

## Modified Gaussian plume model and K-transport and diffusion model efficiency in the same atmospheric conditions

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The aim of this paper is to compare the modified Gaussian plume model and K-model for continuous emission sources in weakly orographically developed regions. Parametrization of input variables is based on the physical methods using similarity theory.

The results show that, when strong winds and stable atmosphere are present, ground level concentrations take similar values. In contrary, when weak winds and unstable atmosphere are present, K-model overestimates values given by Gaussian model due to exclusion of plume rise in the process of diffusion parametrization.

### Efikasnost modificiranog Gaussovskog i K-modela transporta i difuzije u jednakim atmosferskim uvjetima

U ovom radu uspoređeni su modificirani Gaussovski i K-model transporta i difuzije za kontinuirani izvor emisije u orografski slabo razvijenom području. Parametrizacija ulaznih veličina se zasniva na fizici procesa uz uporabu teorije sličnosti.

Rezultati pokazuju sličnost vrijednosti prizemnih koncentracija pri pojavljivanju jačih vjetrova i stabilne atmosfere. No, pri pojavljivanju slabijih vjetrova i labilnije atmosfere, K-model precjenjuje vrijednosti u usporedbi s Gaussovskim modelom što je uzrokovano neuključivanjem dizanja perjanice prilikom parametrizacije procesa difuzije.

### Introduction

Planetary boundary layer, as a part of atmosphere with very strong friction influence, is very hard to model. In past, several groups of models have been developed, but nowadays three basic groups of models are used:

1) models which use numerical integration of differential equations (K-transport and diffusion models),

2) models which use statistical methods for description of movements of large number of individual particles (Monte Carlo models),

3) models which use analytic solutions of differential equations (Gaussian models).

K-models are based on the law of conservation of mass, and it often needs respectable computer time for numerical integration (Nanni and Tagliazucca, 1982). Their advantage is time dependency, while Gaussian models are stationary. The advantage of Gaussian models is that they require very little computer time because of their analyticity, but the approximations are so rough that they can produce nonrealistic field of ground level concentrations of pollutants. The greatest problem is how to model the diffusion processes, which are very variable in time and space.

In this paper a comparison has been made of the ground level concentrations calculated by K-model (Nanni and Tagliazucca, 1982; Vilibić, 1994) and by the modified Gaussian plume model for continuous sources (Vilibić, 1994). They both assume time independence, although K-model is basically time dependent. Input data consist of five sets of values for different weather conditions – from stable through neutral to unstable. In the work of Vilibić (1994) numerical methods for preparing the stability nomograms (Smith, 1979; Vogt et al., 1971) have been converted for the computer use. Further parametrizations necessary for describing processes in both models in the planetary boundary layer are made using the similarity theory (Panofsky and Dutton, 1984; Smith, 1979).

### Gaussian plume model

Gaussian plume model has got the name from the shape of equation which describes the field of ground level concentrations:

$$c = \frac{Q}{2\pi u \sigma_y \sigma_z} e^{-y^2/2\sigma_y^2} \left[ e^{-(z-h_e)^2/2\sigma_z^2} + e^{-(z+h_e)^2/2\sigma_z^2} \right] \quad (1)$$

where:

- $Q$  – source strength (kg/s)
- $z$  – the height above the ground (m)
- $y$  – the distance from the plume axis (m)
- $h_e$  – effective plume height (m)
- $u$  – wind speed at height  $h_e$  (m/s)
- $\sigma_y, \sigma_z$  – dispersion parameters (dependent upon the distance  $x$  from the source and upon the turbulence intensity) (m)
- $c$  – ground level concentration (kg/m<sup>3</sup>)

This equation is an analytic solution of the K-model differential equation with the following approximations (Šinik, 1981):

- 1) stationary wind field
- 2) homogeneous wind field
- 3) no chemical reactions and no deposition
- 4) no ground absorption
- 5) interval of at least 10 minutes, to avoid instantaneous peaks
- 6) wind speed in  $x$ -axis different from zero, so the diffusion in the  $x$ -axis may be neglected.

For parametrization of the wind speed the exponential law is used (Weil and Brower, 1984), dispersion parameters are described by the Briggs curves (Gifford, 1978) which have been modified using the urban factor (Vilibić, 1994), and the effective height is calculated from other sets of Briggs equations (Briggs, 1978; Weil and Brower, 1984). For all parametrizations the use of similarity theory (Panofsky and Dutton, 1984) and the parametrization of radiation are also necessary (Penzar and Penzar, 1991).

