

Physico-Mechanical Properties of Thermally Modified *Eucalyptus Nitens* Wood for Decking Applications

Fizička i mehanička svojstva toplinski modificiranog drva *Eucalyptus nitens* za vanjske podne obloge

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ABSTRACT • *Eucalyptus nitens* is a fast growing plantation species that has a good acclimation in Spain and Chile. At the moment it is mainly used for pulp and paper production, but there is a growing market for solid wood products made from this species. Thermal modification offers a good alternative to produce high quality material to manufacture products with high added value. This study used unmodified and thermally modified *E. nitens* wood from Spanish and Chilean plantations to elaborate external decking and examine if it complies with the necessary properties to be a competitive product. A process similar to ThermoWood® was applied at the following temperatures: 185 °C, 200 °C and 215 °C. For each modification and for an unmodified specimen mass loss, volumetric swelling, anti-swelling efficiency (ASE) and equilibrium moisture content (EMC) were determined. Brinell hardness, dynamic hardness, screw and nail withdrawal resistance, and abrasion resistance according to the Shaker method and the Taber Abraser method were also determined. According to this study, thermally modified *E. nitens* from both countries showed high potential to be used as decking material, particularly when modified at 200 °C.

Keywords: *Eucalypt*, anti-swelling efficiency (ASE), hardness, abrasion resistance, timber

SAŽETAK • *Eukaliptus nitens* brzo je rastuća plantažna vrsta koja se dobro prilagodila klimi u Španjolskoj i Čileu. Trenutačno se uglavnom iskorištava za proizvodnju celuloze i papira, ali sve je veće tržište proizvoda izrađenih od masivnog drva te vrste. Toplinskom modifikacijom dobiva se dobra alternativa za proizvodnju visokokvalitetnih proizvoda s visokom dodanom vrijednošću. U ovom je istraživanju kao materijal za vanjske podne obloge upotrijebljeno nemodificirano i toplinski modificirano drvo *E. nitens* sa španjolskih i čileanskih plantaža te je ispitana njegova sukladnost sa svojstvima potrebnima za postizanje konkurentnosti. Primijenjen je postupak sličan procesu ThermoWood®, i to pri temperaturama 185, 200 i 215 °C. Za svaki modificirani i nemodificirani uzorak određen je gubitak mase, volumno bubrenje, učinak smanjenja bubrenja (ASE) i ravnotežni sadržaj vode (EMC). Određene su i tvrdoća prema Brinellu, dinamička tvrdoća, otpornost na izvlačenje vijaka i čavala te otpornost na

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habanje prema metodama Shaker i Taber abraser. Na temelju ovog istraživanja može se zaključiti da su toplinski modificirani uzorci drva *E. nitens* iz obje zemlje pokazali visok potencijal za uporabu u obliku vanjskih podnih obloga, posebice ako su modificirani pri 200 °C.

Ključne riječi: eukalipt, učinak smanjenja bubrenja (ASE), tvrdoća, otpornost na habanje, drvo

1 INTRODUCTION

1. UVOD

In the last 30 years there has been a steady growth of Eucalyptus nitens plantations in south of Chile and in the region of Galicia in Spain, as it is a species with great adaptability to frost and colder climate conditions. In Chile, there are about 250,000 ha planted as of 2014 (INFOR, 2015), while in Spain no official data are available. Only the current review for the Forestry Plan of Galicia (Xunta de Galicia, 2018), which analyzed the Spanish Forestry Inventory, and the Spanish Forestry Map suggested for *E. nitens* in this region forests of approximately 40,000 ha, and proposed an increase of 30,000 ha during the next 20 years. However, this number should be higher, as *E. nitens* plantations have been replacing *E. globulus* plantations due to its higher resistance against pathogens and cold.

Currently, *E. nitens* plantation wood is mostly used for pulp and paper or biofuels, but there is an interest to widen the use of this fast growing tree species. Solid wood made out of plantation *E. nitens* is being sold at the moment in Chile, but it cannot compete with other fast growing species, as the volume of plantations of radiata pine in Chile (INFOR, 2015) allows the species to maintain a competitive low price. As for Spain, there is still no market for dry *E. nitens* solid wood, but similar species (*E. globulus*). Thermal modification offers a good alternative to produce high quality material from this species that could be used for decking, claddings, windows, doors, flooring, garden products and even saunas or bathrooms (Miltz and Altgen, 2014). Most thermal modification processes apply temperatures between 160 °C and 240 °C and limit the oxygen content during the process (Hill, 2006; Esteves and Pereira, 2009; Miltz and Altgen, 2014). *E. nitens* (durability class 4, Australian Standard 5604 2005) and other eucalypt species, such as *E. globulus*, *E. grandis*, *E. regnans* and *E. pellita* (durability in ground contact class 3 – 4, Australian Standard 5604 2005), have been used as material for thermal modification (Esteves *et al.*, 2007a; Esteves *et al.*, 2007b; González-Prieto and Touza Vázquez, 2009; Calonego *et al.*, 2012; Wang *et al.*, 2014; de Cademartori *et al.*, 2015; Wentzel *et al.* 2019). In most cases research has been focused on the variation of color, the changes of the mechanical and physical properties and variations of the chemical composition.

In Eucalypt species, durability increases after thermal modification, as it has been shown in the resistance against the brown rot fungus *Gloeophyllum trabeum* for modified *E. globulus* from durability class 3 (DC 3, moderately durable) to DC 1 (very durable) (González-Prieto and Touza Vázquez, 2009). Changes

in mechanical properties of thermally modified Eucalypt species, such as a slight increase of *MOE* and a decrease in *MOR* (Table 1), were not a detriment of the potential for using this species for outdoor materials (Esteves *et al.*, 2007a; Calonego *et al.*, 2012; de Cademartori *et al.*, 2015; Knapic *et al.*, 2018; Wentzel *et al.*, 2019), as the *MOE* and *MOR* were still higher than those of commonly used WPC boards (Dias and Alvarez, 2017), a material commonly used for decking production (Zeller, 2018).

