

# CIGARETTE BUTTS AND WASTE COFFEE GROUNDS AS ADDITIVES TO BRICK CLAY

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## ABSTRACT

The paper analyses the influence of cigarette butts and waste coffee grounds addition on the properties of the brick clay. The waste materials were added to the clay in amounts of 5 wt.% and 10 wt.%. Standard consistency, plasticity, drying and firing behaviour and refractoriness were tested on the clay sample and the samples with wastes additions. Apparent density, apparent porosity, water absorption, strength and thermal conductivity were investigated on the samples fired at 1173 K. Addition of the waste materials improved thermal insulation characteristics and drying shrinkage, while other properties remain within the required limits for brick industry.

**Keywords:** waste utilization, clay, cigarette butts, waste coffee grounds, brick

## INTRODUCTION

Environmentally friendly materials are a very important research field nowadays. Clay bricks, as one of the most frequently used building materials, are a very interesting research material because of their durability, fire resistance, strength, aesthetic characteristics, insulating and many other properties. The main raw material for brick production is clay. However, reserves of the clay are limited, and it is necessary to find the additives that could partially replace the main raw material. Part of the raw material can be replaced by waste material which would lead to savings natural resources and solving problems connected to disposal of certain

types of the waste [1 - 4]. In this paper, the effect of adding cigarette butts and coffee waste to the clay was investigated. Cigarette butts and coffee waste are types of organic waste and it is estimated that every year about  $4.5 \cdot 10^{12}$  cigarettes are littered in the world [5] and coffee is consumed by around 40 % of the world's population and for many people, especially in the Western countries, drinking coffee is a part of their lifestyle and an everyday habit [6]. The rate of generation of coffee grounds was estimated at an average rate of 3 t of waste per million euros of product sales [7]. The organic additives such as cigarette butts and coffee waste, mixed in the brick clay are burning out during the firing process producing additional amounts of

energy, and decreasing the total fuel consumption of the industrial furnace [8]. This allows economical use of the energy needed for the firing [7] and shortens the firing time [9]. Also, when the combustible material burns out, it leaves a large fraction of pores within the fired body. The presence of the pores in the materials decreases their thermal conductivity and therefore increases their thermal insulation properties. Also, such produced bricks are lighter compared to the traditional ones [7]. The porous character of these light bricks will increase the quality of structures in terms of heat insulation, thereby reducing heating costs and in turn affecting environment positively. However, mechanical properties of the bricks are negatively affected as a result of physical, chemical and mineralogical alteration [10].

## EXPERIMENTAL

### Materials and sample preparation

The raw materials used in this investigation were clay from “Čavka” deposit situated in the Central Bosnia and Herzegovina near Busovača and cigarette butts and waste coffee grounds from the household. The clay was crushed, dried at  $373 \pm 5$  K and sieved through the 1-mm sieve. Only for the purpose of standard consistency and plasticity determination, clay was sieved through the 425- $\mu$ m sieve. The waste coffee grounds were also dried at  $373 \pm 5$  K. The cigarette butts were dried at  $333 \pm 5$  K and ground in electric kitchen chopper for one minute. Five types of mixture were prepared. Their compositions are shown in Table 1.

Table 1. Compositions of prepared mixtures

Material	Mixture [wt.%]				
	1	2	3	4	5
Clay	100	95	90	95	90
Cigarette butts	0	5	10	0	0
Waste coffee grounds	0	0	0	5	10

The mixtures were manually kneaded with tap water. In the standard consistency and plasticity tests different amounts of water were added to the clay. For other examinations the water was added according to standard consistency. Three different forms of samples were prepared. Plates of dimensions 300 x 300 x 30 mm were prepared for thermal conductivity determination. For compressive and flexural strength determination the prisms with dimensions of 160 x 40 x 40 mm were prepared. For all other tests, 80 x 40 x 14 mm tiles were prepared. All prepared samples were air-dried for 3 days, followed by drying in drying oven for 24 hours at 303 K and 24 hours at 373 K. After drying, all the samples (tiles, prisms and plates) were fired at 1173 K. The overall firing process lasted about 21 hours, while the highest temperature was kept for 2 hours.

