

# Analysis of Low-Power Steam Turbine With One Extraction for Marine Applications

## Analiza parne turbine male snage s jednim oduzimanjem pare za primjenu u pomorstvu

Vedran Medica-Viola

University of Rijeka  
Faculty of Engineering  
e-mail: vmedica@riteh.hr

Vedran Mrzljak

University of Rijeka  
Faculty of Engineering  
e-mail: vedran.mrzljak@riteh.hr

Nikola Anđelić

University of Rijeka  
Faculty of Engineering  
e-mail: nandelic@riteh.hr

Maro Jelić

University of Dubrovnik  
Maritime Department  
e-mail: maro.jelic@unidu.hr

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### Summary

The paper presents thermodynamic (energy and exergy) analysis of low-power steam turbine with one extraction for marine applications. Analyzed steam turbine is divided in two parts - High Pressure (HP) part before steam extraction and Low Pressure (LP) part after steam extraction. Analysis shows that HP turbine part produces the majority of cumulative turbine power and consequentially has higher mechanical, energy and exergy losses when compared to LP turbine part. Regardless of heavier operating conditions, LP turbine part has higher efficiencies and lower specific losses (in both energy and exergy analysis) when compared to HP turbine part. Whole analyzed turbine has energy and exergy efficiencies equal to 62.84% and 65.58%, while energy and exergy turbine losses are 696.74 kW and 618.50 kW. Cumulative produced power at the turbine shaft outlet is equal to 1178.40 kW. Steam extraction which divides analyzed turbine on HP and LP part can deliver a notable amount of heat to any marine heat consumer, what represents a significant advantage of observed turbine in comparison with similar low-power marine steam turbines which usually does not have steam extractions.

### KEY WORDS

steam turbine  
low-power  
steam extraction  
marine applications  
thermodynamic analysis

### Sažetak

*Uradu je prikazana termodinamička (energijska i eksergijska) analiza parne turbine male snage s jednim oduzimanjem pare za primjenu u pomorstvu. Analizirana parna turbina podijeljena je u dva dijela - visokotlačni dio (HP) prije oduzimanja pare i niskotlačni dio (LP) nakon oduzimanja pare. Analiza pokazuje da visokotlačni dio proizvodi većinu snage turbine i posljedično ima veće mehaničke, energijske i eksergijske gubitke u usporedbi s niskotlačnim dijelom turbine. Bez obzira na teže radne uvjete, niskotlačni dio turbine ima veću učinkovitost i manje specifične gubitke (u energijskoj i eksergijskoj analizi) u usporedbi s visokotlačnim dijelom turbine. Cijela analizirana turbina ima energijsku i eksergijsku učinkovitost jednaku 62.84 % i 65.58 %, dok su gubici energije i eksergije turbine 696.74 kW i 618.50 kW. Kumulativna proizvedena snaga na izlazu turbinskog vratila jednaka je 1178.40 kW. Oduzimanjem pare kojim se analizirana turbina dijeli na visokotlačni i niskotlačni dio može se isporučiti značajna količina topline bilo kojem potrošaču topline u pomorskoj industriji, što predstavlja značajnu prednost promatrane turbine u usporedbi sa sličnim brodskim parnim turbinama male snage koje obično nemaju oduzimanje pare.*

### KLJUČNE RIJEČI

parna turbina  
mala snaga  
oduzimanje pare  
primjena u pomorstvu  
termodinamička analiza

## 1. INTRODUCTION / Uvod

Steam turbines are widely used components in power plants for electricity production all over the world [1, 2]. Such steam turbines are high-power, complex components which consist of several cylinders and a number of turbine stages in each cylinder [3, 4]. Small, low-power steam turbines are often used in such power plants for the drive of several power consumers, e.g. water pumps [5].

In marine applications, steam turbines can be used in various combinations and in various systems. The most common usage of steam turbines in marine applications is in the engine rooms

of the LNG (Liquefied Natural Gas) carriers, which still has the steam propulsion system as a dominant one [6, 7]. In such marine steam propulsion system all of the steam turbines (main turbine and auxiliary) are low-power turbines (main turbine maximum power usually did not exceed 30 MW, while auxiliary turbines maximum power usually did not exceed 5-6 MW) [8, 9]. Auxiliary low-power steam turbines in such marine systems (turbo-generators for the electricity generator drive or steam turbines for water pumps drive) are simple steam turbines without steam extractions [10].

Several steam turbine producers in their catalogues offer low-power steam turbines for marine applications which have at least one steam extraction in order to ensure simultaneous power and heat production [11]. One of such low-power steam turbine, which has one steam extraction and is made for the usage in the marine applications, is analyzed in this paper. Thermodynamic (energy and exergy) analysis of steam turbine is performed, based on operating parameters provided by the producer.

