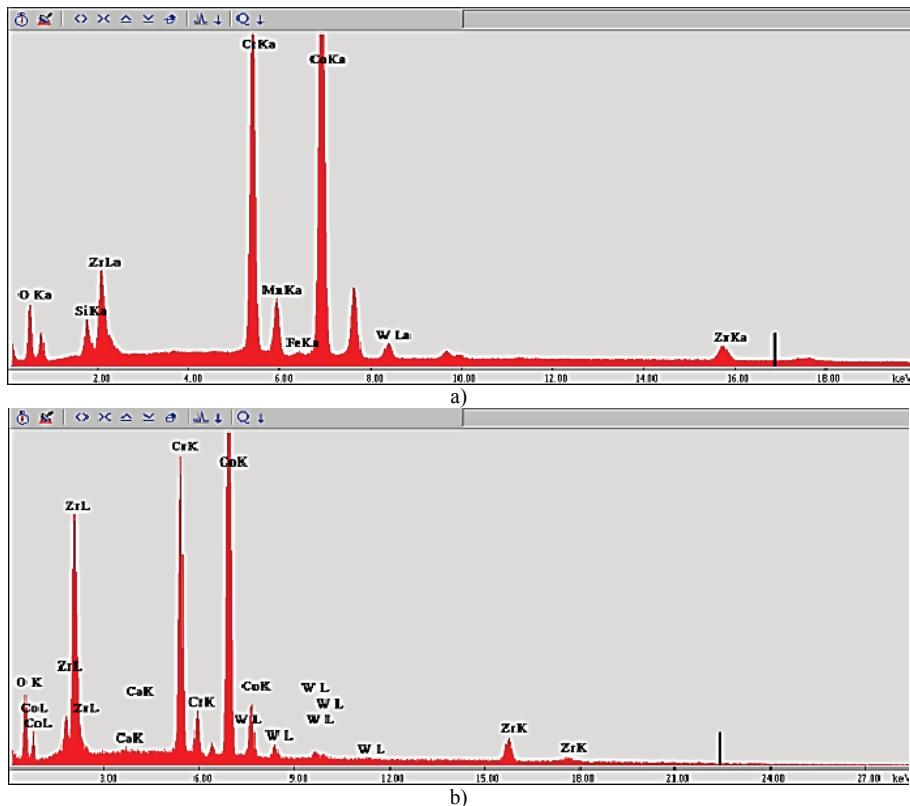
The sintered Co-Cr compact doped with 10 %wt ZrO<sub>2</sub> presents good compacting after immersion in SBF for 21 days (Fig. 6b and 6c). SEM images show the effects of biodegradability on the sintered compact as degradation

of particles. The particles become rounded with peeling like foils. After immersion in SBF new zones of zirconia crystallites of nanometer sizes can be determined.

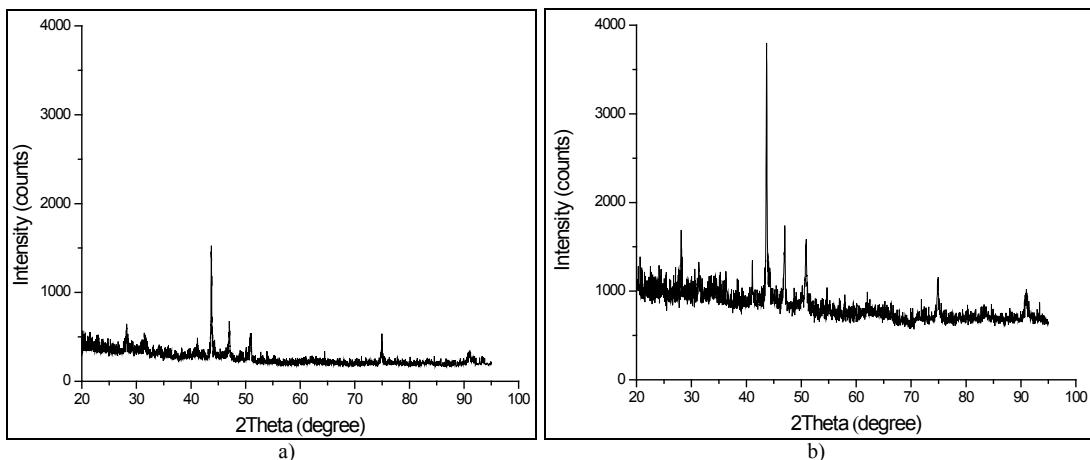
In some zones, the micrometric particles of ZrO<sub>2</sub> are transformed after immersion in SBF in nanometric crystallites. No hydroxyapatite was detected. EDS analysis (Fig. 7) shows the uniform distribution of ZrO<sub>2</sub> in the sintered compact of Co-Cr alloy before and after

immersion in SBF. EDS analysis evidenced small tracks of Ca (< 0,1 %).