### Methods of characterization

Chemical composition of clay and waste coffee grounds was determined by the following procedures: loss of ignition was determined by the gravimetric analysis after annealing at 1173 K, SiO<sub>2</sub> content was also determined by gravimetric method, the contents of Al<sub>2</sub>O<sub>3</sub>, Fe<sub>2</sub>O<sub>3</sub>, TiO<sub>2</sub>, CaO, MgO, K<sub>2</sub>O, Na<sub>2</sub>O and MnO were determined after the acidic dissolution at the Atomic Absorption Spectrophotometer (AAS, Perkin Elmer 3100), the contents of C and H were determined on a STROHLEIN elemental analysis device by combustion in air steam and deposition on appropriate substrate, and content of N was determined with a standard Macro-Kjeldahl method. Differential thermal analysis (DTA) and thermogravimetric (TG) analysis were carried out to investigate the raw materials and mixtures behaviour during the thermal treatment. It was done on the NETZSCH thermal analysis instrument STA 409 CD in nitrogen atmosphere up to 1473 K with heating rate 20 K/min. Phase composition of the clay was investigated by X-ray diffraction analysis on a Shimadzu diffractometer XRD-6000 with Cu K $\alpha$  radiation (XRD), with accelerating voltages of

40 kV and current 30 mA, in the range of angles  $2-80^\circ 2\theta$  with a step  $0.02^\circ 2\theta$  and a dwell time of 0.6 seconds. Standard consistency was determined using Vicat apparatus [11]. Plasticity was determined by the Pfefferkorn plasticity tester [12]. Diagonals were drawn on the prepared tiles and, using a metal device, a circle was drawn with a center at the intersection of the diagonals. The cross-section of the circle with the diagonals gave the reference points which were used to determine drying and firing shrinkage. The equations for the mass loss and shrinkage determination are:

$$\text{Mass loss} = \frac{G_0 - G_1}{G_0} \cdot 100 [\%] \quad (1)$$

$$\text{Shrinkage} = \frac{S_0 - S_1}{S_0} \cdot 100 [\%] \quad (2)$$

where:  $G_0$  – mass of tile before thermal treatment [g],  $G_1$  – mass of tile after thermal treatment [g],  $S_0$  – distance between reference points before thermal treatment [mm],  $S_1$  – distance between reference points after thermal treatment [mm].

To saturate the pore space the tiles were soaked in water to the half of their height for 24 hours. After that, water was added to completely cover the samples and thus left for another 24 hours. The following equations were used to determine water absorption ( $WA$ ), apparent porosity ( $P_a$ ) and apparent density ( $\gamma$ ):

$$WA = \frac{m_3 - m_1}{m_1} \cdot 100 [\%] \quad (3)$$

$$P_a = \frac{m_3 - m_1}{m_3 - m_2} \cdot 100 [\%] \quad (4)$$

$$\gamma = \frac{m_1}{m_3 - m_2} \cdot \rho_w [\text{g/cm}^3] \quad (5)$$

where:  $m_1$  – mass of dry tile [g],  $m_2$  – mass of saturated tile in water – hydrostatic weighing [g],  $m_3$  – mass of saturated tile on air [g],  $\rho_w$  – water density [ $\text{g/cm}^3$ ].

Thermal conductivity was tested on the samples with dimensions of 50 x 50 x 20 mm excised from the plates (two samples for the testing) by device Hot Disk TPS 2200 (the product of the Hot Disk AB Company from Gothenburg in Sweden). Refractoriness of the fired samples was investigated in Kryptol furnace according to the standard EN 993-2. Compressive and flexural strength were determined according to the standard EN 196-1. The images of crushed surfaces after testing for compressive and flexural strength were taken by the OLYMPUS BX60M binocular optical microscope at 12.5x magnification.