Analyzed low-power steam turbine is divided in two parts - High Pressure (HP) part before steam extraction and Low Pressure (LP) part after steam extraction. Thermodynamic analysis is performed for each turbine part independently as well as for the whole turbine. Mechanical losses of each turbine part as well as of the whole turbine are included in the analysis. It is concluded that LP part produces less power in comparison with HP part, but has notable higher efficiencies and lower losses (from both the energy and exergy point of view). Energy and exergy flow streams throughout each turbine part and the whole turbine are also presented and discussed.

## 2. DESCRIPTION AND OPERATING CHARACTERISTICS OF THE ANALYZED LOW-POWER STEAM TURBINE WITH ONE EXTRACTION / Opis i radne značajke analizirane parne turbine male snage s jednim oduzimanjem pare

Analyzed low-power steam turbine consists of two parts - the first is High Pressure (HP) part between steam entrance into the turbine and steam extraction, while Low Pressure (LP) part can be seen between steam extraction and steam outlet from the turbine (condenser inlet), Fig. 1. Steam produced in steam generator [12] expanded firstly in HP part of the turbine, after which follows steam extraction. Extracted steam can be led to any marine heat consumer. Remaining steam mass flow rate expanded through LP part of the turbine and after expansion is led to the main marine steam condenser, which is usually shell and tube type heat exchanger [13].

Steam turbine analyzed in this paper and presented in Fig. 1 drives electricity generator with the necessary usage of gearbox which reduces turbine revolutions and ensures proper drive of any power consumer (not necessary electricity generator only). Thermodynamic analysis of this steam turbine is based on steam expansion processes - real (polytropic) expansion process whose description requires turbine operating points presented in Fig. 1

and ideal (isentropic) steam expansion process whose description requires assumption of constant steam specific entropy during the expansion process [14].

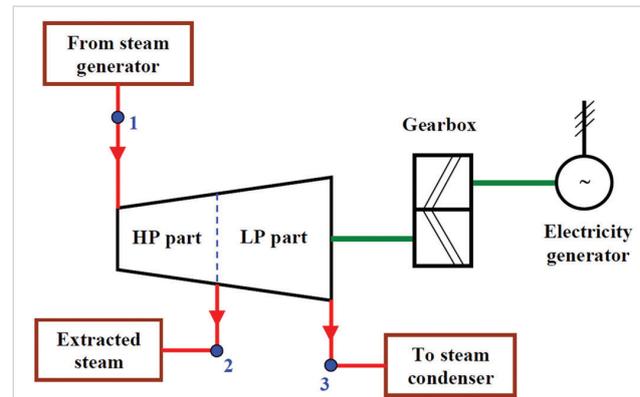


Figure 1 General scheme of the analyzed low-power steam turbine with marked operating points

Slika 1. Opća shema analizirane parne turbine male snage s označenim radnim točkama

As analysis in this paper is performed not only for the entire steam turbine, but also for each turbine part, energy analysis requires comparison of real (polytropic) and ideal (isentropic) steam expansion processes for each turbine part. Expansion processes (ideal and real) of each analyzed steam turbine part begin at the same steam pressure and finished at the same steam pressure. Therefore, for the HP part of the analyzed turbine the ideal steam expansion process (points 1-2<sub>is</sub>, Fig. 2) is compared with real steam expansion process (points 1-2, Fig. 2), while for the LP part of the analyzed turbine the ideal steam expansion process (points 2-3<sub>is</sub>, Fig. 2) is compared with real steam expansion process (points 2-3, Fig. 2) in order to be able to perform complete energy analysis of the entire turbine and both of its parts.

Exergy analysis of presented steam turbine (or any other steam turbine [15]) is based on real (polytropic) steam expansion process (points 1-2-3 in Fig. 2), which is also valid in exergy analysis of each turbine part.

From Fig. 2 can be observed that the majority of real steam expansion process through the analyzed turbine is in the superheated steam area, while only the last section of LP turbine part falls under the steam saturation line.

