EXPERIMENTAL AND NUMERICAL RESEARCH OF MECHANICAL BEHAVIOUR OF TITANIUM ALLOY HIP IMPLANT

Katarina Čolić, Aleksandar Sedmak, Kaled Legweel, Miloš Milošević, Nenad Mitrović, Žarko Mišković, Sergej Hloch

Experimental and numerical research of mechanical behaviour of hip replacement implant is presented. Experimental analysis was based on standard methods for testing mechanical properties and application of Digital Image Correlation (DIC) technique, while the Finite Element Method (FEM) was used for numerical simulation. A hip prosthesis extracted from a patient after revision surgery was used as the specimen. An adapter for the implant testing was constructed to enable the condition of a proximally loosened stem. During FEM analysis, a solid model was made of the assembly. An analysis of presented results indicated good agreement of experimental and numerical research.

Keywords: biomedical implant; digital image correlation; finite element method; Ti-6Al-4V alloy

Introduction

Hip replacement is a surgical procedure in which parts of a hip joint are removed and replaced with prosthesis, most commonly made of titanium-based alloys, especially Ti-6Al-4V, [1]. Although great advances have been made in this field, brittle fracture is still one of major problems associated with hip implant failure, [2-5], Fig. 1.

In vivo, each prosthesis component is subjected to a different set of loads that is specific to the individual patient. In addition, the anchoring conditions vary depending on the patient’s pre-existing diseases, design of prosthesis, quality of bone and surgical implantation techniques, [1, 6-9]. One should also keep in mind that scratches inevitably appear on implant surface, causing stress concentration, and providing location for crack initiation and propagation.

Therefore, despite strict regulation, hip implant failures still occur. Common causes are overloading and cracking, static or dynamic. Typical appearance of failure surface is given in Fig. 2, indicating relatively low toughness.

The main goal of this research was to examine hip implants, both experimentally and numerically, considering different forces acting on the prosthesis.

2 Experimental methodology

The human hip is a ball and socket joint, enabling movement in all directions. To accomplish this, a hip implant is composed of two sections, femoral head and femoral stem. During walking and jogging, the forces acting across the hip joint are several times higher than the body weight, [10]. The loads depend on the walking speed and the weight of the subject.

Throughout normal activity there are a variety of loads acting on the femoral stem and the acetabulum. The femoral stem is a loaded column, and the loads applied to it can be resolved into orthogonal loads acting along vertical, mediolateral, and anteroposterior axes, [10, 11]. Despite the progress in design and testing, fatigue fractures of hip stems still happen. The ISO 7206 standard
defines a laboratory test for determining the endurance properties of femoral components of hip prostheses, [12]. The current ISO 7206 standard defines that the load should be applied at an angle of 10° in adduction to the stem axis, Fig. 3.

Furthermore, test conditions are based on the conservative assumption that the stem becomes unsupported proximally, remaining restrained at 80 mm from the centre of the head of the prosthesis, [8÷10]. To analyse the mechanical behaviour of prosthesis, static testing was performed, based on the ISO 7206 standard, Fig. 3, with some modifications, as explained later.

The force on an implant during normal walking is cca 2,3 kN for a person of average weight (830 N), [10, 13]. However, as the relevant load one should take into account the worst-case scenario - falling over an obstacle (stumbling), which corresponds to the force 6 kN for a person of average weight, [10, 13].

To perform the experiment, an adapter to constrain the implant was constructed and used with the HB250 testing machine. During pre-testing research, a solid model of adapter was made, as shown in Fig. 4.

The experimental system for digital image correlation uses two matched digital cameras that provide a synchronized stereo view of the specimen. It also includes the stand that provides stability of the sensors, an image recording and power control unit, and the data processing system, [16].

3 Experimental results

Artificial hip prosthesis with a conical stem and a spherical femoral head, Fig. 6, removed during revision surgery, was used for testing. The femoral head was made of cobalt-chromium alloy, while the stem component was made of Ti-6Al-4V alloy by casting.

The appearance of hip implant after simple static testing is shown in Fig. 7, indicating large plastic strains.
The force vs. displacement (vertical movement of the loading cell) diagram in Fig. 8 indicates 7.7 kN as the maximum force before the occurrence of plastic straining, i.e. the yielding point. The maximum force during this experiment was cca 9 kN, as shown in Fig. 8.

Having in mind the basic mechanical properties of Ti6Al4V alloy, Yield Strength 780 MPa, Tensile Strength 860 MPa, Young’s modulus 120 GPa and Poisson’s ratio 0.3 [13], one can correlate Yield Strength with the force 7.7 kN, which represents the loading at yielding initiation. This sets the upper limit for linear elastic behaviour of the hip implant made of Ti6Al4V alloy, which is used in this research.

