

Mechanical Properties Testing of P92 Welded Joints Prepared by Manual Metal Arc Welding

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Abstract: This article deals with the new results from measurement of mechanical properties of P92 welded joints. Tested welded joints of P92 steel were prepared using Gas Tungsten Arc Welding (GTAW) for root layer in combination with Manual Metal Arc Welding (MMAW) for filler layers. After the welding, the different modes of Post Weld Heat Treatment (PWHT) were made and the values of hardness, tensile strength and impact toughness of weld metal and Heat-Affected Zone (HAZ) were measured.

Keywords: Gas Tungsten Arc Welding; hardness; impact energy; Manual Metal Arc Welding; tensile strength; welding

1 INTRODUCTION

With development of new electrical devices, the worldwide energy consumption increases. In order to respond to this increasing consumption, it is necessary to build new energetic facilities and to improve their components. Many of these components are exposed to high temperatures and pressures of the water or steam located in the valve system. Higher values of temperatures and pressures are connected with the higher effectivity of power-plants and with the fuel saving and less amount of CO₂ emission [1]

With increasing effectivity of power-plants it is necessary to use new modern materials. These materials should resist high temperatures and pressures and have to be very reliable, because every failure of the steel can have critical consequences. To prevent these failures the increased attention has to be paid to metallurgical composition of used steel, strength calculation of each part and to the joining of these parts – welding.

One of these creep-resistant materials is martensitic steel with the designation P92, which is very often used to build parts exposed to high temperatures and pressures of steam in supercritical blocks of the thermal power-plants [2]. Due to martensitic microstructure, welding of this steel is difficult. Especially, there is only little information concerning the influence of the welding method and the PWHT on mechanical properties of the heat-affected zone.

Welding is a special process of joining, because it causes thermal effects on the surroundings of welded joint and weld metal itself. These thermal changes lead to structural changes and degradation of material properties especially in heat-affected zone. Unwanted effect of welding can be partly removed by the heat treatment with the advantageous setup of the temperature and duration [3]. That is why the research of the post weld heat treatment modes has to be carried out. Based on the results from the experiment it is possible to evaluate the properties after the heat treatment and choose the mode with the best ratio of mechanical and elastic properties.

2 EXPERIMENT

Testing specimens (18 mm thick plates of P92 steel) were prepared using Gas Tungsten Arc Welding (GTAW) for root layer in combination with Manual Metal Arc

Welding (MMAW) for filler layers. Example of macrostructure of the weld can be seen in Fig. 1. The list of filler materials is given in Tab. 1, welding parameters can be seen in Tab. 2. Preheat temperature was 240 °C, interpass temperature did not exceed 300 °C. After welding the different modes of Post-Weld Heat Treatment were carried out (see Tab. 3).



Figure 1 Macrostructure of welded joint

Table 1 List of filler materials

| Type | Designation | Manufacturer |
|--|-------------------|--------------|
| Wire | Thermanit MTS 616 | Böhler |
| EN 12070-WZ CrMoWVNb 9 0,5 1,5 | | |
| Type | Designation | Manufacturer |
| Gas | Argon 4.6 | SIAD |
| EC: 231-174-0 | | |
| Type | Designation | Manufacturer |
| Electrode | Thermanit MTS 616 | Böhler |
| EN ISO 3580-A – EZ CroWVNb 9 0,5 2 B42H5 | | |

Table 2 Welding parameters

| Welding method | Wire dimensions, mm | Current, A |
|----------------|--------------------------|---------------------|
| 141 | ∅ 2 | 90 – 100 |
| Voltage, V | Polarity | Heat input Q, kJ/mm |
| 9 – 11 | DC/- | 0,8 – 1,2 |
| Welding method | Electrode dimensions, mm | Current, A |
| 111 | ∅ 3,2 | 100 – 115 |
| Voltage, V | Polarity | Heat input Q, kJ/mm |
| 21 – 23 | DC/+ | 0,3 – 1,0 |

Table 3 Post weld heat treatment of welded joints

| Duration of PWHT, hours | Temperature 1 | Temperature 2 |
|-------------------------|---|---|
| 1 | 730 °C Heating and cooling rate: 100 °C / hour | 760 °C Heating and cooling rate: 100 °C / hour |
| 2 | | |
| 3 | | |
| 4 | | |
| 5 | | |
| 6 | | |

2.1 Tensile Test

Transverse tensile test of welds was done at temperature of 20 °C. The minimal required value of tensile strength can be found in EN 10216-2 [4] - the values must lay in the range from 620 to 850 MPa for steel P92. Graphical expression of average tensile strength - mode of post weld heat treatment dependence can be seen in Fig. 2.