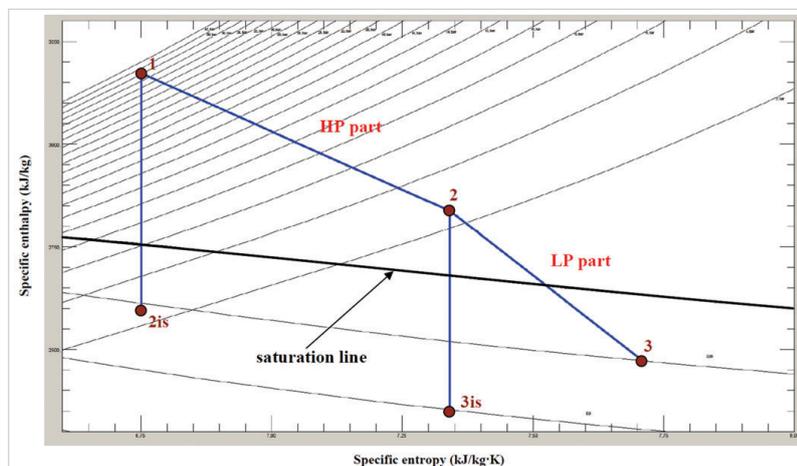


Figure 2 Ideal (isentropic) and real (polytropic) steam expansion through the analyzed turbine presented in h-s diagram - plotted from [16]

Slika 2. Idealna (izentropna) i stvarna (politropska) ekspanzija pare kroz analizanu turbinu prikazanu u h-s dijagramu - nacrtanom iz [16]

### 3. STEAM TURBINE THERMODYNAMIC ANALYSIS / Termodinamička analiza parne turbine

#### 3.1. General equations for the thermodynamic analysis of any control volume or system / Opće jednadžbe za termodinamičku analizu bilo kojeg kontrolnog volumena ili sustava

Thermodynamic analysis (energy and exergy analysis) of any control volume or system is based on the first and the second law of thermodynamics. The first law of thermodynamics defines energy analysis [17], which is independent of the environment in which analyzed control volume or a system operates [18]. On the other side, exergy analysis of any control volume or system is based on the second law of thermodynamics [19] and it takes into account the parameters of the ambient in which control volume or a system operates [20].

Mass flow rate balance for any control volume or system in steady state, when the mass flow rate leakage did not occur, is [21]:

$$\sum \dot{m}_{in} = \sum \dot{m}_{out} \quad (1)$$

Disregarding potential and kinetic energy, the energy balance of a control volume or system can be defined, according to [22, 23], by using the following equation:

$$\sum \dot{m}_{in} \cdot h_{in} - \sum \dot{m}_{out} \cdot h_{out} + \dot{Q} - P = 0 \quad (2)$$

Any fluid flow has a certain amount of energy which can be defined as [24, 25]:

$$\dot{E}_{en} = \dot{m} \cdot h \quad (3)$$

The overall definition of any control volume or system energy efficiency, according to [26, 27] is:

$$\eta_{en} = \frac{\text{Energy output (Energy outlet)}}{\text{Energy input (Energy inlet)}} \quad (4)$$

Disregarding potential and kinetic energy, the exergy balance of a control volume or system can be defined, according to [28, 29], by using the following equation:

$$\sum \dot{m}_{in} \cdot \varepsilon_{in} - \sum \dot{m}_{out} \cdot \varepsilon_{out} + \dot{X}_{heat} - P - \dot{E}_{ex,loss} = 0 \quad (5)$$

In the Eq. 5,  $\varepsilon$  is specific exergy, which is defined as [30, 31]:

$$\varepsilon = (h - h_0) - T_0 \cdot (s - s_0) \quad (6)$$

while  $\dot{X}_{heat}$  is the net exergy transfer by heat (at temperature  $T$ ), which is defined, according to [32, 33], as:

$$\dot{X}_{heat} = \sum (1 - \frac{T_0}{T}) \cdot \dot{Q} \quad (7)$$

Amount of exergy for any fluid flow can be defined according to [34, 35] as follows:

$$\dot{E}_{ex} = \dot{m} \cdot \varepsilon = \dot{m} \cdot [(h - h_0) - T_0 \cdot (s - s_0)] \quad (8)$$

The overall definition of any control volume or system exergy efficiency, according to [36, 37] is:

$$\eta_{ex} = \frac{\text{Exergy output (Exergy outlet)}}{\text{Exergy input (Exergy inlet)}} \quad (9)$$

#### 3.2. Analysis of low-power steam turbine with one extraction for marine applications / Analiza parne turbine male snage s jednim oduzimanjem za primjenu u pomorstvu

Thermodynamic (energy and exergy) analysis of low-power steam turbine with one extraction for marine applications (along with the analysis of each turbine part) is performed by using turbine operating points presented in Fig. 1 and Fig. 2. The

mechanical efficiency of the whole turbine and both of its parts is assumed to be 95% (according to data from [38, 39]).