Currently, tropical woods such as Bangkirai (*Shorea laevis*), IPE-Lapacho (*Tabulea* spp.) or European-grown timbers such as Douglas fir (*Pseudotsuga menziesii*) and Larch (*Larix* spp.), and preservative treated pine are the most commonly used materials for decking. In addition to these traditional decking materials in Europe, wood polymer composite (WPC) decking is gaining market share throughout Europe (Zeller, 2018) not at least due to their good capabilities to suppress the moisture uptake and resulting moisture movements, but also due to the thermal conductivity of polymers. Thermal modification improves natural durability and dimensional stability, and decreases the equilibrium moisture content (*EMC*) of wood (Stamm and Hansen, 1937; Hill, 2006; Esteves and Pereira, 2009). Živković *et al.* (2008) used thermally modified ash (*Fraxinus* spp.) and beech (*Fagus sylvatica*) as flooring elements. When compared to unmodified wood, it showed a lower *EMC* in room conditions and an improvement in dimensional stability.

Thermal modification also leads to an embrittlement of wood coming along with reduced abrasion resistance and the risk of splintering on the wood surface (Kubojima *et al.*, 2000; Phuong *et al.*, 2007). Surface hardness and resistance to abrasion are critical properties in less and non-load-bearing applications. In the case of decking, surface hardness turns into a decisive property for its use (Brischke *et al.*, 2005). Welzbacher *et al.* (2009) showed that thermally treated beech and larch heartwood (*Larix decidua*) presented less abrasion and crack formation in relation to the unmodified wood, but showed long term discoloration by weathering. It is also important to consider how to connect the wood when installing the material. For outside use of thermally modified wood, it is recommended to use stainless screws and embedding screw heads (Ayitn *et al.*, 2015).

In this study the abrasion resistance, hardness (Brinell and dynamic), screw withdrawal resistance (*SWR*), maximum swelling, anti-swelling efficiency (*ASE*) and equilibrium moisture content (*EMC*) of thermally modified Eucalypt were determined since they are critical characteristics of outdoor exposed decking.

Table 1 Highest and lowest MOE and MOR from various thermally treated Eucalypts under different process conditions and their respective control values of unmodified specimens

Tablica 1. Najveći i najmanji modul elastičnosti i modul loma različitih toplinski obrađenih eukalipta pri različitim uvjetima obrade i vrijednosti njihovih nemodificiranih uzoraka

Species <i>Vrsta</i>	Thermal modification <i>Toplinska modifikacija</i>	Temperature, °C <i>Temperatura, °C</i>		MOE Unmodified specimen, MPa <i>MOE nemodificiranih uzoraka, MPa</i>	MOR Unmodified specimen, MPa <i>MOR nemodificiranih uzoraka, MPa</i>	MOE, MPa		MOR, MPa		Reference <i>Literatura</i>
		min	max			min	max	min	max	
<i>E. nitens</i>	Laboratory scale reactor (atmospheric pressure) <i>laboratorijski reaktor (atmosferski tlak)</i>	160	230	18449	119	14604	22224	88	134	Wentzel <i>et al.</i> , 2019
<i>E. nitens</i>	Laboratory scale reactor (high pressure) <i>laboratorijski reaktor (visoki tlak)</i>	150	170	18449	119	14464	16131	85	117	Wentzel <i>et al.</i> , 2019
<i>E. grandis</i>	Modified autoclave (air atmosphere) <i>modificirani autoklav (zračna atmosfera)</i>	180	240	12097	89	10623	12091	69	41	de Cademartori <i>et al.</i> , 2015
<i>E. saligna</i>	Modified autoclave (air atmosphere) <i>modificirani autoklav (zračna atmosfera)</i>	180	240	12869	90	12568	12805	75	47	de Cademartori <i>et al.</i> , 2015
<i>E. grandis</i>	Modified laboratory oven / <i>modificirani laboratorijski sušionik</i>	140	220	12800	69	12100	12400	65	33	Calonego <i>et al.</i> , 2012
<i>E. globulus</i>	Modified laboratory oven / <i>modificirani laboratorijski sušionik</i>	170	200	14197	-	10647	14339	-	-	Esteves <i>et al.</i> , 2007a
<i>E. globulus</i>	Modified laboratory oven / <i>modificirani laboratorijski sušionik</i>	-	210	13909	111	-	13379	-	102	Knapić <i>et al.</i> , 2018

2 MATERIALS AND METHODS

2. MATERIJALI I METODE

2.1 Material

2.1. Materijal

The Chilean *E. nitens* wood came from 19 year old plantations from the Región del Bío-Bío in Chile, while the wood from Spain came from 16 year old plantations from the north of the province of Lugo in Galicia. The wood specimens were taken randomly from piles of industrially dried wood from general production lines from sawmills in Chile and Spain, which is why the humidity was different at the same laboratory conditions before modification and there was a difference in their respective thickness. Flat sawn slats of 20 mm × 60 mm × 650 mm and 30 mm × 50 mm × 650 mm (radial × tangential × longitudinal) size, for the Chilean and Spanish origin, respectively, were prepared from kiln-dried wood free of large knots. Before the modification process, the slats from Chile had an

average moisture content of 13 %, whereas the ones from Spain had an average of 15 %. Twelve slats (six for each country of origin) per modification process were used.

2.2 Thermal modification

2.2. Toplinska modifikacija

Thermal modification was performed in a laboratory-scale treatment reactor. The modification followed the ThermoWood® process (Mayes and Oksanen, 2002) and contained the following steps: The temperature in the vessel was first raised at 12 °C/h to 100 °C and then at 2 °C/h to 130 °C to allow a high-temperature drying of the slats to nearly 0 % MC, before increasing the temperature again at 12 °C/h until reaching the peak temperatures (185, 200 and 215 °C). The peak temperature was hold for 3 h. Afterwards, the temperature was decreased at 20 °C/h until reaching 65 °C, at which the vessel was opened and the specimens were removed.

2.3 Determination of mass loss (ML)

2.3. Određivanje gubitka mase (ML)

To determine the mass loss (ML) for each modified slat caused by the thermal modification, an adaptation of the procedure reported by Metsä-Kortelainen *et al.* (2006) was applied. The mass and the corresponding wood moisture content (MC) were recorded for each slat before and immediately after the process.