The peaks of P are not visible because of superposing after the bands of Zr. In compact with 10 %  $ZrO_2$ , the zones with  $ZrO_2$  crystallites there are more nanostructures than in the compact doped with 5 %  $ZrO_2$ . In Fig. 8 the presence of zirconia 10 %  $ZrO_2$  in Co-Cr composite compact was revealed by XRD analysis.



**Figure 7** EDS (quantitative and qualitative) analyses of sintered Co-Cr compacts doped with 10 %wt ZrO<sub>2</sub>: a) initially and b) after immersion in SBF for 21 days



**Figure 8** XRD patterns of sintered compacts of Co-Cr doped with 10 %wt ZrO<sub>2</sub>: a) before and b) after immersion in SBF for 21 days

### 3.4 Sintered compact of Co-Cr doped with 15 %wt ZrO<sub>2</sub>

Fig. 9 reveals the microscopy SEM for compacts based on Co-Cr doped with 15 %wt  $ZrO_2$  with compact and uniform composition with a great quantity of  $ZrO_2$ .

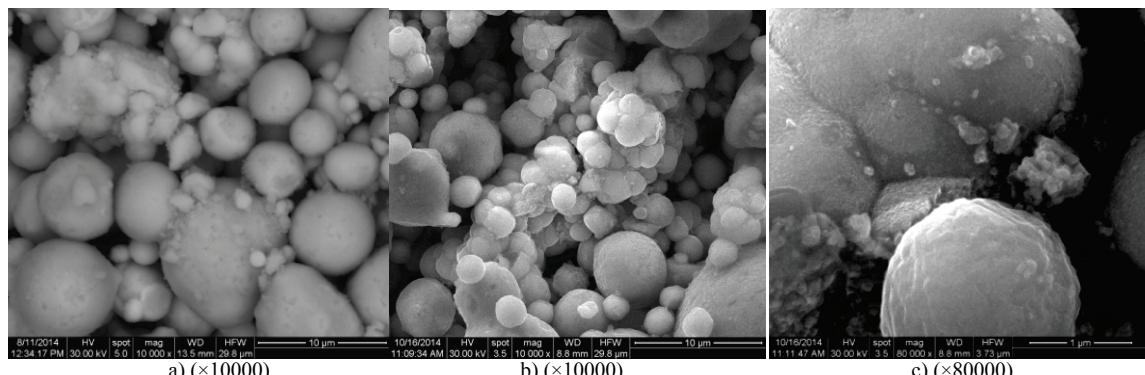
After immersion in SBF, some grains of  $ZrO_2$  are dissolved and nanometer zirconia crystallites appear. The presence of zirconia in sintered compact and uniform

dispersion can be spotted using EDS analysis. In EDS analysis the formation of small Ca and P peaks can be observed in Fig. 10.