#### 3.2.1. Low-power steam turbine with one extraction energy analysis / Energijska analiza parne turbine male snage s jednim oduzimanjem

Real (polytropic) developed power of each turbine part and the whole turbine is:

$$- \text{HP part:} \quad P_{re,HP} = \dot{m}_1 \cdot (h_1 - h_2) \cdot \eta_{mech} \quad (10)$$

$$- \text{LP part:} \quad P_{re,LP} = (\dot{m}_1 - \dot{m}_2) \cdot (h_2 - h_3) \cdot \eta_{mech} \quad (11)$$

$$- \text{Whole turbine:} \quad P_{re,WT} = P_{re,HP} + P_{re,LP} = [\dot{m}_1 \cdot (h_1 - h_2) + (\dot{m}_1 - \dot{m}_2) \cdot (h_2 - h_3)] \cdot \eta_{mech} \quad (12)$$

Mechanical losses of each turbine part and the whole turbine are calculated in accordance with real (polytropic) developed power:

$$- \text{HP part:} \quad \dot{E}_{mech,loss,HP} = \dot{m}_1 \cdot (h_1 - h_2) \cdot (1 - \eta_{mech}) \quad (13)$$

$$- \text{LP part:} \quad \dot{E}_{mech,loss,LP} = (\dot{m}_1 - \dot{m}_2) \cdot (h_2 - h_3) \cdot (1 - \eta_{mech}) \quad (14)$$

$$- \text{Whole turbine:} \quad \dot{E}_{mech,loss,WT} = [\dot{m}_1 \cdot (h_1 - h_2) + (\dot{m}_1 - \dot{m}_2) \cdot (h_2 - h_3)] \cdot (1 - \eta_{mech}) \quad (15)$$

Ideal (isentropic) power of each turbine part and the whole turbine is:

$$- \text{HP part:} \quad P_{is,HP} = \dot{m}_1 \cdot (h_1 - h_{2is}) \cdot \eta_{mech} \quad (16)$$

$$- \text{LP part:} \quad P_{is,LP} = (\dot{m}_1 - \dot{m}_2) \cdot (h_2 - h_{3is}) \cdot \eta_{mech} \quad (17)$$

$$- \text{Whole turbine:} \quad P_{is,WT} = P_{is,HP} + P_{is,LP} = [\dot{m}_1 \cdot (h_1 - h_{2is}) + (\dot{m}_1 - \dot{m}_2) \cdot (h_2 - h_{3is})] \cdot \eta_{mech} \quad (18)$$

Energy losses of each turbine part and the whole turbine are calculated as a difference between the ideal (isentropic) and real (polytropic) power:

$$- \text{HP part:} \quad \dot{E}_{en,loss,HP} = P_{is,HP} - P_{re,HP} = [\dot{m}_1 \cdot (h_1 - h_{2is}) - \dot{m}_1 \cdot (h_1 - h_2)] \cdot \eta_{mech} \quad (19)$$

$$- \text{LP part:} \quad \dot{E}_{en,loss,LP} = P_{is,LP} - P_{re,LP} = [(\dot{m}_1 - \dot{m}_2) \cdot (h_2 - h_{3is}) - (\dot{m}_1 - \dot{m}_2) \cdot (h_2 - h_3)] \cdot \eta_{mech} \quad (20)$$

$$- \text{Whole turbine:} \quad \dot{E}_{en,loss,WT} = P_{is,WT} - P_{re,WT} = \dot{E}_{en,loss,HP} + \dot{E}_{en,loss,LP} \quad (21)$$

Energy efficiencies of each turbine part and the whole turbine are calculated as a ratio between real (polytropic) and ideal (isentropic) power:

$$- \text{HP part:} \quad \eta_{en,HP} = \frac{P_{re,HP}}{P_{is,HP}} = \frac{\dot{m}_1 \cdot (h_1 - h_2) \cdot \eta_{mech}}{\dot{m}_1 \cdot (h_1 - h_{2is}) \cdot \eta_{mech}} = \frac{(h_1 - h_2)}{(h_1 - h_{2is})} \quad (22)$$

$$- \text{LP part:} \quad \eta_{en,LP} = \frac{P_{re,LP}}{P_{is,LP}} = \frac{(\dot{m}_1 - \dot{m}_2) \cdot (h_2 - h_3) \cdot \eta_{mech}}{(\dot{m}_1 - \dot{m}_2) \cdot (h_2 - h_{3is}) \cdot \eta_{mech}} = \frac{(h_2 - h_3)}{(h_2 - h_{3is})} \quad (23)$$

$$- \text{Whole turbine:} \quad \eta_{en,WT} = \frac{P_{re,WT}}{P_{is,WT}} = \frac{P_{re,HP} + P_{re,LP}}{P_{is,HP} + P_{is,LP}} \quad (24)$$

