

## Fractures of clasp-retained partial dentures

**Dragoslav Stamenković**

Department of Dental Prosthetics, University School of Dental Medicine, Belgrade

### Summary

Fractures of cast clasps are practically irreparable and impair both therapeutic and prophylactic value of partial dentures. On purpose to explain causes of this rather frequently occurring damage, examination of fracture surface with optical and electronic microscopes and assessment of stress in the retainers were carried out. Microscopic examinations comprised fracture surfaces of 30 cast clasps divided into 2 groups: Group I (control group): cast clasps formed and cast under controlled laboratory conditions; Group II (test group): fractured cast clasps. It was found that surfaces of cast clasp fractures had a complex structure containing developed dendrites and separated carbide phases. In contrast to the control group, fracture surface from the test group showed signs of alloy fatigue, increased porosity and presence of new phases. On base of the analysis of partial denture movement it was assessed that stress in cast clasps approached both proportionality and fatigue level. In the conclusion it is pointed to two main factors causing cast clasp fractures: plastic deformation and material porosity.

**Key words:** cast clasp, microstructure, assessment of stress.

### INTRODUCTION

Fracture of different framework parts is, unfortunately, a frequently occurring damage. According to clinical experiences, cast clasps are most often subject to fracture. After them come minor connectors, while fractures of lingual and palatal bars take place rather seldom and those of broad palatal major connectors only in exceptional cases. (Bates<sup>1</sup>, Earnshaw<sup>2</sup>, Harcourt<sup>3</sup>)

On purpose to find an explanation of a large number of retainer fractures particularly in comparison with fractures of other framework parts, following research objectives were set:

(1) To analyse microstructure of cast clasp made under controlled laboratory conditions.

(2) To analyse microstructure of fractured cast clasps.

(3) On base of micrograph comparison and assessment of stress in the cast clasp to suppose causes of fractures.

## MATERIALS AND METHODS

A clinical examination of 400 partial dentures that had been in use for 2–5 years discovered 69 fracture surfaces on 62 frameworks. These fractures were mostly found on cast clasps and impaired both prophylactic and therapeutic value of partial denture. Table 1.

Table 1

LOCATION OF PARTIAL DENTURE FRACTURE SURFACE					
		Location	number	%	
1	CAST CLASP	rest . . . . .	11	61	88,4
		retentive clasp arm . . . . .	31		
		stabilizing clasp arm . . . . .	12		
		clasp body . . . . .	7		
2	MINOR CONNECTORS		4		5,8
3	MAJOR CONNECTORS	lingual bar . . . . .	2	3	4,3
		palatal bar . . . . .	1		
4	BROAD PALATAL MAJOR CONNECTOR		1		1,4
total number of fracture surface found in 400 examined partial dentures			69		100,0

Frameworks were cast from cobalt-chromium alloy supplied by the Krupp Company, WG. Clasps to be examined were divided into two groups:

GROUP I 6 clasps assemblies formed and cast under controlled laboratory (control group) conditions.

GROUP II 24 fractured cast clasps (10 clasp assemblies, 10 bar clasp arms, (test group) 2 back-action clasps and 2 ring clasps).

Microscopic examinations were performed on an optical metallographic microscope and a scanning electron microscope (SEM).

Three clasps from Group I and 12 from Group II were cut and ground with abrasive papers from 2/00 to 5/00. Then they were polished by means of machine with abrasive paper and Al<sub>2</sub>O<sub>3</sub> suspension (alumina). Electrolytic etching was carried out in two 30-second periods with 10% HClO<sub>4</sub> solution in C<sub>2</sub>H<sub>5</sub>OH and a 5V electric circuit.

Fracture surfaces of 12, not specially prepared, cast clasps from the Group II were subjected to SEM examination. For the comparison served SEM micrographs of fracture surfaces on 3 clasps fractured (Group I) on purpose in a specially assembled apparatus.

## RESULTS AND DISCUSSION

Cast clasps from Group I had a complex microstructure containing developed crystallographically favourable oriented dendrites and a separated carbide phase.

Carbides were located along grain boundaries and in interdendrits areas in form of continuous formations. In addition there were present eutectic phases and micropores in a smaller extent (Figures 1, 2 and 3., Table 2.).