## RESULTS AND DISCUSSION

Table 2 presents chemical composition of the clay from “Čavka” and waste coffee grounds. Based on the results it can be observed that the examined clay contained  $\text{SiO}_2$  and  $\text{Al}_2\text{O}_3$  in major quantities and is typical brick clay with higher content of  $\text{Fe}_2\text{O}_3$  and a lower content of  $\text{CaO}$ . The chemical composition of the waste coffee grounds indicates that it is an organic material which is almost completely transformed into the gaseous phase when heated. Cigarette filter consists essentially of cellulose acetate. Although cigarette butts contain a large number of compounds (including aromatic and heterocyclic amines, carbonylated compounds, phenols, polycyclic aromatic hydrocarbons, carbon and nitrogen oxides and ammonia) [13], many of which are dangerous, research has shown that the concentration values for 11 metals measured in the leaching test on clay bricks manufactured with cigarette butts were insignificant and much lower than the acceptable regulatory limits [14].

Mineralogical examination based on X-ray diffraction analysis, presented in the Figure 1, revealed the presence of quartz, illite, kaolinite, clinochlor and anorthite in the clay sample. Such composition is typical for the central Bosnia's clays [15].

Table 2. Chemical composition of the clay and the waste coffee grounds

Component	Chemical composition [%]	
	Clay	Waste coffee grounds
SiO <sub>2</sub>	54.1	0.08
Al <sub>2</sub> O <sub>3</sub>	19.1	< 0.01
Fe <sub>2</sub> O <sub>3</sub>	10.2	0.01
TiO <sub>2</sub>	1.5	0.25
CaO	0.36	0.78
MgO	2.82	0.17
K <sub>2</sub> O	3.51	0.47
Na <sub>2</sub> O	1.15	0.01
MnO	0.14	< 0.01
P <sub>2</sub> O <sub>5</sub>	0.183	0.206
LOI	6.57	98.7
C	-	52.8
H	-	8.54
N	-	2.52

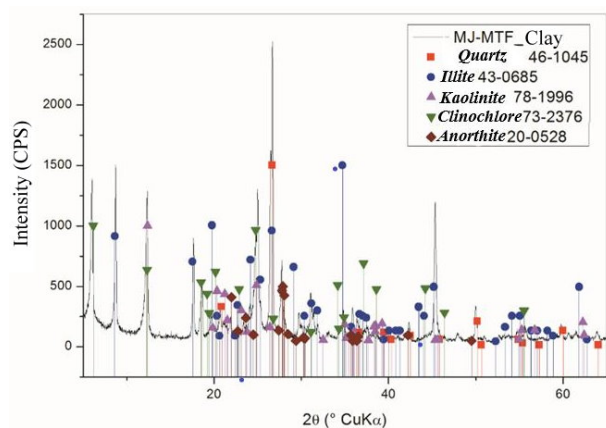


Figure 1. Phase composition of the “Čavka” clay

Figure 2 shows DTA/TG/DTG curves for the clay. Mass loss obtained by thermogravimetric analysis is well-matched with loss on ignition in chemical analysis. Clay lost mass in a few steps indicating a greater number of minerals. The first significant loss occurs up to the temperature of 623 K in three steps. On DTA curve followed by two endothermic peaks at about 433 K and 573 K, corresponding to the loss of adsorbed and zeolite water from illite, chlorite, limonite and goethite [16 - 23].

The content of K<sub>2</sub>O in chemical analysis is indicative of the amount of illite [21]. The presence of kaolinite and illite, identified by

XRD analysis, is confirmed by mild endothermic change on DTA curve and mass loss between 773 and 873 K on TG curve and mild change on DTG curve [16, 17, 24, 25]. DTA curves of cigarette butts and waste coffee grounds show board exothermic changes corresponding to decomposition of organic components. The decomposition of cigarette butts occurs mostly below 673 K (Figure 3a) in one step, which means that it mainly consists of a single substance, while the decomposition of the waste coffee grounds occurs mostly below 800 K (Figure 3b) in two main steps, which points to a more complex composition of waste coffee grounds. The mass loss of waste coffee grounds in thermogravimetry is lower than the loss of ignition, but the test conditions should be considered. Thermogravimetry was made in a nitrogen atmosphere, so there was no complete combustion of the substance as in the chemical analysis.