2.4 Determination of oven-dry density

2.4. Određivanje gustoće apsolutno suhog drvna

The oven-dry density was determined according to ISO 13061-2 (2014) using five 8.5 mm × 8.5 mm × 35 mm (rad. × tang. × long.) specimens per modification, which were oven dried at (103±2) °C until constant mass. They were then weighed to the closest 0.01 g and their dimensions were measured to the nearest 0.01 mm.

2.5 Determination of equilibrium moisture content (EMC), volumetric swelling (S_{max}) and anti-swelling efficiency (ASE)

2.5. Određivanje ravnotežnog sadržaja vode (EMC), volumnog bubrenja (S_{max}) i učinka smanjenja bubrenja (ASE)

To measure EMC, S_{max} and ASE, 30 specimens per process run with dimensions of 10 mm × 10 mm × 10 mm (rad. × tang. × long.) were prepared from the modified wood and from unmodified references. The mass and the dimensions of the specimens were measured after each of the following steps: Conditioning at 20 °C/65 % RH until constant weight; oven drying at 103 °C until constant mass; water saturating (specimens were water-impregnated for 30 min at 13 kPa and water soaked for 14 days).

The EMC (in %) at 20 °C and 65 % RH was determined for each sample using Eq. 1:

$$EMC = 100 \cdot (m_A - m_B) / m_B \quad (1)$$

where m_A and m_B is the mass (in g) at the end of step A and B, respectively.

S_{max} (in %) was measured based on the sample volume at the end of step B and C for each cycle using Eq. 2:

$$S_{max} = 100 \cdot [(V_C - V_B) / V_B] \quad (2)$$

where V_B and V_C are the sample volumes at the end of step B and C, respectively.

ASE (in %) was measured using the S_{max} before and after modification using Eq. 3:

$$ASE = Su_{max} - Sm_{max} / Su_{max} \cdot 100 \quad (3)$$

where Su_{max} is the maximum swelling of the unmodified sample and Sm_{max} is the maximum swelling of the modified sample, respectively.

2.6 Brinell hardness tests

2.6. Tvrdoća prema Brinellu

The Brinell hardness (static hardness) was measured according to DIN EN 1534 (2011) with a universal testing machine (Zwick Roell Z10, Zwick, Ulm, Germany). Ten specimens per modification and country of origin were used. A maximum force of 500 N

using a steel ball with a diameter of 10 mm was applied for 25 seconds on specimens of 15 mm × 50 mm × 50 mm (rad. × tang. × long.) for the Chilean wood, and 25 mm × 50 mm × 50 mm (rad. × tang. × long.) for the Spanish wood. The specimens were conditioned at 20 °C/ 65 % RH during seven days until constant weight. The diameter of the residual impression was automatically determined by the testing machine. The Brinell hardness was then calculated according to Eq. 4:

$$BH = 2 \cdot F / \pi \cdot D \left[D - \sqrt{D^2 - d^2} \right], \quad (4)$$

where BH is the Brinell hardness (N/mm²), F is the maximum force used (N), D is the diameter of the steel ball (mm) and d is the diameter of the imprint on the sample (mm).

2.7 Dynamic hardness tests

2.7. Dinamička čvrstoća

The dynamic hardness was determined according to Meyer *et al.* (2011) using specimens of the same quantity and dimensions as for the Brinell hardness tests. An indentation was generated in the surface of the specimen using a steel weight of 500 g that was dropped down on a steel ball from 300 mm of height. Four measurements were conducted on five replicates per material. The dynamic hardness was calculated according to Eq. 5:

$$DH = m \cdot \sqrt{(2 \cdot g \cdot h)} / r^2 \cdot \pi \quad (5)$$

where DH is the dynamic hardness (N/mm²), m is the mass of the dropping weight (kg), h is the dropping height (m), r is the radius of the imprint on the sample (mm) and g is the gravity acceleration (m/s²).

2.8 Resistance to abrasion: Shaker test

2.8. Otpornost na habanje: metoda Shaker

The resistance against abrasion was determined using the Shaker method described by Brischke *et al.* (2005). Five oven-dry specimens of 8.5 mm × 8.5 mm × 35 mm (rad. × tang. × long.) were placed in polyethylene flasks ($V = 500$ mL) together with 400 g stainless steel balls of 6 mm in diameter and shaken in an overhead shaker at 28 revolutions per minute during 72 h. 25 specimens per material were tested. The distances between the opposite corners at oven-dry state were measured of each specimen, before and after the abrasion process. The loss in dimension (%) was determined according to Eq. 6:

$$\Delta ab = [(d_{a1} + d_{a2} / 2) - (d_{b1} + d_{b2} / 2) / (d_{b1} + d_{b2} / 2)] \cdot 100 \quad (6)$$

where Δab is the abrasion (%), d_{b1} is the diagonal 1 before abrasion (mm), d_{b2} is the diagonal 2 before abrasion (mm), d_{a1} is the diagonal 1 after abrasion (mm) and d_{a2} is the diagonal 2 after abrasion (mm). The average of the 5 samples per flax bottle was determined for each modification.

2.9 Resistance to abrasion: Taber Abraser test

2.9. Otpornost na habanje: metoda Taber abraser

The resistance against abrasion was determined according to the Taber Abraser method (EN 438-2, 2005). The following modifications of the Taber Abra-

ser test were made in order to allow testing of solid wood: Specimens (n=4) of 100 mm × 100 mm × 7 mm of a finished decking were prepared and conditioned in 20 °C/65 % RH. The tree rings of all specimens had an orientation of 45° to their cutting edges. After weighing and measuring the thickness at four points over the ridges of the decking, the specimens (n=5) were clamped into the Taber Abraser and were abraded with sanding paper S-42 with approx. 72 min⁻¹ for 1000 revolutions. Each wheel had a load of 500 g. Afterwards the decrease in thickness at each of the four abrasion points was determined. The percentage loss in thickness (Δt) was determined as a measure of abrasion according to the following Eq. 7 for each specimen and an average was calculated:

$$\Delta t = (t_b - t_a / t_b) \cdot 100 \quad (7)$$

where t_b is the thickness (mm) before the Taber Abrasion test and t_a is the thickness (mm) after the test.