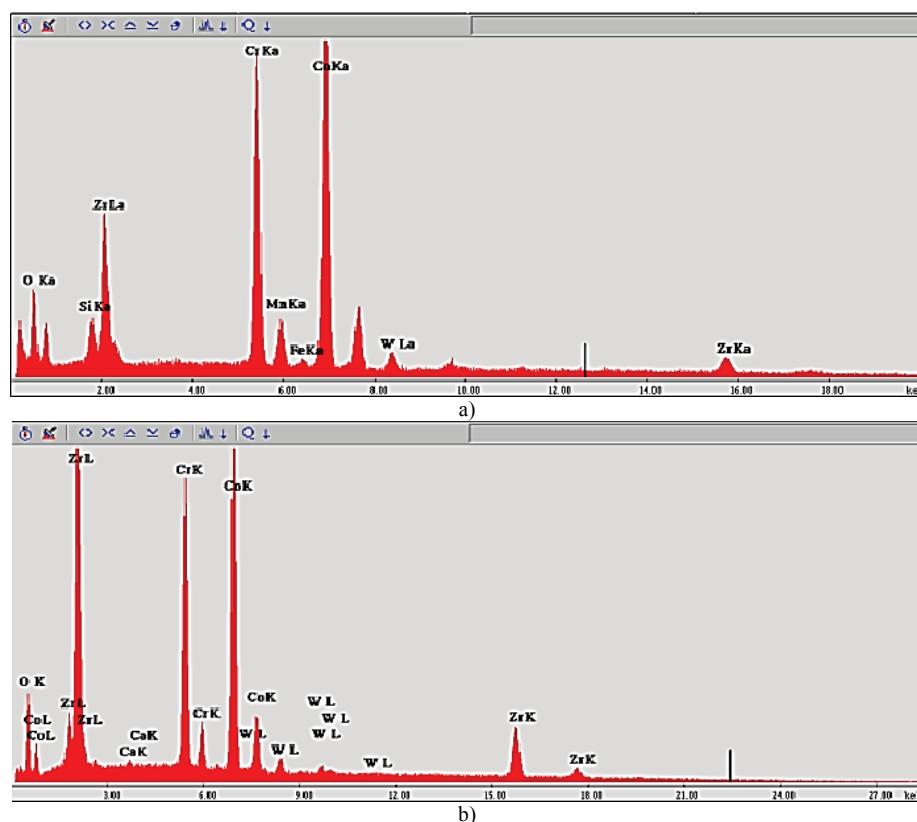
After immersion in SBF for 21 days, hydroxyapatite formation is possible in very small quantity (<0.1%), due to zirconia bioactivity. In Fig. 9 ( $\times 1000$ ) the large spherical particles are Co particles, the medium ones are Cr particles and the small ones are spherical zirconia.

The amount of 15 % ZrO<sub>2</sub> was determined using XRD analysis, like in Fig. 11. The hydroxyapatite amount

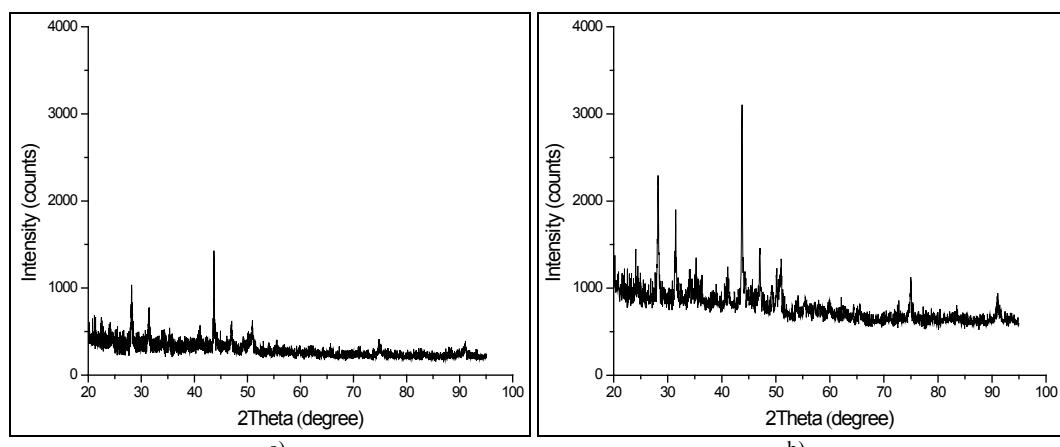
was not determined by XRD analysis, after immersion of sintered compact in SBF.



**Figure 9** SEM images of sintered compacts Co-Cr doped with 15% ZrO<sub>2</sub>: a) before and b-c) after immersion in SBF for 21 days



**Figure 10** EDS (quantitative and qualitative) analyses of sintered compacts of Co-Cr doped with 15 % ZrO<sub>2</sub>: a) initially and b) after immersion in SBF for 21 days



**Figure 11** XRD patterns of sintered compacts of Co-Cr doped with 15% ZrO<sub>2</sub>: a) before and b) after immersion in SBF for 21 days

### 3.5 Sintered compact of Co-Cr doped with 20 %wt ZrO<sub>2</sub>

SEM microscopy of the sintered compacts of Co-Cr doped with 20 %wt ZrO<sub>2</sub> is presented in Fig. 12.

The quantity of zirconia is very big and the dispersion is uniform. The small spherical grains are of ZrO<sub>2</sub>. After immersion in SBF during 21 days, in SEM image appear areas of very fine crystallites of ZrO<sub>2</sub> with size 31÷41 nm.