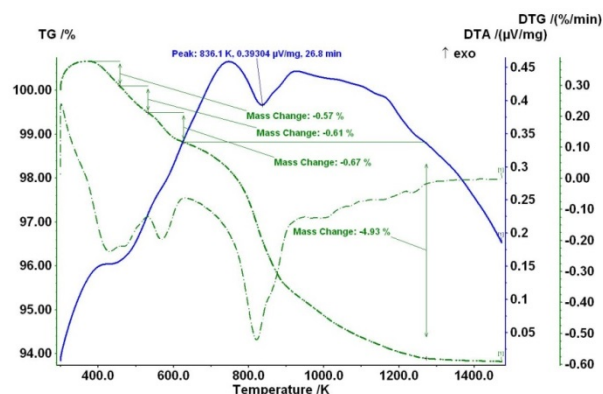


Figure 2. DTA/TG/DTG of the “Čavka” clay

The results of the standard consistency and Pfefferkorn plasticity tests are given in Table 3. Table 4 presents the results of mass loss and shrinkage on drying and firing. The results of the Pfefferkorn plasticity tests indicate that the increase in the additives amounts leads to increasing the amount of water required to reach 30 % height contraction of the test body. So, it might be concluded that the addition of waste coffee grounds and cigarette butts makes the clay more plastic. However, the Pfefferkorn method determines raw material plasticity as water content and not as the resistance to penetration or plastic deformation.

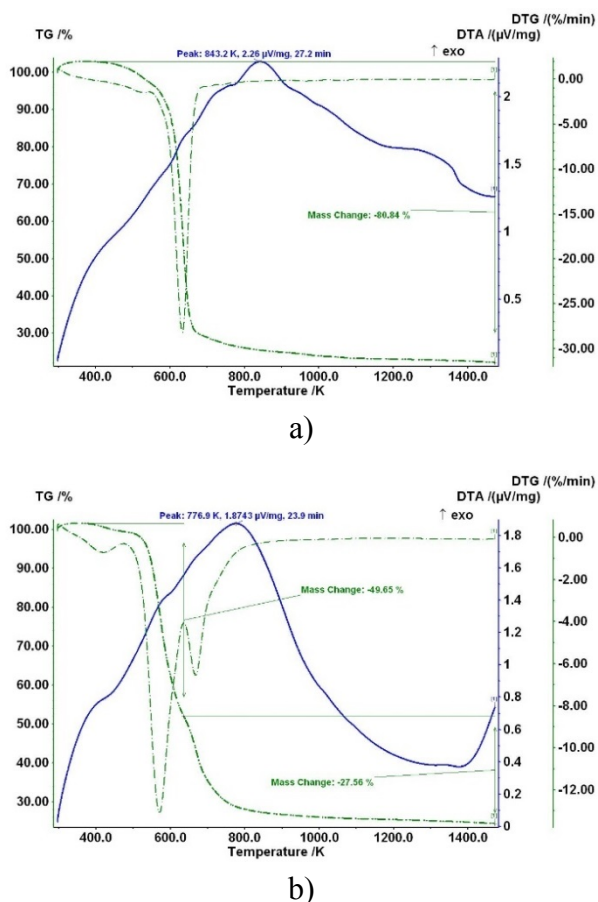


Figure 3. DTA/TG/DTG of cigarette butts (a) and waste coffee grounds (b)

Table 3. Standard consistency and plasticity

Additive [%]	Standard consistency [%]		Pfefferkorn plasticity [%]	
	Cigarette butts	Waste coffee grounds	Cigarette butts	Waste coffee grounds
0	25.7	25.7	25.51	25.51
5	30.4	28.8	33.0	27.55
10	34.0	32.4	40.78	30.32

Table 4. Mass loss and shrinkage

Additive [%]	Mass loss [%]				Shrinkage [%]			
	Drying		Firing		Drying		Firing	
	Cigarette butts	Waste coffee grounds	Cigarette butts	Waste coffee grounds	Cigarette butts	Waste coffee grounds	Cigarette butts	Waste coffee grounds
0	20.60	20.60	6.33	6.33	4.73	4.73	1.62	1.62
5	23.73	22.82	10.87	10.86	3.82	4.46	0.86	0.9
10	26.34	24.26	15.01	14.57	3.32	3.72	0.62	0.54