2.10 Screw withdrawal resistance tests

2.10. Ispitivanje otpornosti na izvlačenje vijaka

Screw withdrawal resistance (*SWR*) tests were performed according to EN 320 (2011), but modified as follows: The same quantity and size of specimens used for the Brinell hardness test were used. Screws with nominal dimensions of 4.2 mm × 38 mm were used to penetrate the tangential face until (15±0.5) mm. Afterwards the screws were attached to a bracket to be pulled out at a constant speed of (10±1) mm min⁻¹. The screw withdrawal resistance corresponds to the maximum force determined to 10 N and was measured according to equation 8:

$$SWR = N_{max} / t \quad (8)$$

where *SWR* is the screw withdrawal resistance, N_{max} the maximum force (N) and *t* the thickness of the specimen (mm).

2.11 Statistical evaluation

2.11. Statistička analiza

Statistical analysis was performed using the Pearson Correlation Coefficient Test to show the correlations between the mass loss and density with the properties of the modified wood, and an ANOVA test to see if there was a significant difference between the

unmodified and the modified wood properties. All statistics were performed using the Statistica Software package Version 13.1 (StatSoft Inc., Tulsa, USA).

3 RESULTS AND DISCUSSION

3. REZULTATI I RASPRAVA

3.1 Changes in mass, oven dry density, EMC, swelling and ASE by thermal modification

3.1. Promjene mase, gustoće apsolutno suhog drva, EMC-a, bubrenja i ASE-a zbog toplinske modifikacije

ML increased with rising treatment temperature (Table 2), which is in line with increasing *ML* obtained in tests with other Eucalypt species at similar process conditions, such as *E. saligna* (from 12.77 % at 180 °C and 19.12 % at 220 °C) in a modified autoclave modification (de Cademartori *et al.*, 2015) and *E. globulus* (8.7 % at 190 °C and 12.1 % at 200 °C) in a modified laboratory oven modification (Esteves *et al.*, 2007a). The higher *ML* of those modifications could be related to the different species and equipment used to do the modifications. Specimens from Chile and Spain showed similar *ML* at each modification temperature. On the other hand, oven-dry density (Table 1) decreased with increasing modification temperature, which also occurred in vacuum-thermally modified *E. pellita* wood (Wang *et al.*, 2014) and *E. grandis* (Calonego *et al.*, 2012). The oven-dry density of the Spanish wood specimens was lower than that of the Chilean ones.

The *EMC* of the modified wood was reduced in both the Chilean and Spanish specimens (Figure 1a) after all the thermal modifications, and so was S_{max} (Figure 1b). Eucalypt modified under similar conditions, such as *E. grandis* in both *EMC* (5.9 % at 200 °C and 4.6 % at 220 °C) and S_{max} (9.94 % at 200 °C and 6.6 % at 220 °C) (Calonego *et al.*, 2012) and *EMC* (3.1 % at 190 °C and 2.8 % at 210 °C) in *E. globulus* (Esteves *et al.*, 2007b), showed similar results. Compared with other tropical wood species used for decking (Choong and Achmadi, 2007), the *EMC* of *E. nitens* was lower after treatment at 215 °C and similar at 185 °C and 200 °C. *ASE* of *E. nitens* was lower after modification at 185 °C (26.14 % and 23.11 % for Chile and Spain, respectively) (Figure 1c) compared to the modifications at higher temperatures. This improvement of the

Table 2 Mean mass loss (*ML*) determined for each process run and oven-dry density for each modification and unmodified reference (standard deviation in parentheses) for both Chilean and Spanish specimens

Tablica 2. Srednja vrijednost gubitka mase (*ML*) određena za svaki proces i gustoća apsolutno suhog drva određena za svaki modificirani i nemodificirani referentni uzorak (standardne devijacije u zagradama) za čileanske i španjolske vrste drva eukalipta

Country of origin <i>Zemlja podrijetla</i>	Temperature, °C <i>Temperatura, °C</i>	<i>ML</i> , %	OD Density, kg/m ³ <i>Gustoća apsolutno suhog drva, kg/m³</i>
Chile / Čile	Reference	-	617 ± (16)
	185	2.4 ± (0.4)	603 ± (39)
	200	6.1 ± (1.0)	592 ± (23)
	215	12.3 ± (0.5)	553 ± (29)
Spain / Španjolska	Reference	-	574 ± (26)
	185	2.6 ± (0.9)	555 ± (35)
	200	5.7 ± (1.3)	529 ± (18)
	215	12.0 ± (0.9)	517 ± (35)