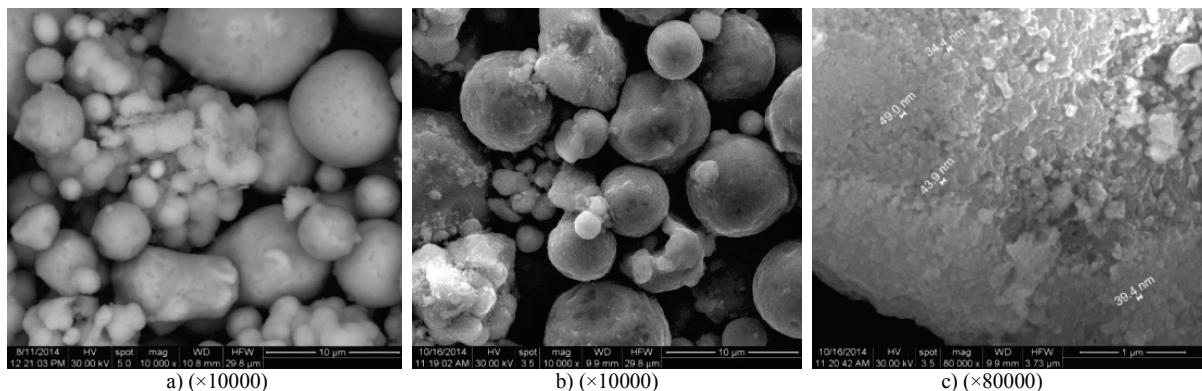


Figure 12 SEM images of sintered compacts of Co-Cr doped with 20 %wt ZrO<sub>2</sub>: a) before, b) and c) after immersion in SBF for 21 days

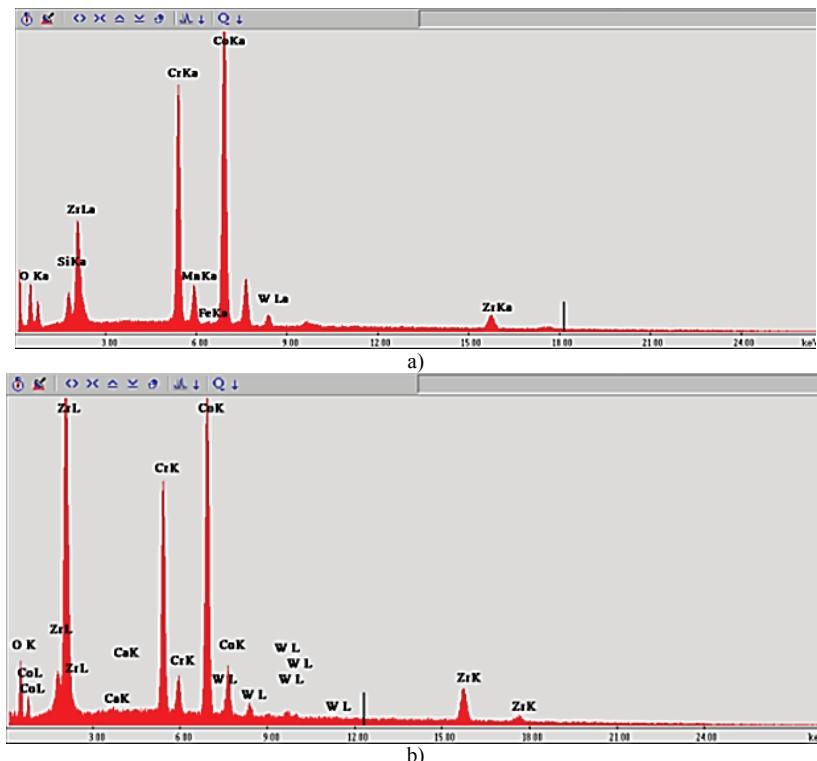


Figure 13 EDS (quantitative and qualitative) analyses of sintered compacts of Co-Cr doped with 20 %wt ZrO<sub>2</sub>: a) initially and b) after immersion in SBF for 21 days