Results obtained by using DIC technique, for the load 6 kN, are shown in Fig. 9, for strain distribution, as well as in Fig. 10 for displacement distribution. One should notice that data in Fig. 9 is valid only for the stem, because only this portion of specimen was prepared for measuring. Therefore, one should take as relevant only the strains obtained in the stem, being at maximum (0.5%) approximately in the region which is typical for hip implant failure, as shown in Fig. 1. The corresponding level of stress is 600 MPa.

![Figure 6 Testing specimen](image1)

![Figure 7 Plastic strains after static testing of hip implant](image2)

![Figure 8 Diagram force-displacement for static testing of hip implant](image3)

![Figure 9 Strain distributions – force 6 kN](image4)
Experimental and numerical research of mechanical behaviour of titanium alloy hip implant

K. Ćolić et al.

Figure 10 Displacement distributions – force 6 kN [13]

4 Numerical analysis

The Finite Element Method has been applied to obtain linear elastic stress distribution in hip implant, loaded in the same way as during the experiment, with force of 6 kN. The mesh is generated so that problem is simulated as realistic as possible. Therefore, the adapter system has been modelled as well, following the solid model shown in Fig. 4. The finite element mesh is shown in Fig. 11.

Figure 11 The finite element mesh

Stress distribution obtained by applying such a model is shown in Fig. 12. The maximum equivalent stress is still in the linear elastic range (698 MPa), enabling simple calculation of the equivalent strain (698 MPa / 120 GPa = 0.0058 = 0.58 %). This is in relatively good agreement with the experimental results, obtained by DIC, shown in Fig. 9 (0.5 %, indicated by red colour). Also the location of maximum stress/strain is in good agreement (compare Figs. 9 and 12), as well as in good agreement with the typical fracture location, as seen in Fig. 1.

Figure 12 Stress distribution obtained by the FEM

Finally, if one takes into account yielding point as recorded during tensile testing, which means that stress level 780 MPa is reached by applying force 7.7 kN, it is clear that DIC measurement provides better agreement (stress 600 MPa - force 6 kN) than FEM (stress 698 MPa – force 6 kN). Possible cause of higher stresses in FEM is modelling of geometry in critical areas.

5 Conclusions

The results of this study show that understanding of mechanical loading and behaviour of a hip implant is very important. Based on the results of experimental and numerical research, one can conclude the following:

• Behaviour of hip implant under 6 kN force, corresponding to the worst case scenario (stumbling), is linear elastic.
• Experimental (DIC) and numerical (FEM) results are in good mutual agreement, difference being cca 15 %.
• Both experimental and numerical simulation of testing of hip implant provide sound basis for further research, since the results are in good agreement with the real ones, being in almost perfect match for DIC measu-
rement, whereas FEM results predict cca 15% larger stresses.

Acknowledgements

The research work is funded by the support of the Ministry of Education and Science of the Republic of Serbia - Contract grants: TR 35040.

Note: This paper is extended and improved version of the paper "Design aspects of fracture behaviour of Titanium artificial hip implant" presented at the Int. Conf. TEAM 2013, in Presov, Slovakia, [21].

6 References


Authors’ addresses

Katarina Ćolić, PhD
University of Belgrade, Innovation Center of Faculty of Mechanical Engineering, Kraljice Marije 16, 11 000 Belgrade, Serbia
kbojic@mas.bg.ac.rs

Aleksandar Sedmak, PhD
University of Belgrade, Faculty of Mechanical Engineering, Kraljice Marije 16, 11 000 Belgrade, Serbia
asedmak@mas.bg.ac.rs

Kaled Legweel, Ph.D. student
University of Belgrade, Faculty of Mechanical Engineering, Kraljice Marije 16, 11 000 Belgrade, Serbia

Miloš Milošević, PhD
University of Belgrade, Innovation Center of Faculty of Mechanical Engineering, Kraljice Marije 16, 11 000 Belgrade, Serbia
mmilosевич@mas.bg.ac.rs

Nenad Mitrović, PhD
University of Belgrade, Faculty of Mechanical Engineering, Kraljice Marije 16, 11 000 Belgrade, Serbia
nmitrovic@mas.bg.ac.rs

Žarko Mišković, MSci
University of Belgrade, Faculty of Mechanical Engineering, Kraljice Marije 16, 11 000 Belgrade, Serbia
zmiskovic@mas.bg.ac.rs

Sergej Hloch, PhD
Faculty of Manufacturing Technologies of Technical University of Kosice with seat in Presov, Bayerova 1, 080 01 Prešov, Slovak Republic

Institute of Geonics Academy of Science of Czech Republic, v.v.i., Studentska 1768, 708 00 Ostrava-Poruba, Czech Republic
hloch sergej@gmail.com