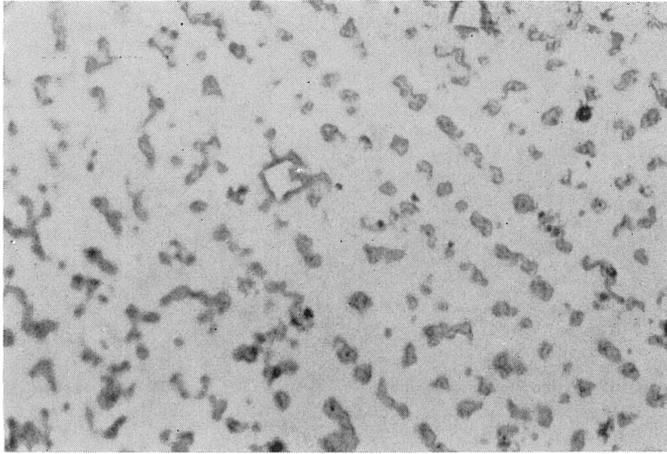


Fig. 1. Metallographic micrograph of a clasp assembly fracture surface.  $\times 300$ .

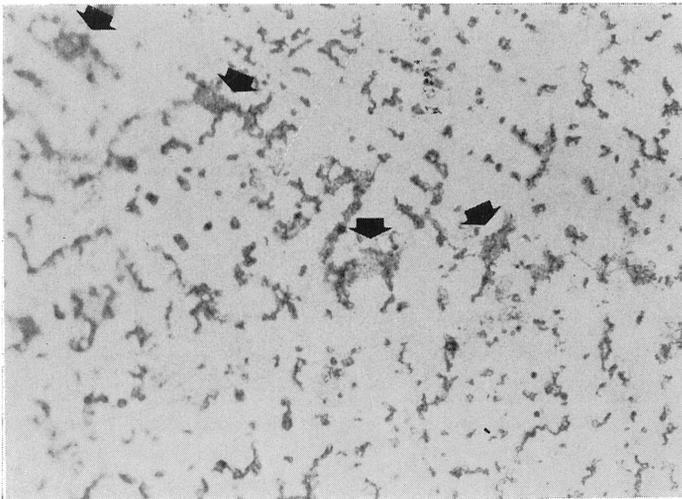


Fig. 1a. Metallographic micrograph of a bar clasp arm fracture surface. Arrow points to dark eutectoid areas lamellar in nature.  $\times 300$ .

Microstructure of cast clasps from Group II was also complex with more or less developed dendrites and material segregation. Carbide phase was in form of both continuous and discontinuous carbide formations separated along grain

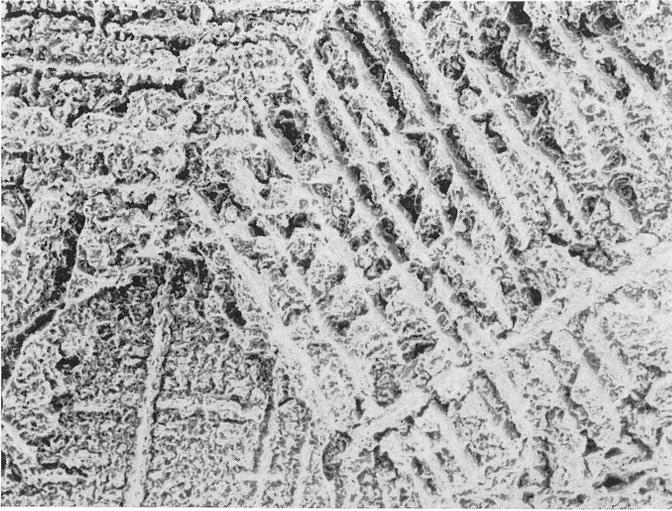


Fig. 2. SEM micrograph of a clasp assembly fracture surface.  
× 120.

