

An Investigation of the Effect of Toughness and Brittleness Indexes on Ampere Consumption and Wear Rate of a Circular Diamond Saw

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Abstract

The circular diamond saw (CDS) is one of the major sawing machines in dimension stone processing plants. Predicting the performance of a circular diamond saw is very important to estimate the cost and the planning of the stone processing plants. The performance of a CDS depends on some important factors such as machine and tool characteristics, physical and mechanical characteristics of rock and tool wear rate. In this research, it is aimed to investigate the relationship between ampere consumption, brittleness indexes and toughness with the wear rate of a CDS. This aim was pursued by using a fully instrumented cutting rig to cut 14 types of hard rock at constant feed rates, cut depths and peripheral speeds. Wear rate, toughness and brittleness indexes were evaluated using simple and multiple curvilinear regression analysis and predicted models were developed. The results indicated that there is a significant correlation between wear rate, ampere consumption and toughness. It is concluded that, the wear rate of a CDS can be reliably estimated using a multiple curvilinear model which includes ampere consumption and toughness.

Keywords:

Dimensional stone, Circular diamond saw, Brittleness index, Toughness, Statistical analysis.

1. Introduction

The prediction of dimension stone sawability is one of the most important factors in estimating the production cost and planning of the quarries and factories. Dimension stone sawability with a CDS dependent on parameters including; the rock and machine characteristics and saw operating characteristics. The investigation of these parameters in the stone industry is important for establishing the most suitable and economic usage of the sawing method in the future. Many studies have been done on the relations between a circular diamond saw (CDS) and stone characteristics such as in the relevant literature (Tonshoff et al. 2002; Konstanty 2002; Ilio and Togna 2003; Eyuboglo et al. 2003; Ersoy and Atici 2004; Ersoy et al. 2005; Fener et al. 2007; Guney 2011; Brook 2012; Aydin et al. 2013; Aydin et al. 2015, Tumac, 2015; Mikaeil et al. 2016). Up to now, the studies carried out in sawability and sawing characteristics in saw operating characteristics and sawing the design in stone processing (Wei et al. 2003; Kahraman et al. 2004; Gunaydin et al. 2004; Delgado et al. 2005; Kahraman et al. 2005; Buyuksagis 2007; Tutmez et al. 2007; Mikaeil et al. 2011a; Ataei et al. 2012; Mikaeil

et al. 2013; Mikaeil et al. 2015). In the others, the ampere consumption, vibration, the loads acting on the abrasive grits and brittleness indexes in cutting process are investigated (Xu et al. 2002; Xu et al. 2003; Aslantas et al. 2009; Atici and Ersoy 2009; Mikaeil et al. 2011b; Mikaeil et al. 2011c; Mikaeil et al. 2012; Yurdakul and Akdas 2012; Engin et al. 2013; Sengun and Altindag 2013; Karakurt 2014a; Karakurt 2014b; Mikaeil et al. 2014; Aryanfar and Mikaeil 2016).

The main goal of this research is to study the possibility of estimating the wear rate of a circular diamond saw from brittleness indexes and toughness in hard rock cutting process. First of all, the wear rate of a CDS was correlated with brittleness indexes and toughness using simple regression and then, multiple regression analysis was performed.

2. Toughness

Toughness refers to a material's ability to deform plastically and thus absorb the applied energy. To measure this property, a sample of the material must be subjected to a static test to acquire its characteristic stress-strain curve. The work done to fracture the sample can then be obtained by measuring the area under this curve. The volume-specific toughness is known as modulus of

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toughness and refers to the maximum work done (in inch-pounds) to rupture a unit volume (in cubic inch) of the material. For materials like cast iron and concrete, which have a parabolic shaped stress-strain curve, an accurate estimate of modulus of toughness, M_t , is given by **Equation 1**:

$$M_t = \frac{2}{3} \times \sigma_a \times \varepsilon_f \quad (1)$$

Where, σ_a is the ultimate strength and ε_f is the strain at failure (**Deer and Miller 1966**).