In the paper by Vilibić (1994) the basic equation (1) has been improved by the inclusion of horizontal plume turning in the model. In the case with the mixing layer height  $z_i$  greater than the effective plume height  $h_e$  the developed equation is given as:

$$c = \frac{Q \varepsilon}{\pi u \sigma_y \sigma_z} e^{-y^2/2\sigma_y^2} \left[ e^{-h_e/2\sigma_z^2} + \sum_{i=1}^5 \left( e^{-(2mz_i - h_e)^2/2\sigma_z^2} + e^{-(2mz_i + h_e)^2/2\sigma_z^2} \right) \right], \quad (2)$$

while in the case  $z_i < h_e$  the developed equation is given by:

$$c = \frac{Q \varepsilon}{\pi u \sigma_y \sigma_z} e^{-y^2/2\sigma_y^2} \left[ e^{-h_e/2\sigma_z^2} + \sum_{m=1}^5 e^{-(2mz_i - h_e)^2/2\sigma_z^2} \right] \quad (3)$$

The parametrization of  $z_i$  is given by the nomogram of Pasquill and Smith (1983) which is here transformed into the set of equations (Vilibić, 1994). Factor of condensation  $\varepsilon$  shows the value of horizontal plume turning, and it's defined as a ratio of areas attached to non-curved and curved plume (Vilibić, 1994). Expressions after the signs of sum define the plume reflection from ground and mixing layer (Šinik, 1981).

Special case of spreading of the Gaussian plume occurs when the mixing layer goes over the effective height (where the maximum concentrations are present). This process is called fumigation which usually occurs in the morning after the night with strong stable conditions (Šinik, 1981). In that case equations given in Vilibić (1994) are used.

### K-transport model

K-model is based on the law of mass conservation:

$$\frac{\partial c}{\partial t} + \nabla \nabla c = \frac{\partial}{\partial x_i} K_{ij} \frac{\partial c}{\partial x_j} + S + D; \quad \forall i, j = 1, 2, 3 \quad (4)$$

where:

$V$  – wind speed

$K_{ij}$  – components of tensor of diffusion

$S$  – source strength, and

$D$  – deposition rate.

If we assume that there is no vertical wind component ( $w = 0$ ), deposition ( $D = 0$ ) and non-diagonal terms of diffusion tensor ( $K_{ij} = 0, i \neq j$ ), equation (4) may be transformed into:

$$\frac{\partial c}{\partial t} = -u \frac{\partial c}{\partial x} - v \frac{\partial c}{\partial y} + \frac{\partial}{\partial x} K_x \frac{\partial c}{\partial x} + \frac{\partial}{\partial y} K_y \frac{\partial c}{\partial y} + \frac{\partial}{\partial z} K_z \frac{\partial c}{\partial z} + S \quad (5)$$

This equation can be separated into a set of equations (Nanni and Tagliazucca, 1982) that are numerically integrated by improved methods of Runca and Sardei (1975). In this paper the numerical integration has been performed in space with dimensions  $10 \text{ km} \times 10 \text{ km} \times z_i$ . The horizontal grid spacing is 500 metres, while the vertical one is  $h_s/4$ , where  $h_s$  is source height (Vilibić, 1994). Vertical changes of the wind speed at grid points are calculated using the exponential law (Weil and Brower, 1984) for  $u$  and  $v$  wind components. Parametrization of diffusion tensor is based on the relations given by Shier and Shieh (1974) for vertical diffusion, and by Nanni and Tagliazucca (1982) for horizontal diffusion. Source strength  $S$  is modelled such that in the source point concentration is  $Q$  and in all other points plume is transported by diffusion and transport processes.

### Results

Both models (K- and modified Gaussian) have been applied to the same atmospheric conditions and compared using five sets of input data for various stability conditions in the planetary boundary layer (Table 1) in orographically weakly developed region. Technological parameters of the source (volume flux and temperature of smoke at stack exit, stack height, source strength) have been estimated using the data from some stacks in the Republic of Croatia *e.g.* Plomin 1 and 2, Rijeka and Zagreb.