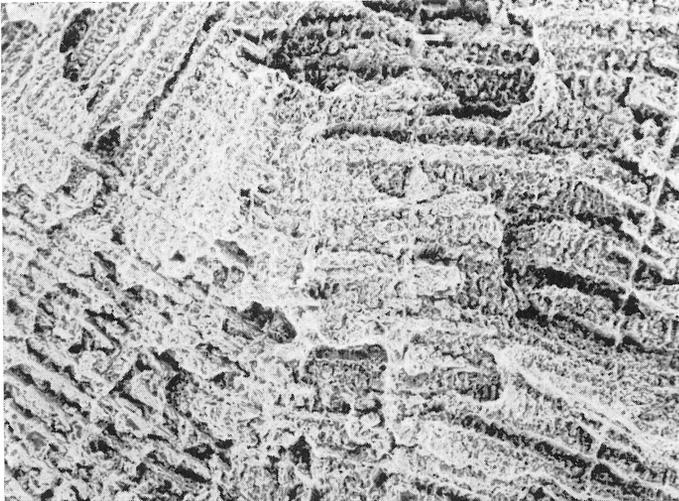


Fig. 2a. SEM micrograph of a clasp assembly fracture surface.  
× 120.

boundaries and in interdendrite areas. It was also characterised by the presence of dark eutectoid areas lamellar in nature (Figures 1a, 2a, 3a, 4, 5, 6, and 7. Table 3).

In many cases microscopic examinations revealed material porosity with heterogeneously distributed micropores and microcavities (Figures 8. and 8a). Micropores were situated within a relatively small area and represented points at which initial fractures took place when small quantities of energy were introduced. (Lewis').

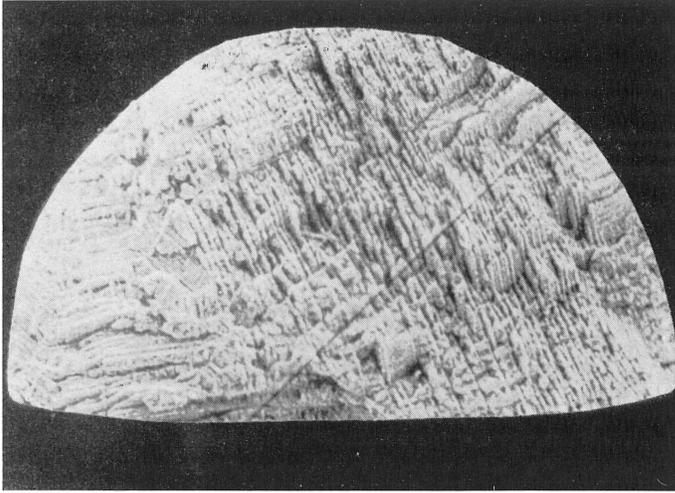


Fig. 3. SEM micrograph of a retentive clasp assembly arm fracture surface. Fracture provoked by a 29 N load on a specially assembled apparatus.  $\times 50$ .

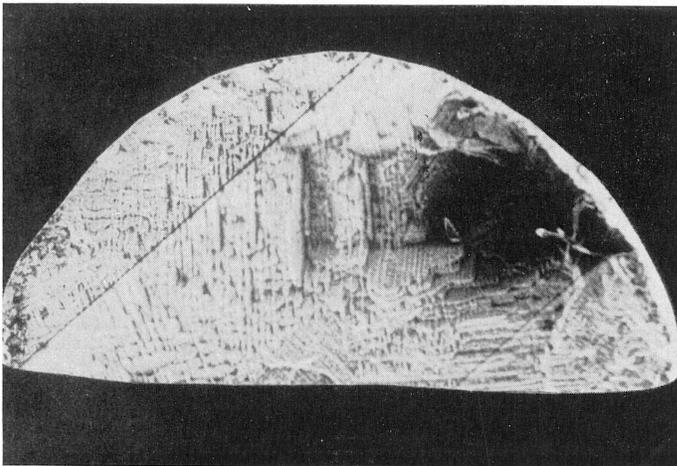


Fig. 3a. SEM micrograph of a clasp assembly fracture surface. Fracture occurred due to the presence of a macrocavity and many micropores in the moment the partial denture was handed to the patient.  $\times 50$ .