Specific energy losses of each turbine part and the whole turbine are calculated as a ratio between energy loss and real (polytropic) power:

$$- \text{HP part:} \quad \dot{E}_{en,specific,HP} = \frac{\dot{E}_{en,loss,HP}}{P_{re,HP}} = \frac{P_{is,HP} - P_{re,HP}}{P_{re,HP}} = \frac{P_{is,HP}}{P_{re,HP}} - 1 \quad (25)$$

- LP part:

$$\dot{E}_{\text{en,specific,LP}} = \frac{\dot{E}_{\text{en,loss,LP}}}{P_{\text{re,LP}}} = \frac{P_{\text{is,LP}} - P_{\text{re,LP}}}{P_{\text{re,LP}}} = \frac{P_{\text{is,LP}}}{P_{\text{re,LP}}} - 1 \quad (26)$$

- Whole turbine:

$$\dot{E}_{\text{en,specific,WT}} = \frac{\dot{E}_{\text{en,loss,WT}}}{P_{\text{re,WT}}} = \frac{P_{\text{is,WT}} - P_{\text{re,WT}}}{P_{\text{re,WT}}} = \frac{P_{\text{is,WT}}}{P_{\text{re,WT}}} - 1 \quad (27)$$

### 3.2.2. Low-power steam turbine with one extraction exergy analysis / Eksergijska analiza parne turbine male snage s jednim oduzimanjem

Exergy losses (exergy destructions) of each turbine part and the whole turbine are calculated as:

- HP part:

$$\dot{E}_{\text{ex,loss,HP}} = \dot{m}_1 \cdot \varepsilon_1 - \dot{m}_1 \cdot \varepsilon_2 - P_{\text{re,HP}} \quad (28)$$

- LP part:

$$\begin{aligned} \dot{E}_{\text{ex,loss,LP}} &= (\dot{m}_1 - \dot{m}_2) \cdot \varepsilon_2 - (\dot{m}_1 - \dot{m}_2) \cdot \varepsilon_3 - P_{\text{re,LP}} = \\ &= \dot{m}_3 \cdot \varepsilon_2 - \dot{m}_3 \cdot \varepsilon_3 - P_{\text{re,LP}} \end{aligned} \quad (29)$$

- Whole turbine:

$$\dot{E}_{\text{ex,loss,WT}} = \dot{m}_1 \cdot \varepsilon_1 - \dot{m}_2 \cdot \varepsilon_2 - \dot{m}_3 \cdot \varepsilon_3 - P_{\text{re,WT}} \quad (30)$$

Exergy efficiencies of each turbine part and the whole turbine are:

- HP part:

$$\eta_{\text{ex,HP}} = \frac{P_{\text{re,HP}}}{\dot{m}_1 \cdot \varepsilon_1 - \dot{m}_1 \cdot \varepsilon_2} \quad (31)$$

- LP part:

$$\eta_{\text{ex,LP}} = \frac{P_{\text{re,LP}}}{(\dot{m}_1 - \dot{m}_2) \cdot \varepsilon_2 - (\dot{m}_1 - \dot{m}_2) \cdot \varepsilon_3} = \frac{P_{\text{re,LP}}}{\dot{m}_3 \cdot \varepsilon_2 - \dot{m}_3 \cdot \varepsilon_3} \quad (32)$$

- Whole turbine:

$$\eta_{\text{ex,WT}} = \frac{P_{\text{re,WT}}}{\dot{m}_1 \cdot \varepsilon_1 - \dot{m}_2 \cdot \varepsilon_2 - \dot{m}_3 \cdot \varepsilon_3} \quad (33)$$

Specific exergy losses (specific exergy destructions) of each turbine part and the whole turbine are calculated as:

- HP part:

$$\dot{E}_{\text{ex,specific,HP}} = \frac{\dot{E}_{\text{ex,loss,HP}}}{P_{\text{re,HP}}} \quad (34)$$

- LP part:

$$\dot{E}_{\text{ex,specific,LP}} = \frac{\dot{E}_{\text{ex,loss,LP}}}{P_{\text{re,LP}}} \quad (35)$$

- Whole turbine:

$$\dot{E}_{\text{ex,specific,WT}} = \frac{\dot{E}_{\text{ex,loss,WT}}}{P_{\text{re,WT}}} \quad (36)$$

## 4. OPERATING PARAMETERS OF LOW-POWER STEAM TURBINE WITH ONE EXTRACTION / Radni parametri parne turbine male snage s jednim oduzimanjem

Thermodynamic (energy and exergy) analysis requires knowledge of steam operating parameters (temperature, pressure and mass flow rate) at each turbine operating point presented in Fig. 1. Those operating parameters are found in the analyzed steam turbine producer catalogue and presented in Table 1. Steam specific enthalpy, specific entropy and specific exergy at the same turbine operating points were calculated by using NIST-REFPROP 9.0 software [16].