Tables 2 to 6 illustrate numerically all the cases (A, B, C, D and E). Horizontal grid spacing is 500 metres. Numbers in the tables represent rela-

Table 1. Input data for cases A, B, C, D and E

| CASE   | A   | B   | C    | D   | E   |
|--|-----|-----|------|-----|-----|
| Month  | 3   | 1   | 6    | 6   | 1   |
| Hour   | 10  | 13  | 13   | 13  | 6   |
| Cloudiness (in 1/8)                                    | 0   | 0   | 0    | 2   | 8   |
| Wind at station 1 ( $\text{ms}^{-1}$ )                 | 2   | 1   | 1    | 4   | 3   |
| Wind at station 2 ( $\text{ms}^{-1}$ )                 | 2   | 1   | 1    | 4   | 3   |
| Atmospheric temperature at stack height (K)            | 280 | 290 | 300  | 300 | 270 |
| Declination of Earth ( $^{\circ}$ )                    | 0   | -15 | 20   | 20  | -15 |
| Roughness (m)  |     |     | 0.5  |     |     |
| Distance from source to station 1 (m)                  |     |     | 3000 |     |     |
| Distance from source to station 2 (m)                  |     |     | 8000 |     |     |
| Urbanization factor                                    |     |     | 0.5  |     |     |
| Angle between winds at stations 1 and 2 ( $^{\circ}$ ) |     |     | 45   |     |     |
| Source height (m)                                      |     |     | 150  |     |     |
| Gas temperature at stack height (K)                    |     |     | 470  |     |     |
| Volume flux ( $\text{m}^3\text{s}^{-1}$ )              |     |     | 200  |     |     |
| Source strength ( $\text{kgs}^{-1}$ )                  |     |     | 1    |     |     |

tive concentrations from 0 to 10000. Exact concentration can be calculated if every number is divided by 10000 and multiplied by the C(CG) or C(CK) which represent Gaussian and K-model maximal concentrations, respectively.

Figures 1 to 5 show graphically the distribution of ground level concentrations for all cases. Figures (a) represent three dimensional view of concentration fields, while Figures (b) and (c) represent the Gaussian and K-model concentrations, respectively. The concentrations are proportional to the area of the circles (the smallest edge points of the plume represent 0.1 % of the maximal concentration). Better understanding of graphical presentation will be achieved by consulting the table presentation.

Case A represents morning situation when fumigation occurs (Fig. 1, Table 2). Analysis of the results lead us to the conclusion that the Gaussian plume model gives very high concentrations close to the source, while farther concentrations decrease rapidly. This is in agreement with the fumigation theory (Šinik, 1981). Meanwhile K-model gives ten times smaller concentrations because here it has been applied as time independent model which is not temporally related to the previous situations and does not include a fumigation process.

Case B describes unstable situation in winter with weak winds (Fig. 2, Table 3). Maximal concentration is 2.5 smaller in K- than in the Gaussian model and its distance from the source is greater (in K-model about 2500 m, in Gaussian about 500 m); so both models give similar concentrations at distances larger than 2000 m from the source. Closer than 2000 m the K-model gives lower values. Yet it should be mentioned that the plume is more

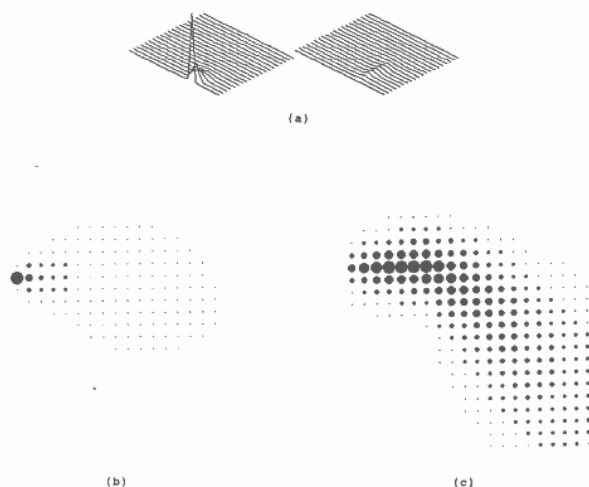


Figure 1. Ground level concentrations for case A. (a) 3D view (Gaussian left, K-model right); (b) 2D view (Gaussian model); (c) 2D view (K-model)

Table 2. Numerical presentation of ground level concentrations for case A

MODIFIED GAUSSIAN MODEL :