#### Assessment of stress in major connectors and cast clasps of partial denture

Stress in lingual and palatal bars are half as high as proportionality limit and pretty below the limit fatigue. (Bates<sup>1</sup>, Stamenković<sup>3</sup>) Therefore fractures of major connectors occur very seldom in the mouth. In course of a 10-years period of use under load in swallowning and chewing processess major connectors are subjected

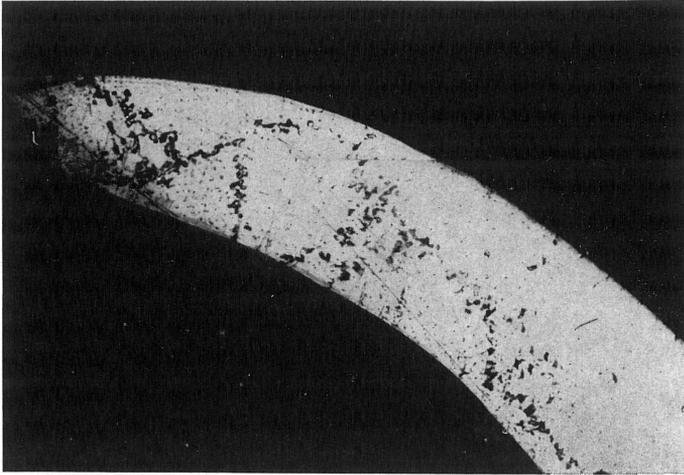


Fig. 4. Metallographic micrograph of a retentive clasps arm fractured after 1,5 year of use. In the microstructure prevail large grains with carbide phase along grain boundary.  $\times 20$ .

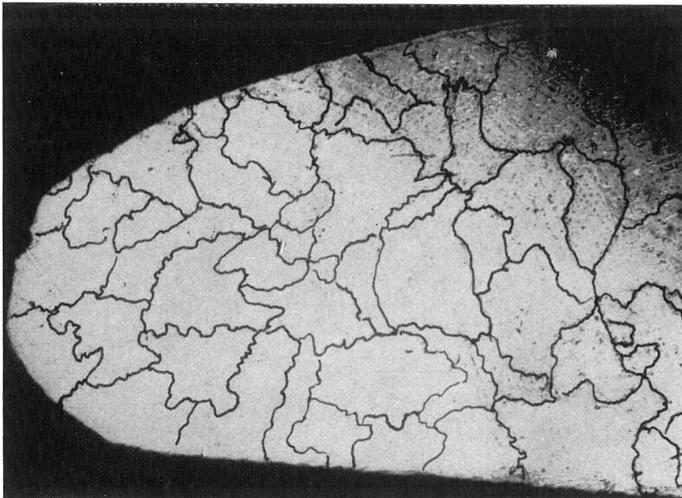


Fig. 5. Metallographic micrograph of the longitudinal section of a rest fractured after 9 years of denture use. Boundaries of extremely fine grains may be seen on the micrograph. There is no developed microstructure.  $\times 20$ .

to a great number of stress that according to Brewer and Hundson amount to  $5 \cdot 10^6$  microinsults. (Bates<sup>1</sup>). Stress in retentive clasp arms approaches both proportionality and fatigue limit. (Bates<sup>1</sup>, Stamenković<sup>5</sup>) However, stress in incorrectly shaped cast clasps may reach the limit fatigue and provoke fracture. In course of

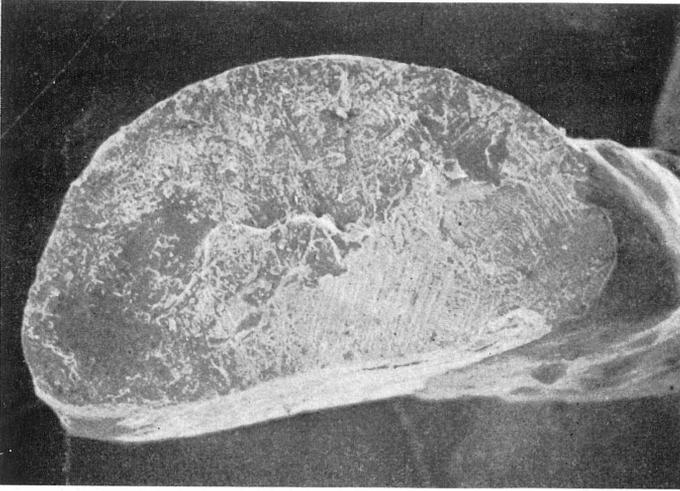


Fig. 6. SEM micrograph of a retentive clasp assembly arm fracture surface.