Tough materials have high strength and ductility while brittle materials have a generally low toughness due to their inability to absorb energy by undergoing plastic deformation (**Jastrzebski 1959**). The toughness of a material or rock is in fact the ability of its matrix to bind its constituent minerals and grains together but also depends on the strength of individual grains or minerals (**Deer and Miller 1966**). Thus, rocks with a strong matrix consisting of strong minerals are expected to be the toughest (**Shepherd 1951**). From a microscale point of view, it is the type and strength of binding forces between atoms, ions, or molecules that decide the hardness and toughness of a material. From a macroscale perspective, both hardness and toughness are closely correlated with the yield strength (**Jastrzebski 1959**). One of the earliest toughness classification systems was introduced in 1926 by **Harley**. In this system, toughness was expressed as the ft-lbs. of work that must be done to drill one cubic inch of rock, and was related to a grinding resistance that could be determined using a small grinding machine.

3. Brittleness indexes

Another important mechanical property of rocks is brittleness, which has been generally defined as the property of materials that rupture or fracture without any measurable plastic deformation (**Glossary of Geology and Related Sciences 1960**). However, alternative definitions of brittleness have also been introduced by researchers of different backgrounds for different applications (**Yarali and Soyer 2011**). The notable definitions of brittleness are the lack of ductility (**Hetenyi 1966**), the deficiency in internal cohesion leading to an easy fracture (**Ramsey 1967**), and the property of materials such as cast iron and many rocks that fracture at or only slightly beyond the yield stress (**Obert and Duvall 1967**). As mentioned, brittleness can be described as a property of materials that rupture or fracture without undergoing measurable if any plastic deformation. The related literature contains a number of stress-strain curve based definitions for brittleness index (**Baron 1962; Coates and Parsons 1966; Aubertin and Gill 1988; Aubertin et al. 1994; Ribacchi 2000; Hajiabdolmajid and Kaiser 2003**). The present study uses the following

definitions available for this index according to **Equations 2 to 5**.

$$B_1 = \frac{\sigma_c}{\sigma_t} \quad (2)$$

$$B_2 = \frac{\sigma_c - \sigma_t}{\sigma_t + \sigma_c} \quad (3)$$

$$B_3 = \frac{\sigma_c \times \sigma_t}{2} \quad (4)$$

$$B_4 = (\sigma_c \times \sigma_t)^{0.72} \quad (5)$$

Where, B_1 , B_2 , B_3 and B_4 are brittleness, σ_c is the uniaxial compressive strength (MPa), σ_t is the Brazilian tensile strength (Mpa).