|     |      |      |     |     |     |     |     |     |    |    |    |    |    |    |    |    |    |    |    |
|-----|------|------|-----|-----|-----|-----|-----|-----|----|----|----|----|----|----|----|----|----|----|----|
| 0   | 0    | 0    | 0   | 0   | 1   | 1   | 2   | 4   | 5  | 6  | 6  | 6  | 5  | 5  | 5  | 4  | 3  | 3  | 2  |
| 0   | 0    | 0    | 0   | 1   | 4   | 6   | 9   | 13  | 12 | 12 | 12 | 11 | 10 | 9  | 8  | 7  | 6  | 5  | 4  |
| 0   | 0    | 0    | 1   | 6   | 16  | 19  | 25  | 24  | 24 | 22 | 21 | 19 | 16 | 14 | 12 | 10 | 9  | 7  | 6  |
| 0   | 0    | 0    | 10  | 29  | 45  | 45  | 46  | 44  | 40 | 36 | 32 | 28 | 24 | 20 | 17 | 15 | 12 | 10 | 9  |
| 0   | 0    | 10   | 42  | 91  | 99  | 87  | 79  | 76  | 60 | 52 | 44 | 38 | 32 | 27 | 23 | 19 | 16 | 14 | 11 |
| 0   | 41   | 100  | 224 | 281 | 274 | 238 | 185 | 95  | 39 | 46 | 55 | 47 | 39 | 33 | 28 | 24 | 18 | 17 | 14 |
| 167 | 859  | 205  | 484 | 339 | 247 | 184 | 114 | 515 | 93 | 77 | 64 | 54 | 45 | 38 | 32 | 28 | 23 | 20 | 17 |
| MAX | 2500 | 3111 | 621 | 440 | 277 | 204 | 156 | 122 | 99 | 82 | 68 | 58 | 49 | 41 | 36 | 32 | 28 | 22 | 18 |
| 167 | 859  | 205  | 484 | 339 | 247 | 180 | 117 | 118 | 96 | 80 | 68 | 58 | 50 | 43 | 37 | 32 | 28 | 24 | 22 |
| 0   | 41   | 100  | 224 | 287 | 276 | 152 | 124 | 102 | 86 | 76 | 63 | 55 | 49 | 42 | 37 | 33 | 28 | 25 | 23 |
| 0   | 0    | 10   | 42  | 91  | 89  | 105 | 95  | 83  | 73 | 64 | 57 | 51 | 45 | 40 | 36 | 32 | 28 | 26 | 23 |
| 0   | 0    | 0    | 10  | 29  | 45  | 64  | 64  | 63  | 59 | 54 | 49 | 45 | 41 | 38 | 34 | 31 | 28 | 25 | 23 |
| 0   | 0    | 0    | 1   | 6   | 16  | 35  | 44  | 47  | 46 | 44 | 42 | 40 | 37 | 34 | 31 | 29 | 27 | 24 | 22 |
| 0   | 0    | 0    | 1   | 4   | 10  | 29  | 34  | 36  | 36 | 35 | 34 | 33 | 30 | 29 | 27 | 25 | 23 | 21 |    |
| 0   | 0    | 0    | 0   | 1   | 9   | 19  | 25  | 28  | 29 | 29 | 29 | 27 | 27 | 26 | 25 | 23 | 22 | 20 |    |
| 0   | 0    | 0    | 0   | 0   | 4   | 13  | 19  | 22  | 24 | 25 | 24 | 24 | 24 | 23 | 23 | 22 | 20 | 18 |    |
| 0   | 0    | 0    | 0   | 0   | 3   | 10  | 15  | 18  | 19 | 19 | 20 | 21 | 21 | 21 | 21 | 20 | 19 | 18 |    |
| 0   | 0    | 0    | 0   | 0   | 0   | 3   | 4   | 12  | 15 | 15 | 17 | 18 | 18 | 19 | 19 | 19 | 18 | 17 | 17 |
| 0   | 0    | 0    | 0   | 0   | 0   | 3   | 7   | 10  | 11 | 13 | 14 | 15 | 16 | 17 | 17 | 17 | 16 | 15 |    |
| 0   | 0    | 0    | 0   | 0   | 0   | 3   | 6   | 7   | 9  | 11 | 12 | 13 | 14 | 15 | 15 | 15 | 15 | 14 |    |
| 0   | 0    | 0    | 0   | 0   | 0   | 4   | 5   | 6   | 8  | 9  | 11 | 12 | 12 | 13 | 13 | 14 | 14 | 14 | 13 |
| 0   | 0    | 0    | 0   | 0   | 0   | 3   | 4   | 5   | 7  | 8  | 9  | 10 | 11 | 12 | 12 | 12 | 12 | 12 | 12 |
| 0   | 0    | 0    | 0   | 0   | 0   | 2   | 3   | 5   | 6  | 7  | 8  | 9  | 10 | 10 | 11 | 11 | 11 | 11 | 11 |
| 0   | 0    | 0    | 0   | 0   | 0   | 2   | 3   | 4   | 5  | 6  | 7  | 8  | 9  | 9  | 10 | 10 | 10 | 10 | 10 |