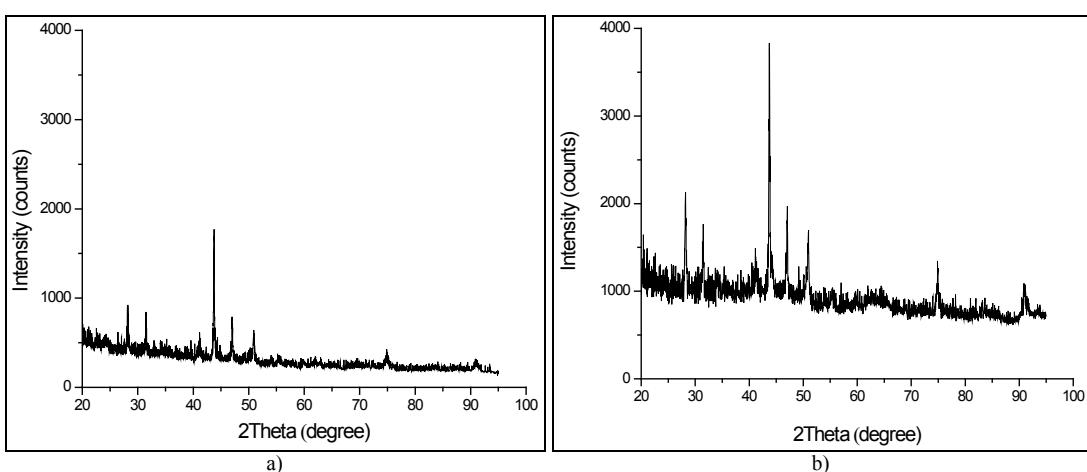


Figure 14 XRD patterns of sintered compacts of Co-Cr doped with 20% ZrO<sub>2</sub>: a) before and b) after immersion in SBF for 21 days

EDS mapping in Fig. 13a shows that the big spherical grains are assigned to Co-Cr and the small ones to ZrO<sub>2</sub> alloy.

Fig. 12b presents the compact after immersion in SBF for 21 days. The EDS spectrum shows low peaks for Ca (approximate 1 %) and the mapping shows the formation of a thin film of hydroxyapatite on the surface of the grains of compact.

If the maps of Ca, Co, Cr and Zr are compared one can remark the presence of the hydroxyapatite everywhere on the ZrO<sub>2</sub> grains and on the Co-Cr grains.

EDS analysis shows the presence of Ca peaks, in very small quantity. The P peaks are not visible because of the bands of Zr that are overlapping on the P bands.

This observation can be explained by possible formation of bonds Co-O-Zr and Cr-O-Zr in initial compact during the sinterization. In figure 14 are presented XRD patterns of compact doped with 20 % ZrO<sub>2</sub>.

Note that after immersion in SBF the compacts doped with high concentration of zirconia give them poor mechanical properties because they are brittle. It is optimal to recommend using Co-Cr sintered compacts doped with 5 % to 10 % ZrO<sub>2</sub>.

Co-Cr sintered compact doped with 5 % ZrO<sub>2</sub>, after SBF immersion during 21 days, presents a biodegradation, evidenced by SEM analysis. The Co-Cr grains are more rounded with fine degradation foils. After immersion of Co-Cr sintered compact with 5 % ZrO<sub>2</sub> in SBF, zones appear with fine crystallites of ZrO<sub>2</sub> of nanometric size between 41-71 nm.

For sintered compact of Co-Cr with 10 % ZrO<sub>2</sub>, after SBF immersion, Co-Cr grains suffer biodegradation and zones with finer zirconia crystallites appear comparing with the compact doped with 5 % ZrO<sub>2</sub>, as can be seen in SEM.

The size of crystallites is between 36÷75 nm. EDS analysis shows the presence of Ca peaks in small quantity (< 0,1 %). Due to bioactive behavior of ZrO<sub>2</sub> hydroxyapatite can appear in compacts.

In the case of the Co-Cr sintered compact with 15 % ZrO<sub>2</sub> the degradation of compact was observed after immersion in SBF during 21 days.

EDS analysis determines Ca peaks in small quantity (< 0,1 %). The quantity of ZrO<sub>2</sub> in sintered compacts is determined by XRD analysis.

After immersion in SBF for 21 days, the sintered Co-Cr compact doped with 20 % ZrO<sub>2</sub> presents some transformation and biodegradation of Co-Cr grains with rounded shape and zones with very fine nanometric zirconia crystallites of 36÷41 nm size. Remark the presence of Ca peaks in small quantity (approximately 0,1 %), by EDS analysis.