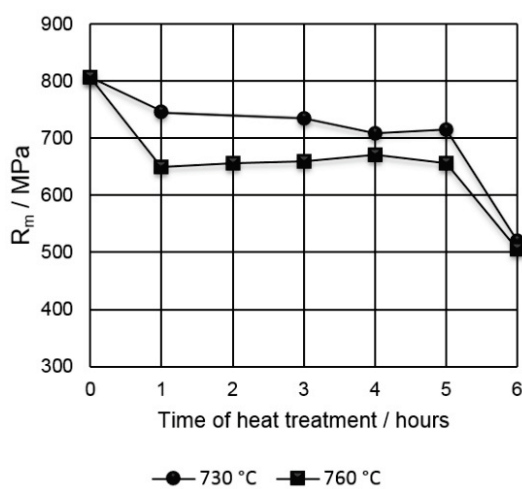


Figure 2 The effect of post weld heat treatment

Fig. 2 shows decreasing trend of tensile strength with increasing dwell on annealing temperature. The maximum value of tensile strength is 807 MPa (without PWHT), the minimum value is 506 MPa (760 °C / 6 hours). The values of tensile strength at heat treatment modes 730 °C / 6 hours and 760 °C / 6 hours are not acceptable according to EN 10216-2 [4].

2.2 Impact Test

On all tested specimens the V-notch was made.

- In a case of VWT 0/2 the V-notch was situated in weld metal, in fusion line, 2 mm under the surface.
- In a case of VHT 2/2 the V-notch was situated in heat-affected zone, 2 mm under the surface, 2 mm far from fusion line.

Impact test was made on specimens with standardized size 10×10 mm according to EN ISO 9016 [5]. The required value of the impact energy according to EN 10216-2 is 27 J [4].

The effect of PWHT on average impact energy is captured in Fig. 3 and Fig. 4.

In Fig. 3 can be seen noticeable increase of impact energy – VHT 2/2 in dwell time of 5 hours (760 °C). The

maximum value in this time of tempering is 81 J. Minimum value of the impact energy (25 J) was reached in 6 hours (730 °C). Without heat treatment the impact energy is not acceptable. The heat treatment modes 730 °C / 1 hour, 760 °C / 1 hour, 730 °C / 2 hours and 730 °C / 6 hours bring not acceptable results according to EN 10216-2 [4].

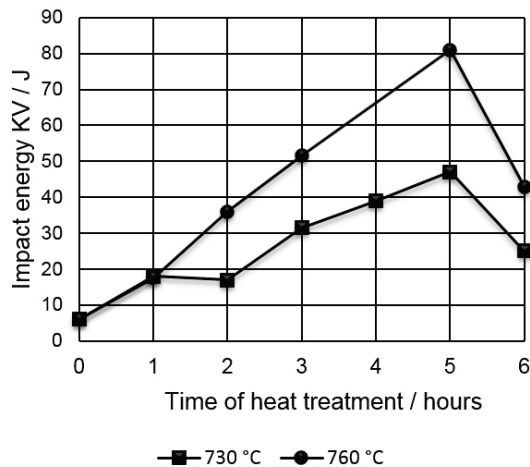


Figure 3 The effect of post weld heat treatment on average values of impact energy – VWT 0/2

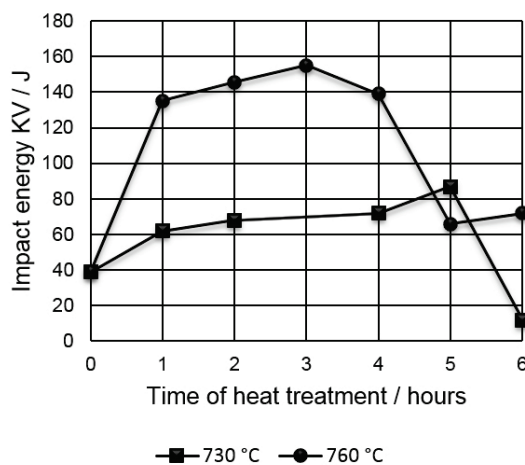


Figure 4 The effect of post weld heat treatment on average values of impact energy - VHT 2/2

In Fig. 4 the values of impact energy were acceptable according to EN 10216-2 [4] – the only exception was heat treatment mode 730 °C / 6 hours where the value was below the required boundary.

2.3 Hardness

Hardness testing was done with Vickers method using the testing load 10 kg (HV10). For the material group 6.4 the maximum value of hardness is 350 HV according to the standard EN ISO 15614-1 [6]. The effect of heat treatment on average values of hardness in weld metal can be seen in Fig. 5.

Hardness of weld metal is decreasing with the time of post weld heat treatment. The hardness without PWHT reaches 400 HV10, which is not acceptable according to EN ISO 15614-1 [6].

The effect of post weld heat treatment on average values of hardness in coarse grained zone can be seen in Fig. 6.