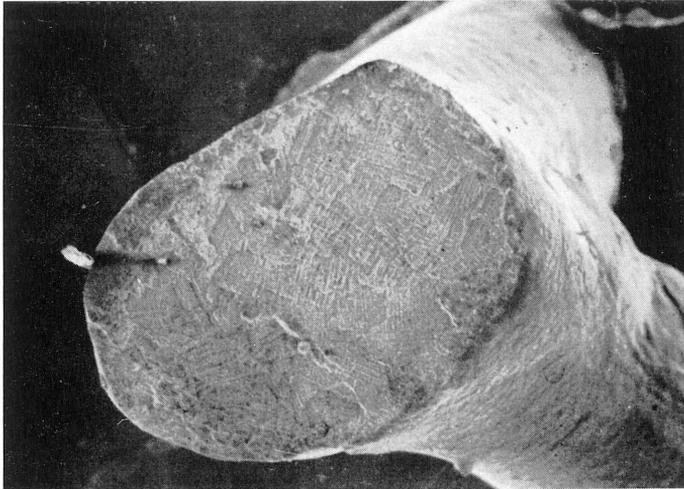


Fig. 7. SEM micrograph of a retentive bar clasp arm fracture surface.

a 10-year period of use, a partial denture is alternatively put in and taken out of the mouth, so that retentive clasp arms suffer a relatively small number of macroinsults: about 10.000 (Babić<sup>6</sup>) or 30.000 (Bates<sup>7</sup>). Consequently, major connectors are subjected to low, but numerous stresses of no essential influence on alloy fatigue, while retentive clasp arms support high, but fewer stress that under given circumstances may lead to plastic deformation. These facts confirm clinical

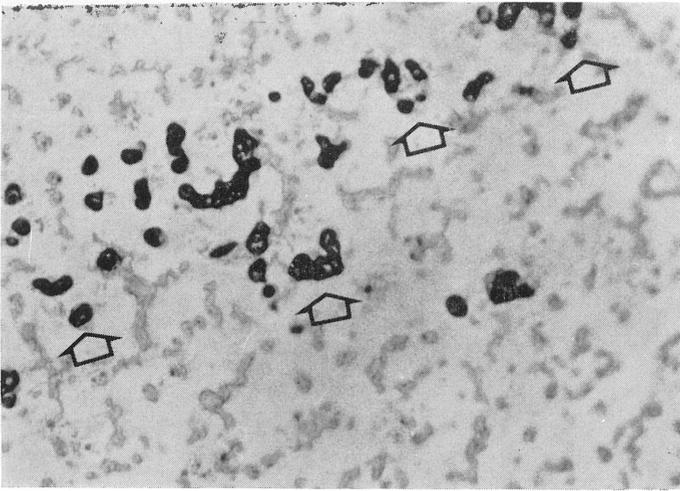


Fig. 8. Metallographic micrograph of a bar clasp arm fracture surface. Arrow points to micropores.  $\times 400$ .

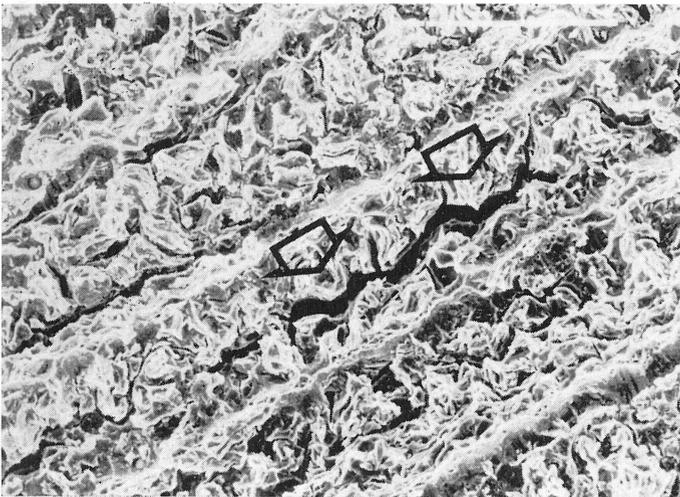


Fig. 8a. SEM micrograph of a back-action clasp fracture surface. Arrow points to micropores.  $1000 \times$ .

experiences according to which fractures and plastic deformation of retentive clasp arms take place very often and those of bars relatively seldom. Experimental measurements have shown that a 15–20 N force provokes plastic deformation of retentive clasp arms, while a force above 20–30 N causes cast fracture in most cases, (Stamenković<sup>3</sup>).