It should be borne in mind that particles of additives used are highly porous (Figure 4) and absorb a high amount of water leaving less water available for clay particles lubrication which is decisive for clay plasticity. The effect of organic residues on drying shrinkage is explained in the same way. The porous and absorbent nature of the additives particles and fibres stabilizes the drying behaviour of the clay despite the increase in water demand with the addition of organic residues. In clay mixture without additives, the distance between the particles is reduced as water molecules leave the clay during drying process, so that the clay body undergoes significant shrinkage. On the other hand, clay mixtures containing porous particles and fibres lose water during drying process, but a substantial part of evaporated water is contained in particles of additives. This results in decreasing the shrinkage by increasing the percentage of the additives (Table 4) and it is a very favourable effect as it reduces clay sensitivity on drying process and possibility of cracking. In this way it is possible to reduce drying time and save energy.

Table 5 presents effect of the waste content on water absorption and apparent porosity and density. In Table 6, flexural and compressive strength are presented, and in Table 7 thermal conductivity and refractoriness.



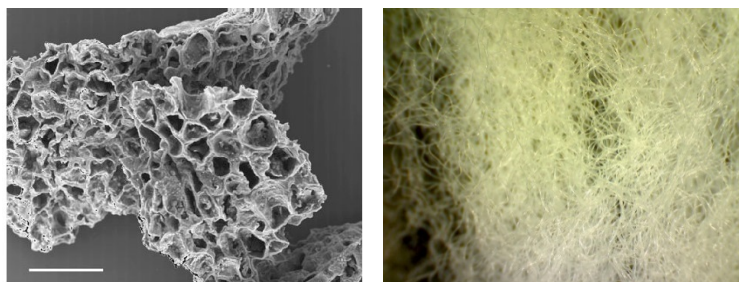


Figure 4. SEM image of waste coffee grounds (bar = 100 μm) [26] (left) and filter of cigarette recorded on PCE -MM200 microscope at 12.5x magnification (right)

Table 5. Apparent porosity, water absorption and apparent density

Additive [%]	Apparent porosity [%]		Water absorption [%]		Apparent density [g/cm <sup>3</sup> ]	
	Cigarette butts	Waste coffee grounds	Cigarette butts	Waste coffee grounds	Cigarette butts	Waste coffee grounds
0	27.21	27.12	15.64	15.64	1.74	1.74
5	36.57	34.91	25.07	23.49	1.47	1.49
10	42.84	42.13	33.88	31.2	1.26	1.28

Table 6. Flexural and compressive strength

Additive [%]	Flexural strength [MPa]		Compressive strength [MPa]	
	Cigarette butts	Waste coffee grounds	Cigarette butts	Waste coffee grounds
0	4.2	4.2	21.1	21.1
5	2.5	2.7	10.7	12.8
10	1.6	2.2	4.7	5.5

Table 7. Thermal conductivity and refractoriness

Additive [%]	Thermal conductivity [W/mK]		Refractoriness [K]	
	Cigarette butts	Waste coffee grounds	Cigarette butts	Waste coffee grounds
0	0.5	0.5	1438	1438
5	0.41	0.45	1398	1438
10	0.34	0.38	1373	1398

Increasing the content of the additives increases the mass loss on firing (Table 4), because the additives mainly transform to the gaseous phase in the firing process, creating a porous structure. This porosity decreases apparent density and mechanical strength while increases water absorption (Tables 5 and 6). The effect is more pronounced in the

mixtures with the cigarette butts. The specimens with a higher porosity are lighter (Figure 5). That can be considered as positive effect for the transport, handling and particularly for the installation of the bricks. Due to the increased porosity, the flexural and compressive strength decrease but are still acceptable according to clay brick requirements [12]. The results shown in Table 7 indicate that the addition of the additives reduces thermal conductivity and slightly decreases refractoriness. Lower thermal conductivity is desirable because it will reduce the energy required for heating and cooling of buildings.