K-MODEL :

|      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |     |     |     |     |     |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|-----|-----|-----|-----|-----|
| 0    | 0    | 0    | 0    | 0    | 1    | 1    | 1    | 1    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0   | 0   | 0   | 0   |     |
| 0    | 0    | 0    | 1    | 2    | 2    | 1    | 2    | 1    | 1    | 0    | 0    | 0    | 0    | 0    | 0    | 0   | 0   | 0   | 0   |     |
| 0    | 5    | 4    | 7    | 11   | 15   | 18   | 12   | 4    | 5    | 3    | 1    | 0    | 0    | 0    | 0    | 0   | 0   | 0   | 0   |     |
| 4    | 13   | 25   | 45   | 59   | 76   | 94   | 64   | 44   | 27   | 16   | 8    | 4    | 1    | 0    | 0    | 0   | 0   | 0   | 0   |     |
| 25   | 74   | 140  | 212  | 294  | 371  | 451  | 299  | 246  | 130  | 76   | 41   | 20   | 9    | 4    | 1    | 1   | 0   | 0   | 0   |     |
| 147  | 396  | 696  | 1064 | 1262 | 1222 | 1672 | 1184 | 523  | 316  | 204  | 140  | 86   | 43   | 18   | 8    | 5   | 2   | 1   | 0   |     |
| 781  | 1824 | 2936 | 3870 | 4584 | 4937 | 5606 | 3648 | 2423 | 1400 | 965  | 543  | 284  | 142  | 66   | 30   | 10  | 4   | 3   | 0   |     |
| 3181 | 6231 | 8402 | 8631 | 6482 | 3955 | 2081 | 7161 | 5147 | 3460 | 2187 | 1288 | 722  | 376  | 184  | 89   | 52  | 31  | 19  | 10  |     |
| 925  | 2089 | 3201 | 4051 | 4628 | 4895 | 5281 | 3962 | 2431 | 1388 | 8195 | 5226 | 3304 | 1746 | 984  | 581  | 324 | 176 | 47  | 27  |     |
| 193  | 483  | 818  | 1133 | 1408 | 1637 | 1954 | 2462 | 4180 | 4213 | 3516 | 2672 | 1839 | 1180 | 689  | 372  | 241 | 155 | 100 | 40  |     |
| 76   | 18   | 177  | 241  | 358  | 428  | 459  | 3756 | 2915 | 2242 | 2239 | 2412 | 2137 | 1556 | 961  | 564  | 389 | 267 | 179 | 111 |     |
| 4    | 10   | 35   | 55   | 77   | 100  | 126  | 163  | 1606 | 2284 | 2645 | 2614 | 2266 | 1744 | 1215 | 799  | 569 | 400 | 276 | 176 |     |
| 1    | 3    | 6    | 10   | 15   | 21   | 31   | 55   | 286  | 894  | 1492 | 1983 | 2315 | 2338 | 1817 | 1382 | 978 | 728 | 522 | 379 | 240 |
| 0    | 0    | 1    | 2    | 3    | 4    | 17   | 174  | 478  | 926  | 1330 | 1750 | 1872 | 1745 | 1414 | 1039 | 653 | 443 | 477 | 321 |     |
| 0    | 0    | 0    | 0    | 0    | 6    | 79   | 254  | 554  | 942  | 1309 | 1550 | 1569 | 1485 | 1146 | 754  | 473 | 347 | 301 |     |     |
| 0    | 0    | 0    | 0    | 0    | 2    | 35   | 125  | 232  | 422  | 622  | 843  | 1214 | 1333 | 1283 | 1129 | 845 | 590 | 500 | 424 |     |
| 0    | 0    | 0    | 0    | 0    | 1    | 16   | 65   | 183  | 386  | 653  | 911  | 1086 | 1133 | 1049 | 912  | 757 | 605 | 445 |     |     |
| 0    | 0    | 0    | 0    | 0    | 0    | 7    | 33   | 102  | 238  | 446  | 667  | 858  | 953  | 936  | 840  | 719 | 591 | 447 |     |     |
| 0    | 0    | 0    | 0    | 0    | 0    | 3    | 14   | 36   | 144  | 291  | 478  | 654  | 778  | 807  | 744  | 653 | 552 | 429 |     |     |
| 0    | 0    | 0    | 0    | 0    | 0    | 1    | 4    | 31   | 64   | 109  | 132  | 185  | 416  | 674  | 639  | 573 | 495 | 386 |     |     |
| 0    | 0    | 0    | 0    | 0    | 0    | 0    | 4    | 16   | 55   | 120  | 225  | 355  | 491  | 540  | 535  | 486 | 420 | 355 |     |     |
| 0    | 0    | 0    | 0    | 0    | 0    | 0    | 2    | 9    | 29   | 73   | 144  | 248  | 346  | 429  | 433  | 404 | 364 | 309 |     |     |
| 0    | 0    | 0    | 0    | 0    | 0    | 0    | 4    | 15   | 42   | 92   | 162  | 243  | 311  | 374  | 311  | 280 | 250 |     |     |     |