4. Methodology of study

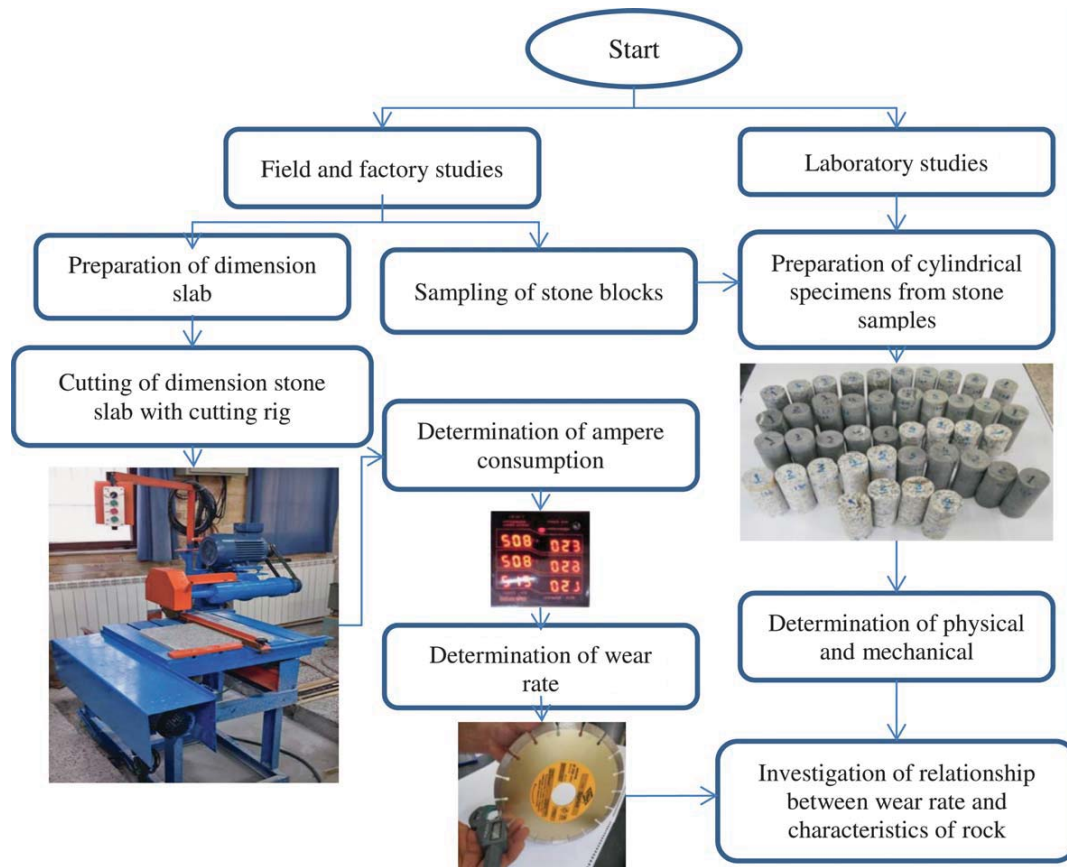
In this study, the relationship of wear rate of a CDS with ampere consumption, brittleness indexes and toughness is investigated. This goal is pursued by using a fully instrumented cutting rig with a maximum spindle motor power of 4 kW and spindle speed of 3000 rpm to cut 14 types of hard rock at constant feed rates, cut depths and peripheral speeds, and measuring the uniaxial compressive strength (UCS), Brazilian tensile strength (BTS), and Young's modulus (YM) as suggested by (**ISRM 1981**). To determine the UCS, the five standard NX core samples (length to diameter ratio of 2.5:1) were taken using a diamond rotating drill from a block sample. The mechanical tests were carried out by a servo controlled testing machine designed for rock test. The standard uniaxial compressive strength test of core samples was carried out under a loading rate of 1 Mpa/s. The tangent Young's modulus at a stress level equal to 50% of the ultimate UCS is used in this study.

The circular diamond saw used in this study was 250 mm in diameter and had a 50 mm thick steel core with a standard narrow radial slot and 18 pieces of 35 mm×2.5 mm×6.0 mm diamond impregnated segments fixed around its periphery, giving a grit size of about 50/60 US mesh at 35 percent concentration. In the course of this study, fourteen rock specimens were cut by the described saw. In the cutting process for each sample, the length of cutting was 120 cm in three steps and the cutting time was 60 seconds at each cutting step.

During the cutting test, ampere consumption was monitored by ampere meter. A digital ampere meter installed on the cutting machine was used to measure ampere consumption. For each sample, the average electrical current consumption was calculated in terms of ampere. The wear rate of the circular diamond saw was determined based on one segment. The measurement was taken for a selected segment, at the beginning and