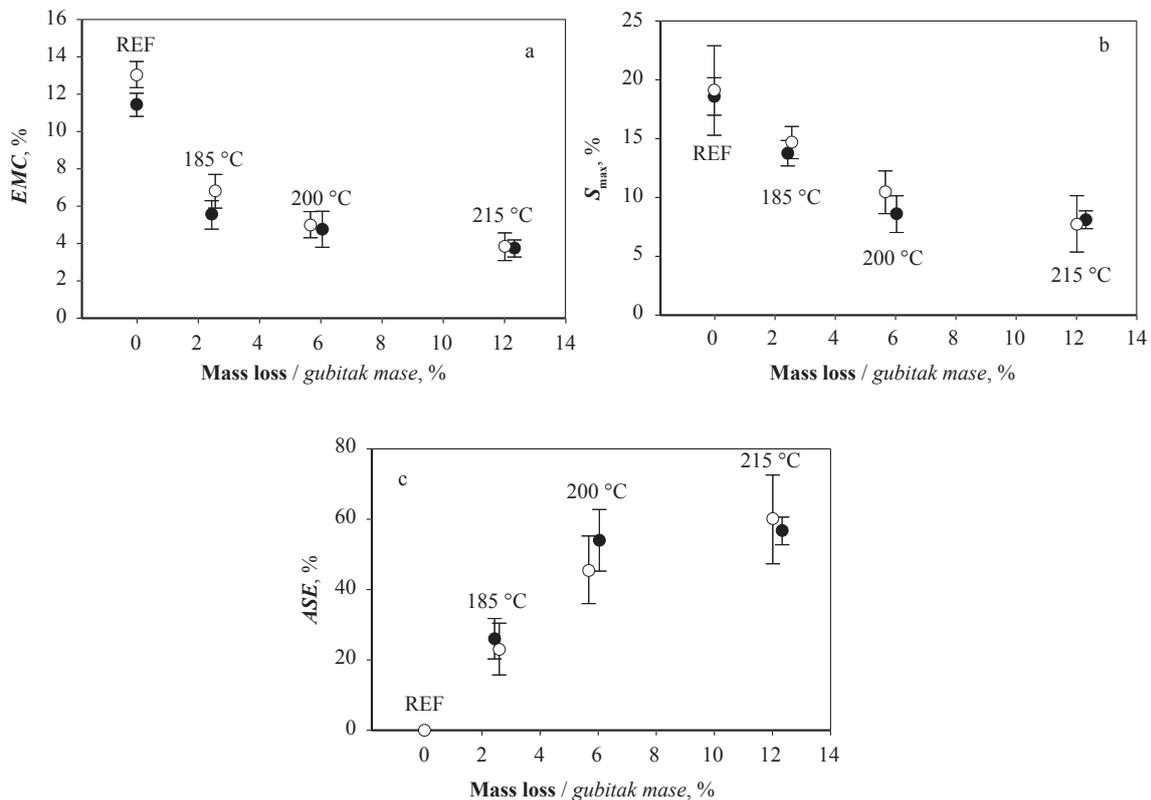


Figure 1 EMC at 20 °C and 65 % RH (a), S_{max} (b) and ASE (c) of *E. nitens* depending on the mass loss by thermal modification. Black circles: Chilean specimens. White circles: Spanish specimens. Standard deviations are indicated by error bars
Slika 1. EMC pri 20 °C i 65 % RH (a), S_{max} (b) i ASE (c) drva *E. nitens* u ovisnosti o gubitku mase zbog toplinske modifikacije (crni krugovi – čileanski uzorci; bijeli krugovi – španjolski uzorci); standardne devijacije prikazane su kao stupci pogreške

dimensional stability in thermally modified wood was also shown for *F. sylvatica* and *Fraxinus* spp. (Živković *et al.*, 2008). As for other eucalypt species, the ASE of thermally modified *E. globulus* reported by Esteves *et al.* (2007b) was higher (73 – 90 % at 190 to 210°C).

3.2 Changes in hardness, abrasion and screw withdrawal by thermal modification

3.2. Promjene tvrdoće te otpornosti na habanje i izvlačenje vijaka zbog toplinske modifikacije

Static hardness (Brinell) of the Chilean material was higher than that of the Spanish material. A Pearson correlation test showed that only the decrease in density was statistically significantly correlated with the dynam-

ic and static hardness in the Chilean specimens (Table 3), while the Spanish specimens showed an increase in hardness unrelated to their densities after thermal modification at 200 °C (Figure 2). There was a slight decrease until 200 °C, and then a clear difference between unmodified specimens and those modified at 215 °C, while the Spanish material showed a noticeable decrease after all modifications (Figure 2a). Dynamic hardness decreased with increasing treatment temperature in the Chilean specimens, while at 185 °C and 200 °C similar results were obtained for the Spanish specimens (Figure 2b). The static and dynamic hardness at all temperatures was lower compared to both WPC (70 N/mm²) and tro-

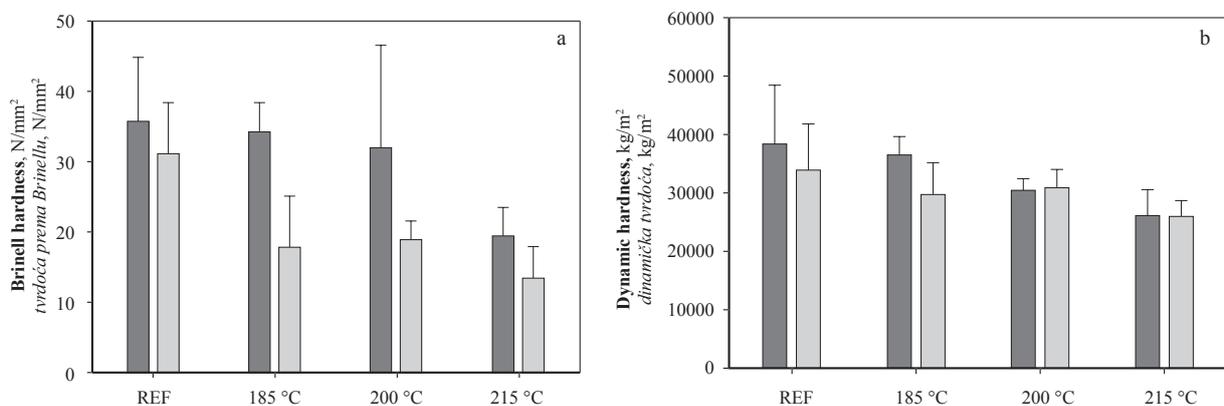


Figure 2 Brinell (a) and dynamic (b) hardness of *E. nitens* after each thermal modification process. Black column: Chilean specimens. Grey column: Spanish specimens

Slika 2. Tvrdoća prema Brinellu (a) i dinamička tvrdoća (b) drva *E. nitens* nakon svake toplinske modifikacije (crni stupci – čileanski uzorci; sivi stupci – španjolski uzorci)

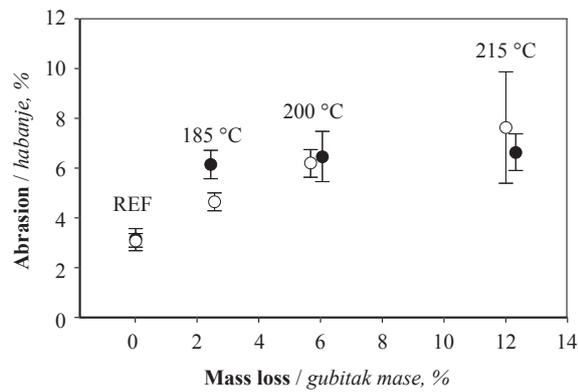


Figure 3 Abrasion of *E. nitens* after shaker tests depending on the mass loss by thermal modification. Black circles: Chilean specimens. White circles: Spanish specimens. Standard deviations are indicated by error bars

Slika 3. Otpornost na habanje drva *E. nitens* određena metodom *Shaker* u ovisnosti o gubitku mase zbog toplinske modifikacije (crni krugovi – čileanski uzorci; bijeli krugovi – španjolski uzorci); standardne devijacije prikazane su kao stupci pogreške

pical species, such as Bongossi (*Lophira alata*) and Balau (*Shorea* spp) (both 83 N/mm²), but similar to Douglas fir (35 N/mm²) and Beech (39 N/mm²) (Brischke *et al.*, 2014) at 200 °C for the Chilean specimens. The Brinell hardness was similar to thermally treated European beech and European ash (35 N/mm²)

treated between 180 and 200 °C in standard thermal modification under atmospheric conditions (Standfest and Zimmer, 2008), while the dynamic hardness was lower than that of European beech modified at 180 °C and with similar mass loss (Meyer *et al.*, 2011).