It should be noted that steam specific enthalpy after ideal (isentropic) expansion in HP turbine part (operating point 2is, Fig. 2) is calculated also with NIST-REFPROP 9.0 software [16] by using steam pressure at the HP turbine part outlet and the same steam specific entropy as at the HP turbine part inlet (operating point 1, Fig. 2). The identical procedure is used for calculation of steam specific enthalpy after ideal (isentropic) expansion in LP turbine part. The same calculation procedure can be found in the literature, applied during the energy analyses of other steam turbines [40, 41].

Specific exergies in each turbine operating point (presented in Table 1) are calculated for the base ambient state (the base ambient conditions) which is in this paper taken as proposed in [42]:

- pressure:  $p_0 = 100 \text{ kPa} = 1 \text{ bar}$ ,
- temperature:  $T_0 = 298 \text{ K} = 25 \text{ }^\circ\text{C}$ .

Steam turbine producer for defined operating parameters in Table 1 specifies an electricity generator driving power of 1100 kW. This power also includes losses in the gearbox and in electricity generator, Fig. 1. Therefore, produced power at the turbine outlet shaft should be higher than the specified value for mentioned losses.

## 5. THE RESULTS OF LOW-POWER STEAM TURBINE WITH ONE EXTRACTION ANALYSIS AND DISCUSSION / Rezultati analize i rasprava o parnoj turbini male snage s jednim oduzimanjem

### 5.1. The results of energy analysis / Rezultati energijske analize

The results of low-power steam turbine energy analysis showed that the majority of real (polytropic) turbine power is produced in HP turbine part (66.10%) while LP turbine part produces

Table 1 Steam operating parameters at each operating point of observed turbine  
Tablica 1. Radni parametri pare u svakoj radnoj točki promatrane turbine

Operating point*	Temperature (°C)	Pressure (bar)	Mass flow rate (t/h)	Specific enthalpy (kJ/kg)	Specific entropy (kJ/kg·K)	Specific exergy (kJ/kg)
1	379.6	36.34	8.80	3172.9	6.7505	1164.8
2	184.8	2.47	4.66	2837.5	7.3405	653.5
3	49.8	0.1223	4.14	2471.8	7.7095	177.8

\* According to Fig. 1.

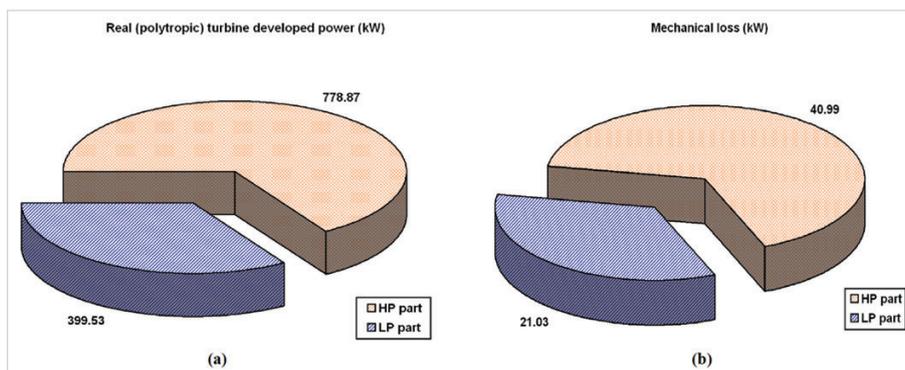


Figure 3 Analyzed turbine: (a) Real (polytropic) developed power; (b) Mechanical loss  
 Slika 3. Analizirana turbina: (a) Stvarna (politropska) razvijena snaga; (b) Mehanički gubitak

only 33.90% of real cumulative power, Fig. 3 (a). For the steam operating parameters specified by turbine producer and presented in Table 1, cumulative real (polytropic) developed power at the turbine shaft outlet is equal to 1178.40 kW. This turbine power is calculated by using Eq. 12, which takes into account mechanical losses in both turbine parts.

The accuracy of calculated real developed power at the turbine shaft outlet (1178.40 kW), along with used assumption for mechanical losses inside both turbine parts, can be easily validated. If this power is reduced for losses in the gearbox (according to [38] gearbox efficiency can be taken between 95% and 96%) and for losses in the electricity generator (according to [39] electricity generator efficiency is around 98%), Fig. 1, electricity generator driving power will be around 1100 kW, as specified by turbine producer.

Identical to turbine real developed power, the majority of turbine mechanical losses appears in HP turbine part (Fig. 3 (b)), while the mechanical losses of the whole turbine are equal to 62.02 kW.