Table 1. The mechanical test results and the characteristics of studied rocks

Sample Number	Name of granite rock	UCS (MPa)	BTS (MPa)	YM (GPa)	T (MPa)	B1	B2	B3	B4	I (A)	Wr (mm ³)
1	Gray Astan	141	10.15	41.5	31.94	13.89	0.87	715.58	187.11	15.9	8.0E-07
2	Blue Nehbandan	155	13.1	39	41.07	11.83	0.84	1015.25	240.7	15.7	8.0E-07
3	White Natanz	150	11.28	43	34.88	13.3	0.86	846	211.08	16	2.5E-06
4	Red Yazd	142	8.52	44	30.55	16.67	0.89	604.92	165.79	16	1.6E-06
5	Morvarid Mashhad	125	7.4	31	33.6	16.89	0.89	462.5	136.65	15.5	8.0E-07
6	Khoramdareh	133	8.3	29	40.66	16.02	0.88	551.95	155.21	15.4	6.0E-07
7	Ceram Nehbandan	145	9.2	36	38.94	15.76	0.88	667	177.87	15.9	6.0E-07
8	Black Natanz	157	15.46	37	44.41	10.16	0.82	1213.61	273.70	16.5	4.5E-06
9	Astan nehbandan	138	8.15	29	43.78	16.93	0.89	562.35	157.31	15.2	1.1E-06
10	Black Alamot	173	15.98	46	43.38	10.83	0.83	1382.27	300.59	16.1	9.2E-07
11	Black Hamedan	185	17	49	46.56	10.88	0.83	1572.5	329.83	16.5	1.5E-06
12	Jangali Birjand	239	18.86	52	73.23	12.67	0.85	2253.77	427.40	17	6.4E-06
13	Green Yazd	199	16.14	49.5	53.33	12.33	0.85	1605.93	334.86	16.6	2.5E-06
14	Black Chayan	173	15	49	40.72	11.53	0.84	1297.5	287.2	15.8	2.2E-06

**Figure 1:** Flowchart of study

end of each cutting test. Changes of segment height, width and length of the circular diamond saw were measured for determination of the wear rate by a digital micrometer (resolution of 0.001mm). During the sawing trials, the cutting operating parameters such as periph-

eral speed (3000 rpm), feed rate (0.67 cm/s), and depth of cut (0.5 cm) were considered constant. The results of laboratory study are given in **Table 1**.

Wear rate, ampere consumption, toughness and brittleness indexes were evaluated using simple and multi-

ple curvilinear regression analysis and predicted models were developed. The flowchart of this study is illustrated in **Figure 1**.

5. Statistical analysis

5.1. Simple regression

In this statistical analysis, the wear rate of the circular diamond saw, toughness and brittleness indexes were correlated by the least squares regression method. We tested the linear, logarithmic, exponential and power regressions and determined, for each regression, the approximation equation that yields the highest correlation coefficient. The wear rate versus type of brittleness are