The abrasion resistance of *E. nitens* decreased with increasing treatment intensity in all the specimens (Figure 3). Traces of abrasion on unmodified and thermally modified *E. nitens* at 215 °C after the shaker test can be seen in Figures 4 and 5 for Chilean and Spanish specimens, respectively. The thermally modified specimen (Figure 4c, d and Figure 5c, d) had more severely rounded edges and a slight loss of material due to splintering. The reduced abrasion resistance is likely due to an increased brittleness of the material (Kuboji-ma *et al.*, 2000; Phuong *et al.*, 2007), and the lower density of the material after thermal modification (Esteves and Pereira, 2009). Previous reports indicated that the decrease in abrasion resistance is correlated with the decrease in wood density (Brischke *et al.*, 2014). This also occurred in both our Spanish and Chilean specimens, shown to be statistically significant in Table 3. Wentzel *et al.* (2019) showed that there was a decrease in the degree of polymerization of the cellulose in thermally modified *E. nitens* wood, which means that there was a change in the cellulose crystallinity. Estevez and Pereira (2009) suggest that changes in the cellulose crystallinity influence the mechanical

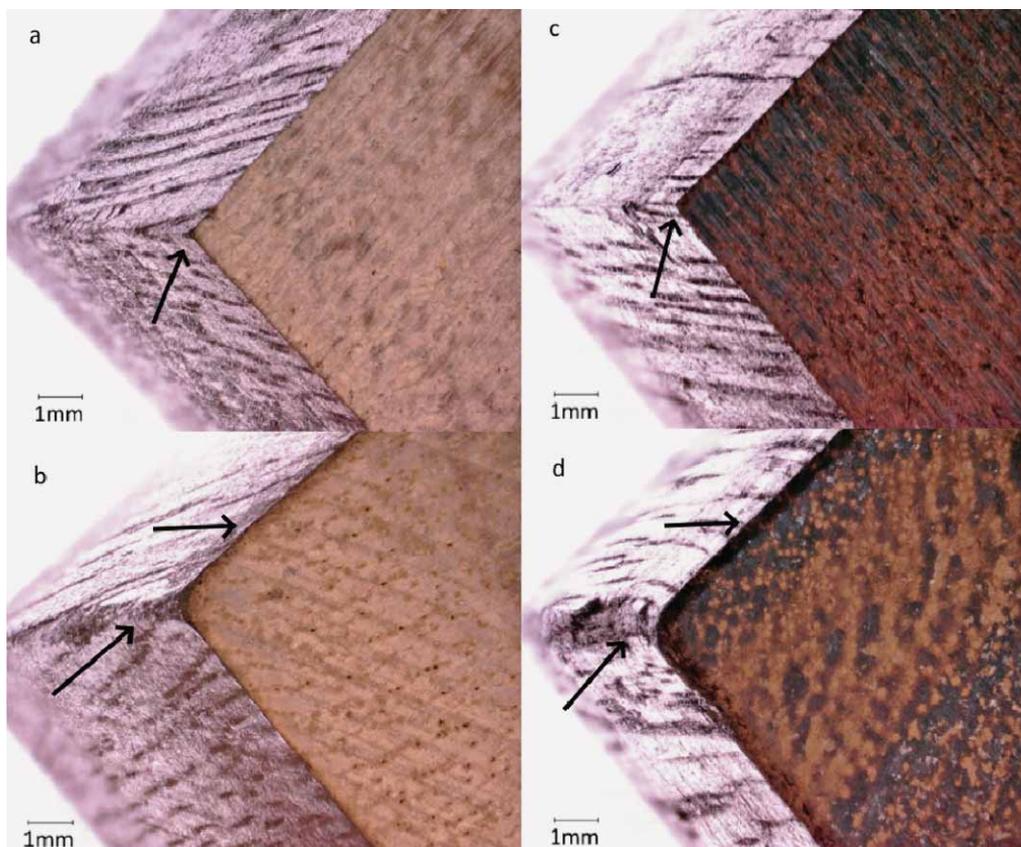


Figure 4 Cross section of *E. nitens*, unmodified and thermally modified at 215 °C of the Chilean specimens before (a and c) and after (b and d) the shaker abraser test. Arrows show the differences of wear between unmodified and modified specimens

Slika 4. Poprečni presjek čileanskih nemodificiranih i na 215 °C modificiranih uzoraka drva *E. nitens* prije (a i c) i nakon (b i d) ispitivanja otpornosti na habanje metodom *Shaker*; strelice pokazuju razlike u habanju između nemodificiranih i toplinski modificiranih uzoraka drva