XRD analysis shows the presence of ZrO<sub>2</sub> in sintered compact (20 %).

#### 4 Mechanical tests of sintered powder of Co-Cr (ST2724G) by DMLS process

Six samples of Co-Cr (ST2724G), dental alloy manufactured by DMLS process were evaluated concerning mechanical properties, three samples for

traction test and the other three samples for compression test.

The samples are projected by SolidWorks soft and save like "stl" file.

The samples are sintered using Phenix Systems machine type PXS & PXM Dental, the fiber laser ( $P = 50$  W,  $\lambda = 1070$  nm), manufactured volume is  $100 \times 100 \times 80$  mm, machine dimensions are  $L = 1,20$  m;  $l = 0,77$  m;  $H = 1,95$  m. Machine soft used is Phenix Dental. The sintering temperature is 1300 °C. The nitrogen gas is used for the process.

#### 4.1 SolidWorks designing and DMLS manufacturing

The pieces necessary for research were designed by SolidWorks 2010 software. In figure 15 was designed the piece necessary for traction test and in figure 16 was designed the piece necessary for compression test.

The pieces design is realized like "sldprt" file and saved like "stl" to be viewed by computer of Phenix System PXS & PXM Dental machine.

The pieces are manufactured using Phenix System PXS & PXM Dental machine, by DMLS process.

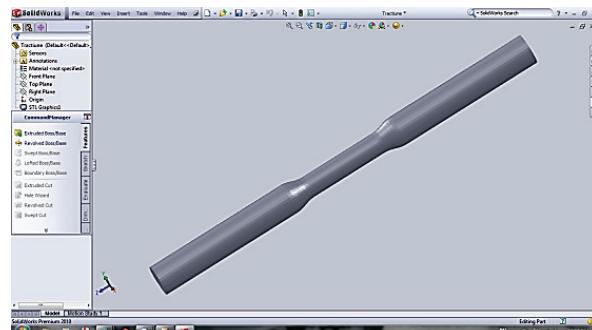


Figure 15 "stl" file of traction sample projected on SolidWorks

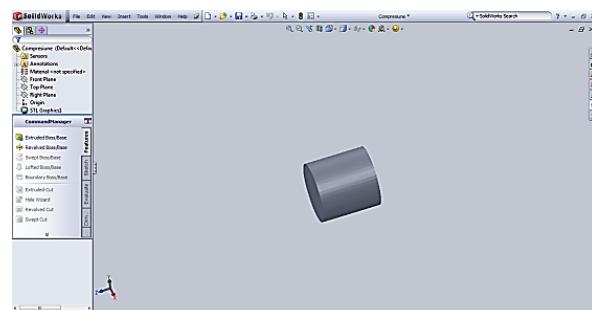


Figure 16 "stl" file of compression sample projected on SolidWorks

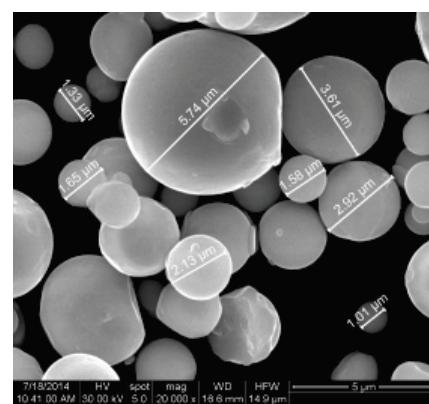


Figure 17 SEM analysis of Co-Cr alloy powder (×20000)

The SEM analysis of Co-Cr powder used by DMLS process is presented in Fig. 17 and the sintered pieces present the structure morphology like in Fig. 18.

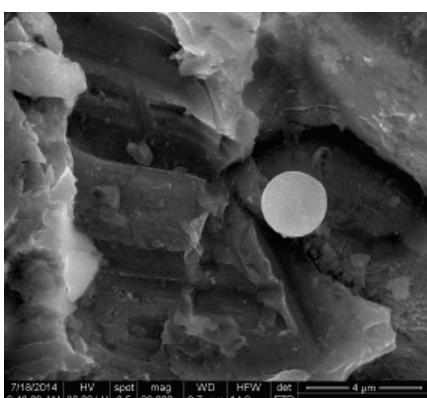


Figure 18 SEM analysis of sintered probe of Co-Cr alloy powder (x20000)

It can be seen from Fig. 17 that the Co-Cr alloy powder is very fine with spherical form of grain and grain size of around 20 µm. The sinterization process DMLS used a laser with power of 50 W, the temperature of sinterization varied between 1300 °C ÷ 1600 °C, the powder layer was approximately 20 µm.