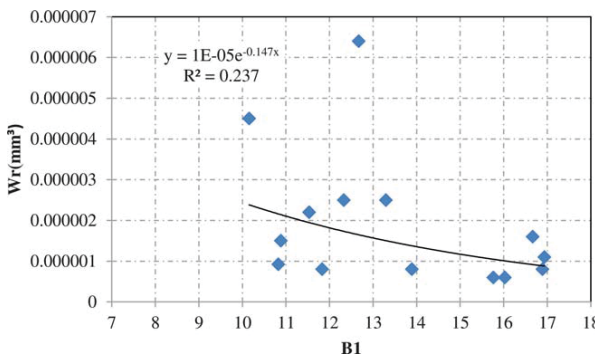


Figure 2: Wear rate versus B1

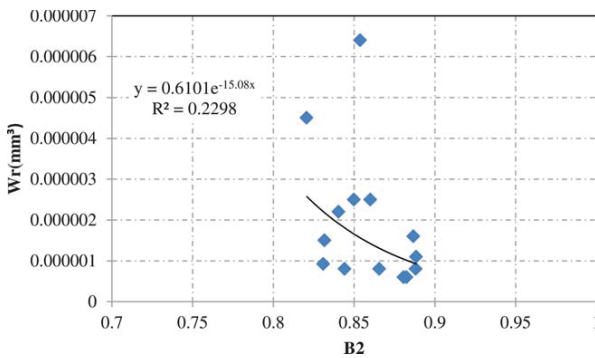


Figure 3: Wear rate versus B2

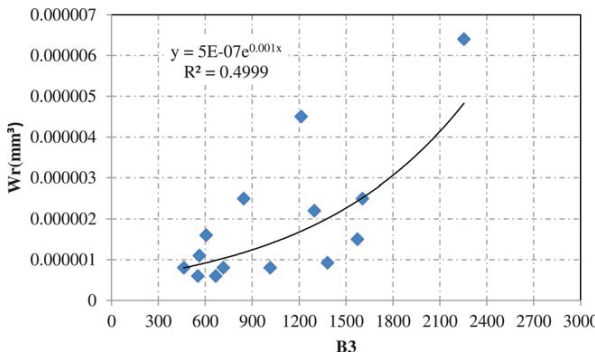


Figure 4: Wear rate versus B3

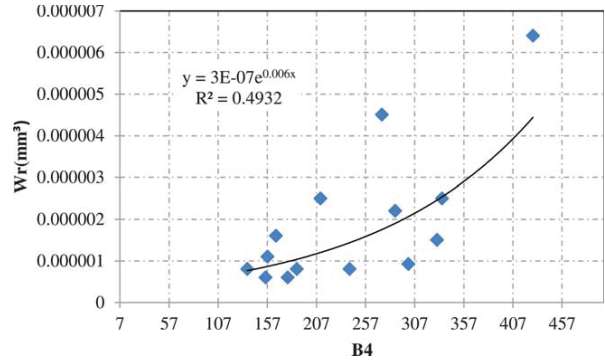


Figure 5: Wear rate versus B4

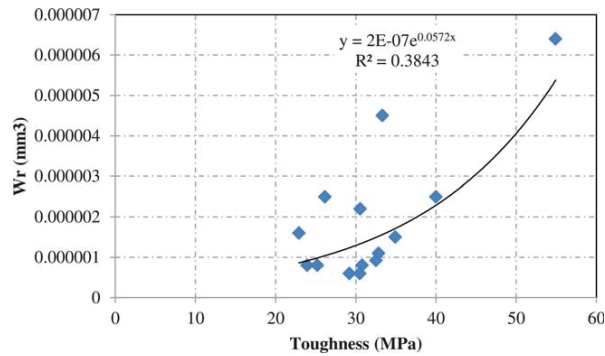


Figure 6: Wear rate versus toughness

shown in **Figures 2 to 5**. **Figure 6** shows the relationship between the wear rate and toughness. **Equations 6 to 9** express the relationship between the wear rate and type of brittleness, and **Equation 10** expresses dependence of wear rate on toughness. These equations are presented by **Equations 6 to 10**:

$$W_r = 10^{-5} \times \text{EXP}(-0.147B_1) \quad (6)$$

$$W_r = 0.6101 \times \text{EXP}(-15.08B_2) \quad (7)$$

$$W_r = 5 \times 10^{-7} \times \text{EXP}(0.001B_3) \quad (8)$$

$$W_r = 3 \times 10^{-7} \times \text{EXP}(0.006B_4) \quad (9)$$

$$W_r = 2 \times 10^{-7} \times \text{EXP}(0.0429T) \quad (10)$$

Where W_r is the wear rate of the diamond saw, mm³, B_1 , B_2 , B_3 and B_4 are brittleness indexes.

5.2. Multiple curvilinear regression analysis

In this section, the wear rate of the diamond saw at different brittleness indexes, toughness and ampere consumption were analysed using multiple curvilinear regression. Regression analysis was performed by the computing software “Statistical Package for the Social Sciences (SPSS)”. The regression models including two independent variables are presented in **Equations 11 to 15**:

$$W_r = \frac{I^{17.35}}{B_1^{0.121} \times 10^{26.59}} \tag{11}$$

$$W_r = \frac{I^{17.25}}{B_2^{1.01} \times 10^{26.68}} \tag{12}$$

$$W_r = \frac{I^{14.17} \times B_3^{0.275}}{10^{23.72}} \tag{13}$$

$$W_r = \frac{I^{14.17} \times B_4^{0.382}}{10^{23.8}} \tag{14}$$

$$W_r = \frac{I^{15.01} \times T^{0.619}}{10^{24.92}} \tag{15}$$

Where I is ampere consumption, A.