MAX(CG) = 3.362E-06  
MAX(CK) = 1.417E-07

narrow in the K-model, especially when weak winds and unstable atmosphere are present. This is due to additional modelling of horizontal diffusion and plume rise in the Gaussian model (Briggs, 1978; Weil, 1979) and the influence of edge walls in the K-model.

Case C represents a very unstable situation in summer with strong convection and weak winds (Fig. 3, Table 4). Ground level concentration field calculated by K-model gives thousand times larger values than the Gaussian model. The reason for this disagreement lies in the modelling of vertical diffusion processes without inclusion of plume rise in K-model. This produces much smaller effective height of the source in K-model, as strong convective eddies bring more plume gases to the ground.



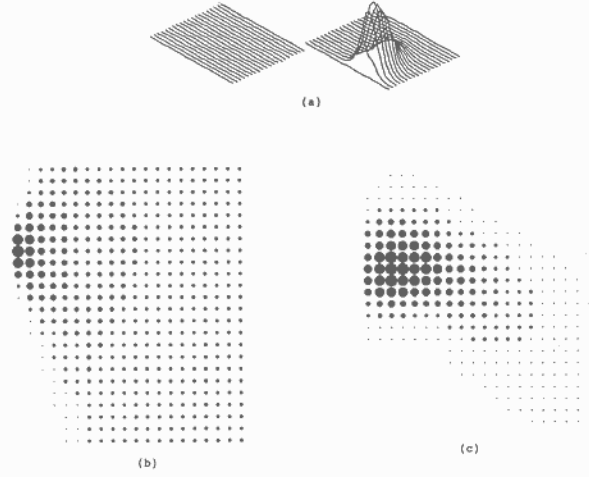


Figure 3. Ground level concentrations for case C. (a) 3D view (Gaussian left, K-model right); (b) 2D view (Gaussian model); (c) 2D view (K-model)

Table 4. Numerical presentation of ground level concentrations for case C

MODIFIED GAUSSIAN MODEL :