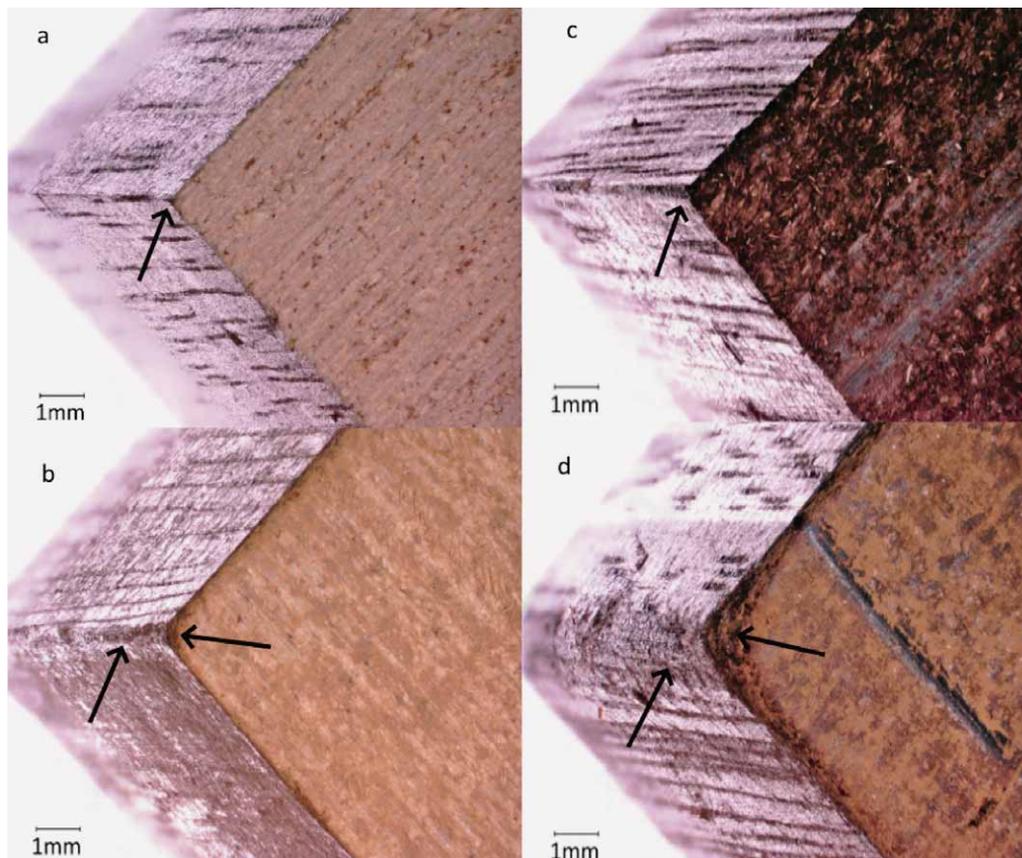


Figure 5 Cross section of *E. nitens*, unmodified and thermally modified at 215 °C of the Spanish specimens before (a and c) and after (b and d) the shaker abraser test. Arrows show the differences of wear between unmodified and modified specimens **Slika 5.** Poprečni presjek španjolskih nemodificiranih i na 215 °C modificiranih uzoraka drva *E. nitens* prije (a i c) i nakon (b i d) ispitivanja otpornosti na habanje metodom *Shaker*; strelice pokazuju razlike u habanju između nemodificiranih i toplinski modificiranih uzoraka drva

properties of thermally modified wood, which could also be an explanation of the reduction of abrasion resistance. Compared to other flooring materials, the unmodified *E. nitens* showed similar abrasion resistance as wood-polymer composites (WPC) and tropical species such as Balau (2.9 and 3 %), while *E. nitens* modified at 200 °C and 215 °C presented similar resistance to abrasion as Douglas fir and Norway spruce (*Picea abies*), and namely 6.2 % (Brischke *et al.*, 2014)

The abrasion expressed as Δt increased with increasing modification temperature in the Spanish spe-

cimens, while the Chilean specimens showed only small differences between modifications (Figure 6). The measurements were performed on finished decking (Figure 7), where the difference in Δt can be seen between the modified specimens at 215 °C (Chile in Figure 7c and Spain in Figure 7d), more material being lost in the Spanish specimens.

The screw withdrawal resistance (*SWR*) decreased with increasing treatment temperature, but did not differ between Spanish and Chilean *E. nitens* (Figure 8). Similar effects of thermal modification on

Table 3 Pearson correlation coefficients for mass loss and density in relation to *EMC*, *ASE*, shaker test, Taber Abraser test, Brinell hardness, dynamic hardness and *SWR*. Significant correlations ($p < 0.05$) were marked with an asterisk (*)

Tablica 3. Pearsonov koeficijent korelacije za gubitak mase i gustoću u ovisnosti o *EMC*-u, *ASE*-u, metodi *Shaker*, metodi *Taber abraser*, tvrdoći prema Brinellu, dinamičkoj tvrdoći i *SWR*-u. Značajne korelacije označene su zvjezdicom (*).

Properties Svojstva	Pearson correlation coefficient Pearsonov koeficijent korelacije			
	Chile / Čile		Spain / Španjolska	
	Mass loss Gubitak mase	Density Gustoća	Mass loss Gubitak mase	Density Gustoća
<i>EMC</i>	-0.996*	0.991*	-0.952*	0.994*
<i>ASE</i>	0.797*	-0.913*	0.955*	-0.993*
Shaker Test / Metoda <i>Shaker</i>	0.950*	-0.996*	0.977*	-0.979*
Taber Abraser Test / Metoda <i>Taber abraser</i>	0.999*	-0.962*	0.943*	-0.996*
Brinell Hardness / Tvrdoća prema Brinellu	-0.973*	0.896*	-0.873*	0.597
Dynamic Hardness / Dinamička tvrdoća	-0.966*	0.999*	-0.856*	0.570
<i>SWR</i>	-0.985*	0.998*	-0.805*	0.492

Table 4 Average values of EMC, abrasion tests, hardness tests and screw withdrawal test of unmodified and modified specimens. Significant differences with unmodified average values are marked by letter a. No significant differences are marked by letter b

Tablica 4. Srednja vrijednost EMC-a, otpornosti na habanje, tvrdoće i otpornosti na izvlačenje vijaka nemodificiranih i modificiranih uzoraka. Značajne razlike u odnosu prema srednjim vrijednostima nemodificiranih uzoraka označene su slovom a, dok su slučajevi bez značajne razlike označeni slovom b.