Equations 11 to 15 were derived from B1, B2, B3, B4, toughness and I. the wear rate of the circular diamond saw increases with an increase in the ampere consumption. The ampere consumption is easy to detect during the sawing process, so it can be used in the stone processing plants to predict the wear rate in different sawing conditions.

5.3. Validation of models

Validation of the developed models was performed while considering the F test, the t test, correlation coefficient (R²), and the plots of predicted values versus the actual values. The statistical results of the five models are given in Table 2.

The R² of Equations 11 to 15 are 0.56, 0.56, 0.57, 0.57, and 0.58, respectively. These values are fair, however, they show better values in comparison with Equations 6 to 10. The t test was used to determine the sig-

nificance of R². For the use of this test, the tabulated t value (t*) according to the confidence level is compared with the computed t value to accept or reject the null hypothesis. A computed t value that is greater than the tabulated t value disproves the null hypothesis; in this case, R² is important. Otherwise, the null hypothesis is not rejected, and R² is not significant. With a 90% confidence level, the tabulated t value ±1.363 for equations

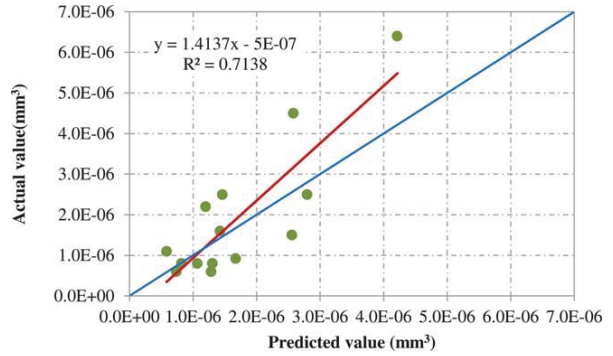


Figure 7: Predicted wear rate versus actual wear rate for Eq. (11)

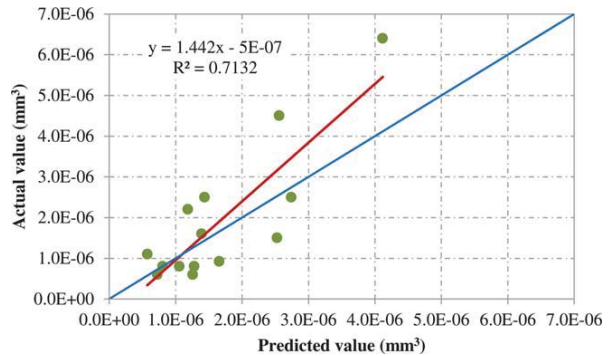


Figure 8: Predicted wear rate versus actual wear rate for Eq. (12)

Table 2. Statistical results of the multiple regression models

Model	Independent variables	Coefficients	Std. Error	t	t*	F	F*	R ²
Eq. (11)	Constant	-26.59	8.11	-3.277	±1.36	6.99	±4.75	0.56
	I	17.35	6.09	2.85				
	B ₁	-0.121	1.05	-0.12				
Eq. (12)	Constant	-26.68	6.96	-3.83	±1.36	6.99	±4.75	0.56
	I	17.25	5.99	2.88				
	B ₂	-1.01	6.8	-0.148				
Eq. (13)	Constant	-23.72	9.154	-2.591	±1.36	7.24	±4.75	0.57
	I	14.17	8.727	1.624				
	B ₃	0.275	0.559	0.492				
Eq. (14)	Constant	-23.8	9.023	-2.638	±1.36	7.24	±4.75	0.57
	I	14.17	8.727	1.624				
	B ₄	0.382	0.773	0.492				
Eq. (15)	Constant	-24.92	6.42	-3.88	±1.36	7.59	±4.75	0.58
	I	15.01	5.96	2.52				
	T	0.619	0.83	0.744				