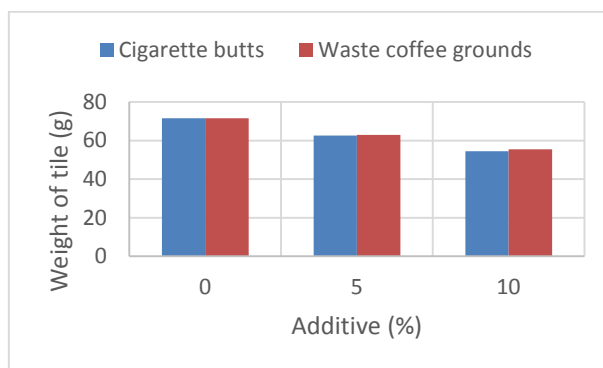


Figure 5. Weight changes of fired tiles

From optical microscope images in Figure 6 it can be seen that the addition of the cigarette butts changes structure considerably, while the addition of the waste coffee grounds gives porous texture but the structure remains homogeneous. Larger, elongated or eyelash

pores and significant inhomogeneity of the structure are observed in the samples with the cigarette butts, which is why the strength of these samples is lower in comparison to the samples with the waste coffee grounds.

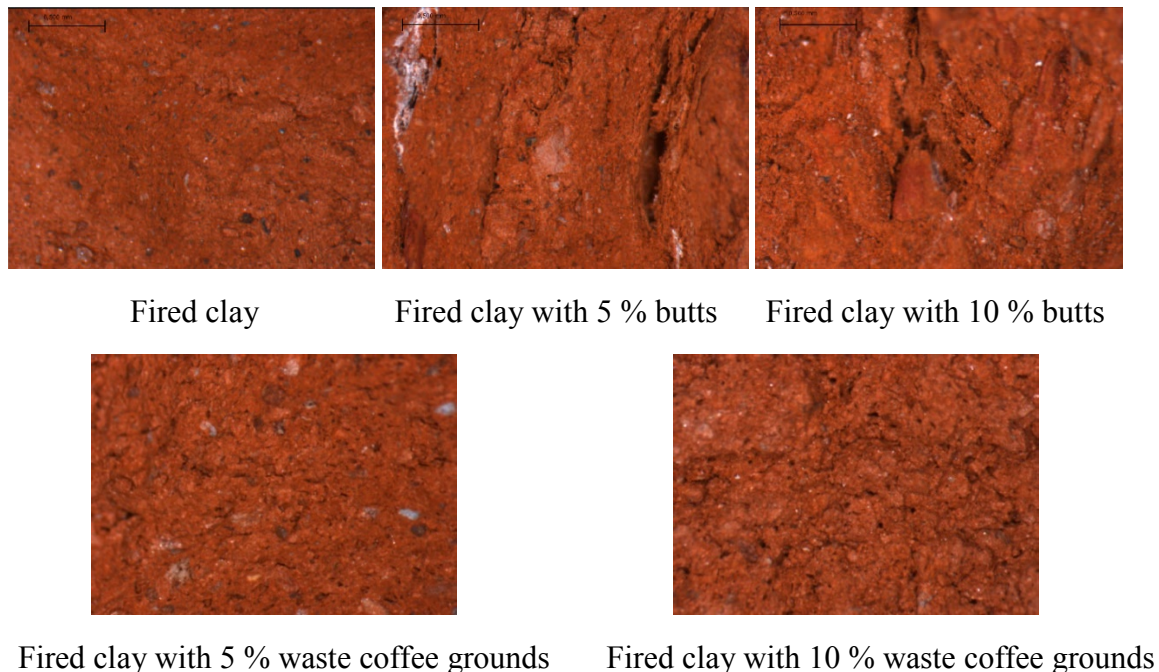


Figure 6. Optical microscopy images of fired clay and fired clay with additives

## CONCLUSION

Based on the examination it can be concluded that the cigarette butts and the waste coffee grounds can be added to the brick clay from the "Čavka" deposit in the amount of 10 wt.%, while mechanical strength remains within the limits prescribed by standards. Moreover, the additives advantageously affect the drying process of the clay and their addition can provide lighter products with improved insulation properties. In this way it is possible to dispose a larger amount of the waste material and thus deal with this growing ecological problem. At the same time, a better-quality product can be obtained that will enable greater energy efficiency in the production and application of clay bricks.

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