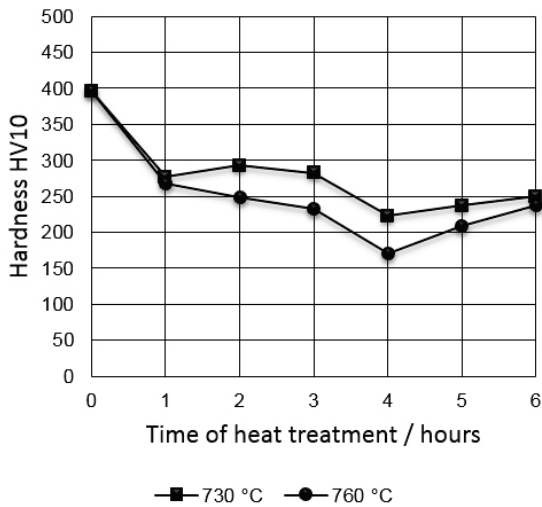


Figure 5 The effect of post weld heat treatment on average values of hardness measured in weld metal

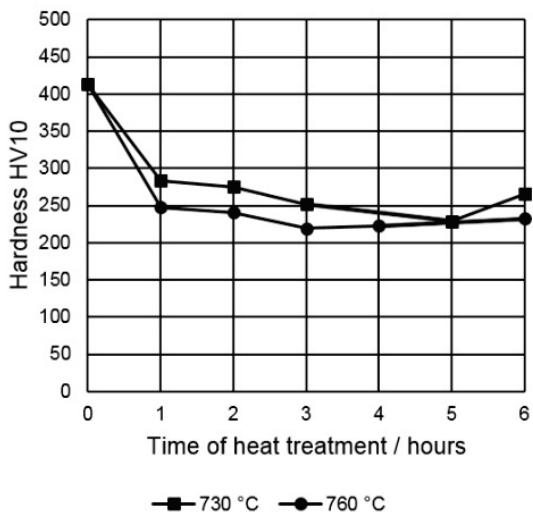


Figure 6 The effect of post weld heat treatment on average values of hardness measured in coarse grained zone of HAZ

From the graphical expression in Fig. 6 for coarse grained zone it is clear that the values of hardness are decreasing with the time of the heat treatment. The hardness without post weld heat treatment reaches 450 HV10, which is not acceptable according to EN ISO 15614-1 [6].

Fig. 6 shows that the welds of P92 steel have to be heat treated and the time of heat treatment does not have too big influence on hardness.

3 CONCLUSIONS

P92 is progressive martensitic 9% Cr steel, which can work in the ultra-supercritical conditions. It has very good mechanical properties and resistance against creep, nevertheless during welding the properties are devalued due to heat input. To improve the mechanical properties the post weld heat treatment is necessary. In order to find out the optimal heat treatment a series of experiments

were made and the testing of tensile strength, impact energy and hardness was carried out.

Experiments showed that tensile strength has decreasing trend with increasing dwell on annealing temperature. All values of tensile strength except the modes of heat treatment 730 °C / 6 hours and 760 °C / 6 hours are in the acceptable range from 620 to 850 MPa.

Impact energy in weld metal shows the increasing trend with the increasing time of heat treatment. Maximum value of impact energy was obtained in heat treatment mode 760 °C / 5 hours. Minimum value of the impact energy was reached in 6 hours at 730 °C. The impact energy of P92 weld metal is not acceptable without post weld heat treatment.

All the values of impact energy in heat affected zone were acceptable according to EN 10216-2 except of post weld heat treatment mode 730 °C / 6 hours, where the impact energy was below the required boundary.

Values of hardness are decreasing with the time of heat treatment. The hardness without post weld heat treatment reaches not acceptable value in weld metal and in heat affected zone as well.

For achieving high strength and sufficient impact toughness can be recommended PWHT at 730 °C for 5 hours. To obtain maximum values of impact toughness while achieving a sufficient strength can be recommended PWHT at 760 °C for 3 hours.

Acknowledgement

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4 REFERENCES

- [1] Heat Resistant Steels, Microstructure Evolution and Life Assessment in Power Plants. Thermal Power Plants Edited by Mohammad Rasul / Zheng-Fei Hu. Croatia : InTech, 2011, 195-226.
- [2] Chen, Q. & Scheffknecht, G. (2002). Boiler design and materials aspects for advanced steam power plants. *Proceedings of COST Programme part II: Materials for Advanced Power Engineering, Vol. 21*, 1019-1034.
- [3] Koukal, J., Sondel, M. & Schwarz, D. (2010). Correlation of Creep Properties of Simulated and Real Weld Joints in Modified 9 %Cr Steels. *Welding in the World, 54*(1), R27-R34. <https://doi.org/10.1007/BF03263481>
- [4] EN 10216-2, (2008). Seamless steel tubes for pressure purposes – Technical delivery conditions – Part 2: Non-alloy and alloy steel tubes with specified elevated temperature properties, CEN.
- [5] EN ISO 9016, (2012). Destructive tests on welds in metallic materials - Impact tests - Test specimen location, notch orientation and examination, CEN.
- [6] EN ISO 15614-1, (2004). Specification and qualification of welding procedures for metallic materials - Welding procedure test - Part 1: Arc and gas welding of steels and arc welding of nickel and nickel alloys, CEN.

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