Ideal (isentropic) power of the whole analyzed steam turbine is calculated by using Eq. 18 and is equal to 1875.14

kW. The majority of ideal power of the whole turbine (71.75%) refers to the HP turbine part, while only 28.25% refers to the LP turbine part, Fig. 4 (a).

Energy losses of each turbine part and whole turbine are calculated by using Eq. 19 - Eq. 21 and presented in Fig. 4 (b). Energy loss of the whole turbine is equal to 696.74 kW and the highest amount of that loss (81.33%) refers to the HP turbine part. It is interesting to observe this fact, because LP turbine part operates in much heavier conditions when compared to HP part (last stages of LP turbine part operates with wet steam which, due to water droplets, increases inner losses). However, HP turbine part has much higher energy loss (in comparison to LP part) due to significantly higher steam mass flow rate.

Energy losses of steam turbines or its parts are reverse proportional to turbine (or its parts) energy efficiencies [10]. The same conclusion can be obtained when compared Fig. 4 (b) and Fig. 5. LP part of the analyzed steam turbine has an energy efficiency of 75.43% - much higher in comparison to the HP turbine part which energy efficiency equals 57.89%. The energy efficiency of the whole turbine is 62.84%, what is expected for low-power steam turbines [43, 44].

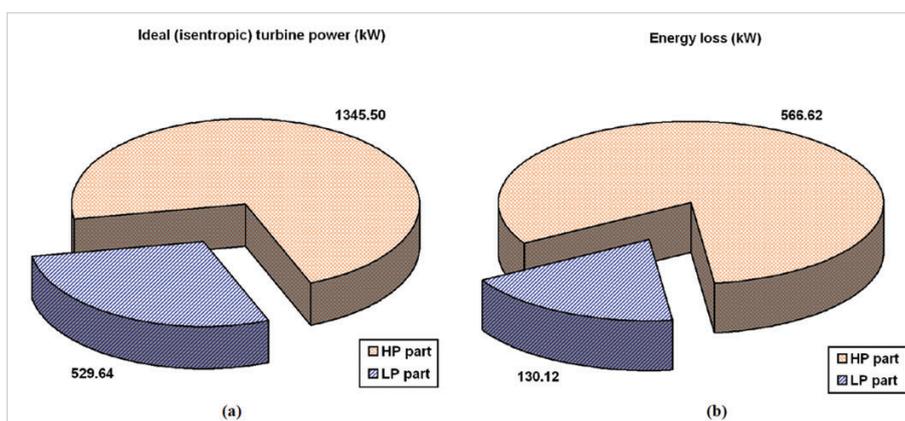


Figure 4 Analyzed turbine: (a) Ideal (isentropic) power; (b) Energy loss  
 Slika 4. Analizirana turbina: (a) Idealna (izentropska) snaga; (b) Gubitak energije

Specific energy loss of the steam turbine or any of its parts is defined by using the same methodology as for specific fuel consumption, which is commonly used parameter for tracking the internal combustion engine process [45]. Specific energy loss of steam turbine or each turbine part is obtained by dividing of energy loss with real developed power (for the whole turbine as well as for each turbine part, Eq. 25 - Eq. 27). Specific energy loss presents which part in the real developed power takes an energy loss (for the whole turbine or each of it parts). From Fig. 5 can be seen that specific energy loss of HP turbine part has a share of 72.75% in real developed power of this turbine part. The same parameter for the LP turbine part is equal to 32.57% and for the whole turbine is equal to 59.13%.

Regardless of worse operating conditions (wet steam, high steam volume and speed), from Fig. 5 it can be seen that LP part of the analyzed turbine has much higher energy efficiency and much lower specific energy loss in comparison with the HP turbine part.

Energy flow streams of the analyzed steam turbine (turbine real developed power and steam flow streams), presented in Fig. 6 are calculated by using general equations (Eq. 1 - Eq. 4) and Eq. 10 - Eq. 27 as well as steam operating parameters from Table 1. It should be noted that analyzed turbine parts (HP part and LP part) are separated in Fig. 6 in order to present energy flow streams of each turbine part and of the whole turbine.

Real (polytropic) produced power of the whole turbine (of the both turbine parts) is 1240.42 kW and it is reduced for

mechanical losses of both turbine parts (62.02 kW), therefore power which can be used for power consumer drive (power at the turbine shaft outlet) is equal to 1178.40 kW, Fig. 6.

While presenting energy flow streams of the analyzed steam turbine (or any other steam turbine), energy balance equation (Eq. 2) considered only mechanical losses of each turbine part (and cumulative mechanical losses of the whole turbine) as the real steam turbine energy dissipation parameters.