Table 2

CHARACTERISTICS OF GROUP I  
CAST CLASPS MICROSTRUCTURE

GRAIN	— Larger with developed and favourably crystallographically oriented dendrites.
PHASES	— Continuous carbide formations separated along grain boundaries and in interdendrite area. — Eutectic areas.
POROSITY	— Smaller number of micropores.

Table 3

CHARACTERISTICS OF GROUP II  
CAST CLASP MICROSTRUCTURE

GRAIN	— Larger with developed dendrites and/or — smaller with less developed dendrites and material segregation.
PHASES	— Continuous carbide formations. — Discontinuous carbide formations. — Eutectic areas. — Dark eutectic areas lamellar in nature.
POROSITY	— Larger number of micropores. — Smaller number of micro and macrocavities.

**CONCLUSION**

It is fully justified to make researches related to fractures of partial denture cast clasps, since elimination of main factors causing these fractures creates new possibilities for increasing prophylactic value of partial dentures, and thereby also new perspectives for the reparatory therapy in the field of dentistry.

Cast clasp fractures result mostly from a joint action of several factors. As it may be concluded from all abovesaid, main factors inducing these fractures are:

(1) material porosity due to incorrectly performed laboratory procedures for alloy melting and casting and

(2) plastic deformation resulting from putting partial denture in and taking it out of the mouth by force and at a wrong angle, as well as from »adjusting« cast clasps with forceps.

## References

1. BATES, J. F.: Studies Related to the Fracture of Partial Dentures, Brit. Dent., J., 120:79, 1966.
2. EARNSHAW, R.: Fatigue Tests on a Dental Cobalt-Chromium, Brit. Dent., J., 110: 341, 1961.
3. HARCOURT, H. J.: Fractures of Cobalt-Chromium Castings, Brit. Dent. J., 110: 43, 1961.
4. LEWIS, A. J.: Radiographic evaluation of porosities in removable partial denture castings, J. Prosth. Dent., 39:278, 1978.
5. STAMENKOVIĆ, D. S.: Analiza svojstava i vrednosti retencionog sistema skeletirane proteze, Ph. D. Thesis, Belgrade, 1983.
6. BABIĆ, B., STAMENKOVIĆ, D. S.: Analiza faktora elastičnosti Ney-evog retencionog sistema skeletiranih proteza, SGS, 4:257, 1979.
7. BATES, J. F.: Clinical and laboratory studies on the behavior of cobalt-chromium alloys as partial denture materials, DDS Thesis, Manchester, 1963.

## Sažetak

## ANALIZA PRELOMA SKELETIRANIH PROTEZA SA LIVENIM KUKICAMA

Praktično nemogući za reparaturu, prelomi livenih kukica skeletiranih proteza umanjuju terapijsku i profilaktičnu vrednost proteze. Sa ciljem da se objasne uzroci, ovoj relativno čestoj pojavi, obavljena su optička i elektronska mikroskopska ispitivanja prelomnih površina i procenjeni su pritisci u retencionim elementima. Mikroskopska ispitivanja su obavljena na ukupno 30 prelomnih površina livenih kukica, svrstanih u dve grupe: 1. grupa (kontrolna) — livene kukice modelovane i livene pod kontrolisanim laboratorijskim uslovima. 2. grupa (ispitivana) — prelomljene livene kukice. Prelomne površine livenih kukica imaju složenu mikrostrukturu sa razvijenim dendritnim granama i izdvojenom karbidnom fazom. Za razliku od kontrolne grupe, ispitivana grupa prelomnih površina pokazuje znakove zamora materijala, prisustvo novih faza i povećanu poroznost materijala. Nakon analize kinematike skeletirane proteze procenjeno je da je pritisak u livenim kukicama u blizini tačke proporcionalnosti i blizu granice zamaranja. U zaključku su izdvojena dva najvažnija uzroka preloma livenih kukica: plastična deformacija i poroznost materijala.

**Ključne reči:** livene kukice, mikrostruktura, procena pritiska