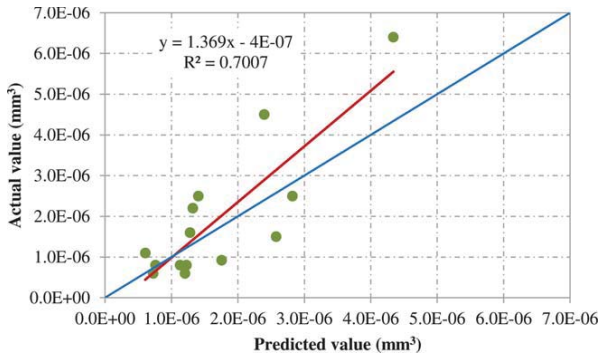


Figure 9: Predicted wear rate versus actual wear rate for Eq. (13)

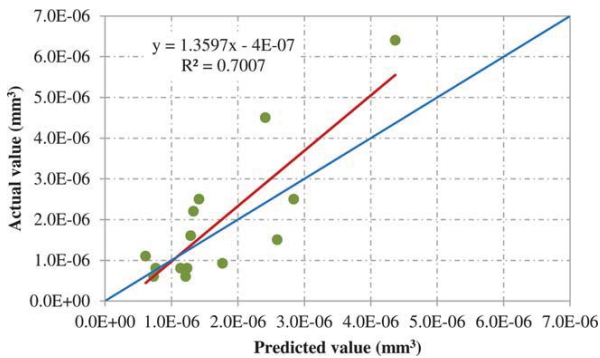


Figure 10: Predicted wear rate versus actual wear rate for Eq. (14)

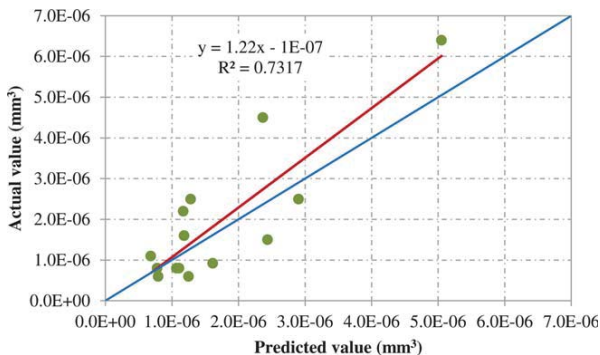


Figure 11: Predicted wear rate versus actual wear rate for Eq. (15)

was found. According to Table 2, the computed t values are greater than the tabulated t value. However, some computed t values for equations are lower than tabulated t values. This means there is some doubt for these models. Among these models, only Eq. 15 is valid with a 75% confidence level. Analysis of variance was done to test the significance of regressions with the F test. In this study, a 95% level of confidence was selected. The computed F values are greater than the tabulated F values (F^*), therefore, the null hypothesis is rejected and the models are valid. The scatter diagrams of the actual and predicted values were used to see the prediction capabil-

ity of the developed models. The scatter diagram of predicted versus actual values for the equations are shown in **Figures 7 to 11**, respectively. As can be seen in these **Figs**, a systematic deviation from the 1:1 diagonal straight line is low for **Equation 15** in comparison with the other equations.

6. Conclusion

The circular diamond saw is one of the most important machines used in stone processing plants. The performance prediction of these saws is important in the cost estimation and the planning of the plants. An accurate estimation of wear rate helps to make the planning of the rock sawing programs more effectual. In this study, the relationship between wear rate of a circular diamond saw, toughness, and brittleness indexes of hard rocks were investigated using simple and multiple curvilinear regression analysis. According to the results of simple regression analysis, B3, B4, and toughness indexes show a better correlation with the wear rate. For practical considerations, ampere consumption was measured during the sawing process. Some models were obtained using multiple curvilinear regression with respect to ampere consumption, toughness, and brittleness indexes. Finally, validation of the developed models were analysed while considering the F test, the t test, correlation coefficient, and the plots of predicted values versus actual values and the best model was selected. The results showed that the wear rate of a CDS can reliably be predicted from ampere consumption and toughness. It is important to emphasize, the developed model can be applied only on granite rocks. More research must be done to check the validity of the obtained model for other types of rocks and the effect of the type of saw.

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