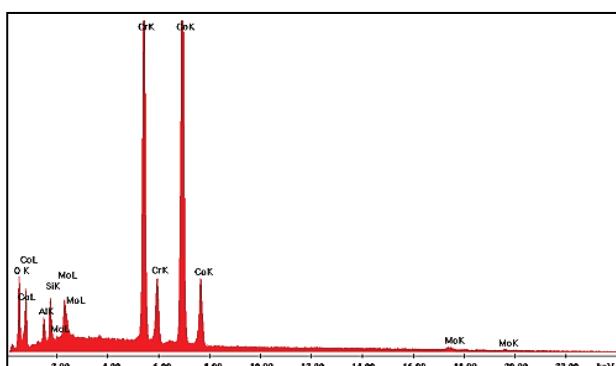


Figure 19 EDS analysis of sintered probe of Co-Cr alloy powder

The SEM analysis of sintered piece shows a porous material, like in Fig. 18. EDS analysis realized for the sintered piece shows the composition of Co-Cr alloy. After sinterization by DMLS process, the material shows great purity, like in the EDS analysis, Fig. 19.

#### 4.2 Mechanical tests - Traction test

Diameter of the traction sample is 5 mm in the center and 7 mm at the ends of sample. The length of the sample is 10 mm. The samples manufactured by DMLS present great precision and good mechanical properties. In Fig. 20 is presented the traction test on INSTRON 8810 machine using cross head speed of 0,5 mm/min. 3 samples were subjected to traction test.

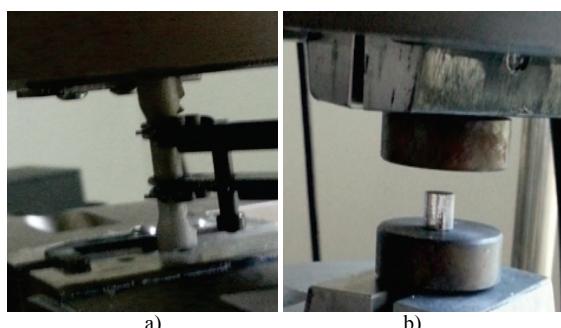


Figure 20 Traction test a) and compression test b) of Co-Cr alloy sample

In Tab. 2 are presented the values obtained after traction test of sintered sample of Co-Cr alloy by DMLS process. Good tensile of the sintered samples obtained by DMLS process can be noticed. The maximal tensile strength is around 1200 MPa.

Samples break suddenly perpendicular to the axis, around tensile strength of 1200 MPa and the strong fragile mechanical behavior can be observed. The morphological structure of Co-Cr alloy, after the traction test, was obtained by SEM analysis, like in Fig. 21.

Table 2 Traction strength of sintered samples of Co-Cr alloy by DMLS process

Nb. probe	Modulus (Segment 0,01 % ÷ 0,1 %) (MPa)	Tensile stress at Tensile Strength (MPa)	Tensile strain at Tensile Strength (%)	Diameter (mm)	Tensile stress at Yield (Offset 0,2 %) (MPa)
1	215070,31036	1199,20208	10,53235	4,92000	938,26940
2	220511,41664	1191,53786	11,52003	4,92000	841,89392
3	217965,73120	1197,37192	11,38575	4,92000	933,14574