|      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|------|
| 0    | 01   | 425  | 154  | 462  | 885  | 710  | 696  | 675  | 659  | 623  | 596  | 569  | 543  | 519  | 496  | 473  | 453  | 433  | 414  |
| 0    | 257  | 818  | 1002 | 1041 | 1010 | 811  | 770  | 742  | 705  | 669  | 634  | 601  | 572  | 543  | 517  | 493  | 469  | 449  | 430  |
| 3    | 686  | 1231 | 1259 | 1222 | 1129 | 909  | 855  | 803  | 754  | 709  | 667  | 629  | 595  | 564  | 534  | 504  | 484  | 461  | 440  |
| 50   | 1527 | 1924 | 1954 | 1933 | 1727 | 1400 | 1346 | 1297 | 1251 | 1207 | 1165 | 1125 | 1087 | 1051 | 1017 | 984  | 953  | 924  | 896  |
| 511  | 2347 | 2116 | 1801 | 1545 | 1227 | 886  | 965  | 983  | 1008 | 1037 | 1064 | 1086 | 1104 | 1116 | 1121 | 1121 | 1116 | 1104 | 1086 |
| 2647 | 4413 | 2922 | 2002 | 1459 | 1036 | 652  | 834  | 852  | 783  | 725  | 675  | 631  | 594  | 564  | 534  | 504  | 484  | 461  | 440  |
| 7184 | 5804 | 3320 | 2240 | 1720 | 1230 | 800  | 1067 | 955  | 845  | 797  | 770  | 739  | 713  | 683  | 653  | 623  | 593  | 563  | 533  |
| MAKS | 1312 | 1467 | 1291 | 1159 | 1054 | 1216 | 1089 | 965  | 848  | 793  | 726  | 676  | 630  | 591  | 558  | 527  | 500  | 475  | 455  |
| 7184 | 5804 | 3320 | 2240 | 1720 | 1230 | 800  | 1067 | 955  | 845  | 797  | 770  | 739  | 713  | 683  | 653  | 623  | 593  | 563  | 533  |
| 2647 | 4413 | 2922 | 2002 | 1459 | 1036 | 652  | 834  | 852  | 783  | 725  | 675  | 631  | 594  | 564  | 534  | 504  | 484  | 461  | 440  |
| 511  | 2347 | 2116 | 1801 | 1545 | 1227 | 886  | 965  | 983  | 1008 | 1037 | 1064 | 1086 | 1104 | 1116 | 1121 | 1121 | 1116 | 1104 | 1086 |
| 50   | 1527 | 1924 | 1954 | 1933 | 1727 | 1400 | 1346 | 1297 | 1251 | 1207 | 1165 | 1125 | 1087 | 1051 | 1017 | 984  | 953  | 924  | 896  |
| 2    | 646  | 1271 | 1289 | 1222 | 1129 | 911  | 877  | 846  | 791  | 681  | 633  | 598  | 570  | 541  | 513  | 484  | 455  | 430  | 412  |
| 0    | 237  | 818  | 1002 | 1041 | 1010 | 1091 | 923  | 799  | 711  | 645  | 598  | 559  | 521  | 483  | 444  | 405  | 375  | 352  | 332  |
| 0    | 81   | 425  | 754  | 826  | 882  | 1022 | 868  | 745  | 665  | 601  | 568  | 533  | 497  | 470  | 454  | 434  | 422  | 404  | 394  |
| 0    | 21   | 246  | 536  | 583  | 761  | 917  | 102  | 638  | 628  | 572  | 536  | 481  | 466  | 451  | 436  | 422  | 408  | 394  | 381  |
| 0    | 4    | 124  | 345  | 541  | 640  | 867  | 719  | 629  | 575  | 532  | 472  | 459  | 446  | 433  | 419  | 406  | 393  | 380  | 368  |
| 0    | 0    | 62   | 237  | 410  | 528  | 781  | 641  | 576  | 539  | 482  | 451  | 439  | 427  | 415  | 403  | 391  | 379  | 367  | 356  |
| 0    | 0    | 27   | 147  | 302  | 427  | 681  | 579  | 559  | 495  | 441  | 411  | 406  | 410  | 399  | 388  | 377  | 366  | 355  | 344  |
| 0    | 0    | 10   | 67   | 176  | 259  | 585  | 525  | 455  | 429  | 421  | 402  | 403  | 393  | 383  | 373  | 363  | 353  | 343  | 332  |
| 0    | 0    | 4    | 49   | 150  | 243  | 515  | 420  | 415  | 410  | 403  | 395  | 387  | 379  | 369  | 359  | 350  | 340  | 331  | 321  |
| 0    | 0    | 1    | 28   | 101  | 209  | 403  | 401  | 397  | 392  | 386  | 379  | 371  | 363  | 355  | 346  | 337  | 328  | 319  | 311  |
| 0    | 0    | 0    | 13   | 66   | 149  | 285  | 388  | 395  | 370  | 363  | 357  | 349  | 341  | 333  | 325  | 317  | 309  | 300  | 290  |
| 0    | 0    | 0    | 6    | 42   | 109  | 204  | 267  | 364  | 360  | 355  | 345  | 343  | 336  | 329  | 321  | 314  | 306  | 298  | 289  |

K-MODEL :