Chile / Čile	EMC, %	Shaker test Metoda Shaker, %	Taber Abraser test / Metoda Taber abraser, %	Brinell hardness Tvrdoća prema Brinellu, N/mm ²	Dynamic hardness Dinamička tvrdoća kg/m·s	SWR, N/mm
Unmodified nemodificirani	11.48 ^a	5.79 ^a	3.21 ^a	35.82 ^a	38341 ^a	48.68 ^a
C185	5.55	7.41	6.15	34.24	36481	40.46
C200	4.75	7.91	6.46	32.08	30395	31.62
C215	3.76	8.96	6.64	19.51	26224	23.34
Spain Španjolska	EMC, %	Shaker test Metoda Shaker, %	Taber Abraser test / Metoda Taber abraser, %	Brinell hardness Tvrdoća prema Brinellu, N/mm ²	Dynamic hardness Dinamička tvrdoća kg/m·s	SWR, N/mm
Unmodified nemodificirani	13.06 ^a	3.41 ^a	3.06 ^a	31.19 ^a	33836 ^b	47.36 ^a
S185	6.81	4.93	4.67	17.88	29728	34.12
S200	5.00	8.41	6.20	18.91	30835	37.48
S215	3.81	10.51	7.63	13.52	25891	26.60

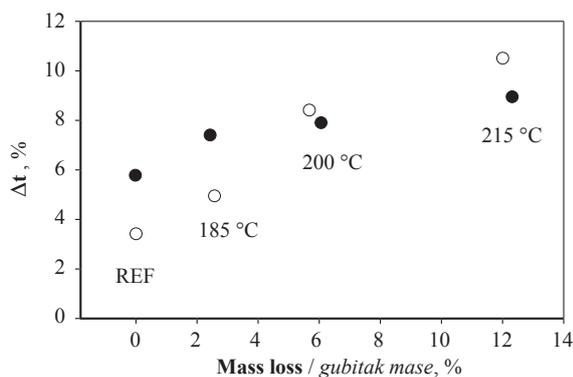


Figure 6 Abrasion of *E. nitens* after Taber Abraser tests depending on the mass loss by thermal modification. Black circles: Chilean specimens. White circles: Spanish specimens
Slika 6. Otpotnost na habanje drva *E. nitens* određena metodom *Taber abraser* u ovisnosti o gubitku mase zbog toplinske modifikacije (crni krugovi – čileanski uzorci; bijeli krugovi – španjolski uzorci)

SWR were previously reported for birch (Poncsák *et al.*, 2006) and wild cherry (Aytin *et al.*, 2015).

3.3 Statistical analysis 3.3. Statistička analiza

The correlations presented in Table 3 show that mass loss was positively correlated with ASE and negatively with the resistance to abrasion in the shaker and abraser test, EMC, SWR and dynamic and Brinell hardness. Most correlations were significant. Only density was not correlated with SWR and dynamic and Brinell hardness in the modified wood from Spain, due to a slight increase of the properties in the modification at 200 °C.

As for the ANOVA test, all properties presented significant differences between the unmodified and modified specimens, with the exception of the dynamic hardness of the modified samples from Spain, as can be seen in Table 4.

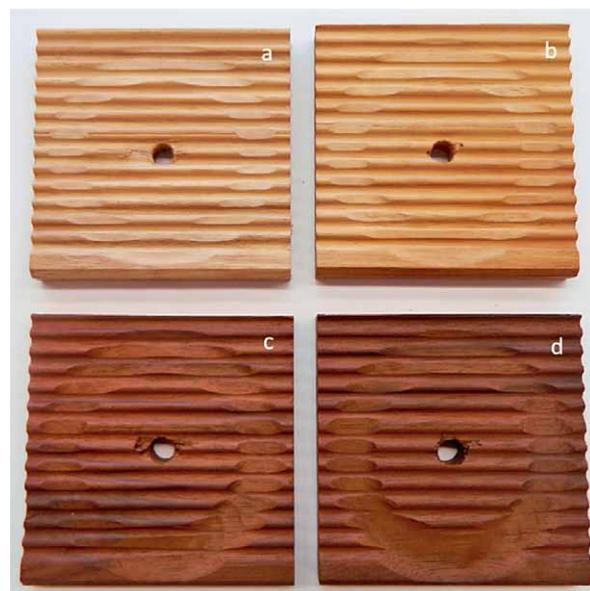


Figure 7 Finished decking specimens after the Taber Abraser test. *E. nitens* wood, unmodified and thermally modified at 215°C of the Chilean and Spanish specimens before (a and b) and after (c and d) the Taber Abraser test
Slika 7. Uzorci vanjskih podnih obloga nakon ispitivanja otpornosti na habanje metodom *Taber abraser*; nemodificirani i na 215 °C modificirani uzorci drva *E. nitens* iz Čilea i Španjolske prije (a i c) i nakon (b i d) ispitivanja otpornosti na habanje metodom *Taber abraser*

The results indicate that the characteristics of thermally treated *E. nitens* from our study, especially the modification at 200 °C for both countries, were similar to other species commonly used for decking, such as Douglas fir (Brischke *et al.*, 2014), and other thermally modified species, like *Larix decidua* (Welzbacher *et al.*, 2009), *F. sylvatica* and *Fraxinus* spp. (Živković *et al.*, 2008), which means that the modified *E. nitens* wood could be a probable alternative for decking.

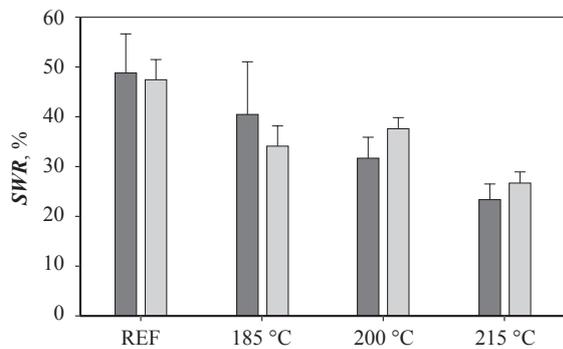


Figure 8 Screw withdrawal resistance of *E. nitens* depending on the mass loss by thermal modification. Black column: Chilean specimens. Grey column: Spanish specimens

Slika 8. Otpornost na izvlačenje vijaka drva *E. nitens* u ovisnosti o gubitku mase zbog toplinske modifikacije (crni stupci – čileanski uzorci; sivi stupci – španjolski uzorci)

4 CONCLUSIONS

4. ZAKLJUČAK

Thermally modified *E. nitens*, from both Chile and Spain, showed very similar characteristics compared to each other. The properties obtained modifying at 200 °C were similar to other species commonly used for decking, showing high abrasion resistance and similar dynamic and static properties. This shows the potential of use of *E. nitens* as decking material, particularly modified at 200 °C. To further develop the potential of this species as decking material, additional weathering and durability tests should be performed to determine the long-term use of this material.

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