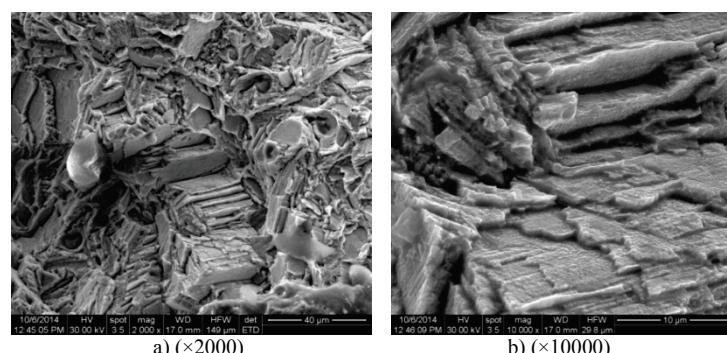


Figure 21 SEM analysis of traction test of sintered samples of Co-Cr alloy

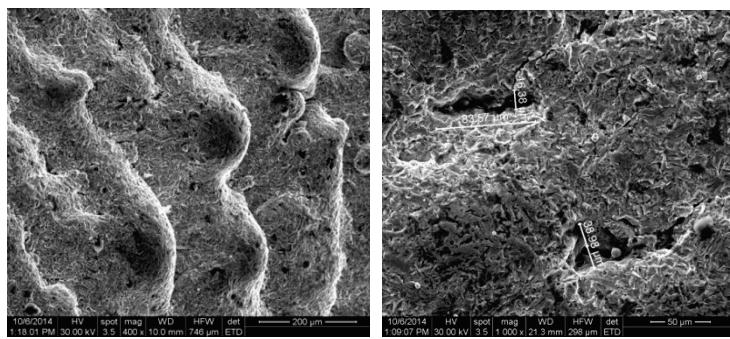


Figure 22 SEM analysis of compression test of sintered samples of Co-Cr alloy

After traction tests the material deformation, flattened pores, regular layers can be observed and the cracking is perpendicular on sample.

#### 4.3 Mechanical tests - Compression test

The compression samples are manufactured by DMLS and present great precision and good mechanical properties. Diameter of the compression sample is 7 mm in center and the length is 7 mm.

In Tab. 3 are presented the values obtained after compression test of sintered samples of Co-Cr alloy manufactured by DMLS process. The results show a good compression resistance and the maximal tensile is around 1200 MPa.

**Table 3** Compressive strength of sintered sample of Co-Cr alloy by DMLS process

Nb. probe	Compressive stress at Tensile Strength (MPa)	Modulus (Segment 2 % $\div 3\%$ ) (MPa)
1	1791,62067	10495,54594
2	1821,92217	15905,64368
3	1822,51273	15757,25712

SEM analysis presented in Fig. 22 shows the behavior at compression at 20 °C for Co-Cr sintered compacts. The samples present strong fragile mechanical behavior. The material deformation, flattened pores of 16 µm can be remarked. Strain hardening and some fine fissures are present in the material.

#### 5 Conclusions

In this paper, sintered compacts on the basis of the Co-Cr-doped with 5 %, 10 %, 15 %, 20 % by mass of ZrO<sub>2</sub> were obtained in order to use them for implants. Zirconia present a bioactive behavior and can increase the bioactivity of implants. The sintering treatment of Co-Cr compacts doped with ZrO<sub>2</sub> at 700 °C determines a dense structure of compacts with uniform distribution of grains of Co, Cr and ZrO<sub>2</sub>. SEM and EDS show high homogeneity of ZrO<sub>2</sub> in all compacts regardless of the amount used for doping. XRD analysis determines the presence of ZrO<sub>2</sub> in sintered compacts. The sintered compacts were immersed in SBF during 21 days, to determine the biodegradation behavior of Co-Cr compacts doped with different concentration of ZrO<sub>2</sub>.

In case of the sintered compacts Co-Cr doped with different concentration of ZrO<sub>2</sub> a good corrosion resistance in SBF was remarked.

After immersion in SBF, all sintered Co-Cr compacts doped with ZrO<sub>2</sub> present biodegradation, with grains that have rounded shape with some foils, determined by SEM analysis. The zirconia micrometric size is transformed after SBF immersion in nanostructure size. Zones with nanometric grains of ZrO<sub>2</sub> appear. For the sintered compacts with 10 %, 15 %, 20 % ZrO<sub>2</sub>, EDS analysis shows the presence of Ca peaks in small quantity (< 0,1 %). Due to bioactive behavior of ZrO<sub>2</sub> hydroxyapatite can appear in compacts. The quantity is very small and is shown only by EDS analysis.

Concerning the mechanical properties, the sintered Co-Cr compacts doped with 10 % and 15 % ZrO<sub>2</sub> are optimal to be used for dental implants manufacturing.

The sintered pieces obtained by DMLS manufacturing show very good mechanical properties and have fragile strength characteristics, because of porous structure specific to sintered pieces. The sintered samples show tensile resistance to traction of approximately 1200 MPa. During the compression tests, the sintered samples are damaged to the compression tensile at 1200 MPa. The mechanical resistance is satisfactory for a microsurgery instrument. The microstructure shows a deformation structure with flattened pores and some fine fissures.

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