|      |      |      |      |      |      |      |      |      |      |      |     |     |     |     |     |     |      |      |      |
|------|------|------|------|------|------|------|------|------|------|------|-----|-----|-----|-----|-----|-----|------|------|------|
| 6    | 24   | 40   | 44   | 35   | 29   | 20   | 10   | 4    | 3    | 1    | 0   | 0   | 0   | 0   | 0   | 0   | 0    | 0    | 0    |
| 11   | 45   | 73   | 74   | 64   | 52   | 37   | 19   | 11   | 4    | 3    | 1   | 0   | 0   | 0   | 0   | 0   | 0    | 0    | 0    |
| 49   | 164  | 238  | 226  | 197  | 152  | 108  | 54   | 31   | 17   | 9    | 4   | 2   | 1   | 0   | 0   | 0   | 0    | 0    | 0    |
| 188  | 538  | 696  | 668  | 561  | 468  | 385  | 162  | 93   | 52   | 28   | 15  | 7   | 3   | 1   | 0   | 0   | 0    | 0    | 0    |
| 592  | 1520 | 1818 | 1671 | 1438 | 1126 | 770  | 451  | 274  | 168  | 90   | 49  | 24  | 11  | 5   | 2   | 1   | 0    | 0    | 0    |
| 1658 | 3225 | 2782 | 2312 | 1875 | 1500 | 1020 | 481  | 281  | 171  | 87   | 47  | 23  | 11  | 5   | 2   | 1   | 0    | 0    | 0    |
| 2383 | 3886 | 4627 | 4104 | 3528 | 2826 | 2184 | 1380 | 864  | 511  | 287  | 149 | 75  | 36  | 19  | 12  | 7   | 4    | 2    | 1    |
| 2645 | 3526 | 4159 | 3739 | 3141 | 2421 | 1810 | 1158 | 708  | 423  | 251  | 151 | 81  | 46  | 24  | 12  | 7   | 4    | 2    | 1    |
| 4498 | 6695 | MAKS | 9426 | 8384 | 7245 | 5222 | 3628 | 2548 | 1785 | 1012 | 589 | 379 | 223 | 159 | 100 | 68  | 45   | 29   | 15   |
| 4188 | 6213 | 9227 | 8122 | 7081 | 5061 | 3447 | 2389 | 1626 | 1041 | 633  | 388 | 240 | 153 | 106 | 71  | 47  | 31   | 19   | 10   |
| 2518 | 3719 | 5647 | 5216 | 4615 | 3887 | 3116 | 2043 | 1318 | 838  | 508  | 302 | 182 | 110 | 72  | 46  | 29  | 16   | 10   | 5    |
| 1162 | 2122 | 2984 | 2815 | 2127 | 1625 | 1018 | 657  | 454  | 274  | 161  | 91  | 48  | 25  | 14  | 9   | 5   | 3    | 2    | 1    |
| 449  | 141  | 512  | 843  | 722  | 561  | 407  | 248  | 148  | 898  | 512  | 300 | 172 | 96  | 54  | 33  | 20  | 12   | 7    | 4    |
| 160  | 161  | 374  | 254  | 220  | 178  | 127  | 77   | 484  | 555  | 571  | 525 | 451 | 371 | 304 | 248 | 201 | 161  | 127  | 90   |
| 54   | 79   | 41   | 75   | 66   | 62   | 75   | 161  | 219  | 222  | 263  | 296 | 339 | 390 | 457 | 539 | 644 | 781  | 952  | 1123 |
| 17   | 23   | 22   | 22   | 19   | 18   | 25   | 71   | 124  | 182  | 224  | 274 | 345 | 431 | 544 | 684 | 864 | 1104 | 1414 | 1814 |
| 5    | 7    | 6    | 6    | 5    | 5    | 8    | 33   | 64   | 106  | 152  | 196 | 246 | 304 | 374 | 454 | 554 | 674  | 814  | 974  |
| 1    | 2    | 1    | 1    | 1    | 1    | 1    | 3    | 15   | 31   | 53   | 76  | 96  | 111 | 123 | 137 | 153 | 171  | 191  | 211  |
| 0    | 0    | 0    | 0    | 0    | 0    | 1    | 6    | 15   | 29   | 44   | 69  | 74  | 86  | 93  | 92  | 81  | 77   | 69   | 56   |
| 0    | 0    | 0    | 0    | 0    | 0    | 2    | 8    | 15   | 25   | 37   | 50  | 61  | 68  | 70  | 66  | 61  | 56   | 56   | 46   |
| 0    | 0    | 0    | 0    | 0    | 0    | 1    | 4    | 8    | 11   | 24   | 34  | 43  | 50  | 51  | 51  | 44  | 45   | 45   | 37   |
| 0    | 0    | 0    | 0    | 0    | 0    | 0    | 2    | 5    | 9    | 15   | 22  | 26  | 34  | 39  | 39  | 33  | 33   | 35   | 28   |
| 0    | 0    | 0    | 0    | 0    | 0    | 0    | 0    | 2    | 3    | 9    | 14  | 20  | 25  | 24  | 21  | 21  | 25   | 25   | 21   |

MAKS(CS)= 7.724E-07  
MAKS(CI)= 1.521E-01

Conclusion

Processing different cases of planetary boundary layer stability, it can be noticed that the Gaussian plume model gives lower concentrations than K-model when weak winds and unstable atmosphere are present. This occurs because the plume rise is not included in the K-model, so theoretically the plume reaches the ground faster and produces larger concentrations. In the Gaussian model this problem has been smoothed with additional modelling of plume rise. Also, because of comparison with the Gaussian model, K-model is here time independent, so it couldn't describe the fumigation process (forced time independence). K-model is, basically, a prediction model and, when this characteristic is taken into account, it gives better description of the time variations of







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