In comparison with energy analysis, exergy analysis of the same steam turbine will take into account additional losses of steam (along with mechanical losses). Such steam losses (steam exergy destruction) are caused by taking into account parameters of the ambient (pressure and temperature) in which analyzed turbine operates. The energy analysis did not take into account the parameters of the ambient; therefore additional steam energy losses did not occur [46].

It should be noted that, due to the lack of data, steam mass flow rates lost on the front and rear gland seals of the analyzed turbine are not taken into account in this analysis. It can be assumed that the cumulative mass flow rate lost on both turbine gland seals (front and rear) is approximately equal to 1% of the steam mass flow rate which enters in the analyzed turbine [47, 48].

## 5.2. The results of exergy analysis / Rezultati eksergijske analize

Exergy losses (exergy destructions) of the whole turbine and each turbine part are calculated by using Eq. 28 - Eq. 30. Similar

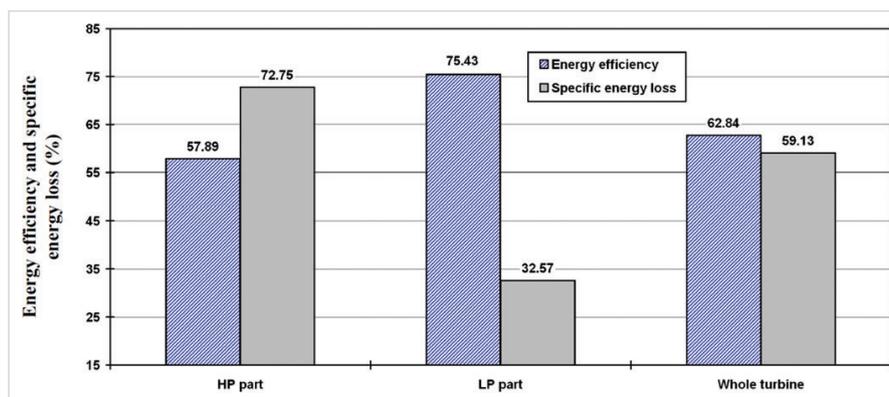


Figure 5 Energy efficiency and specific energy loss of the analyzed steam turbine and its parts  
Slika 5. Energetska učinkovitost i specifični gubitak energije analizirane parne turbine i njezinih dijelova

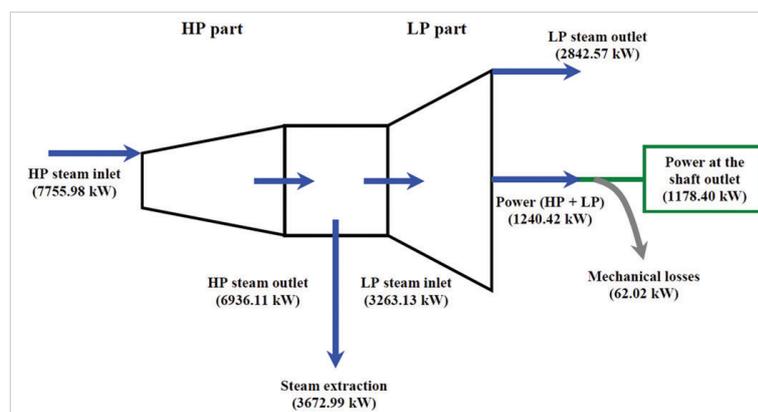


Figure 6 Energy flow streams (steam and power) throughout the analyzed steam turbine  
Slika 6. Struje protoka energije (para i snaga) kroz analiziranu parnu turbinu

to energy losses, exergy loss of HP turbine part takes a share of 76.15% in cumulative exergy loss of the whole turbine. Therefore, LP turbine part share in the cumulative exergy loss of the whole turbine is only 23.85%, Fig. 7. As can be seen from Fig. 7, cumulative exergy loss (cumulative exergy destruction) of the whole turbine is equal to 618.50 kW, and it consists of steam exergy destruction and mechanical losses of both turbine parts (HP and LP part).

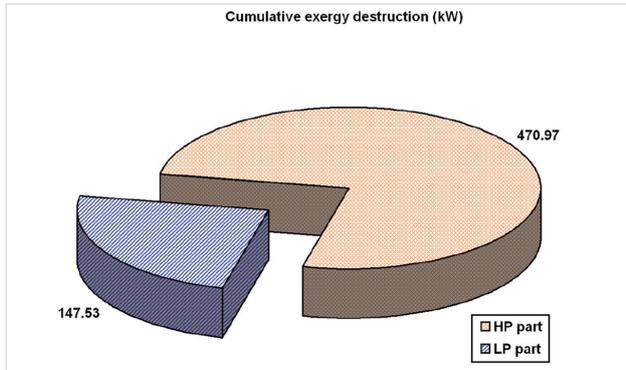


Figure 7 Cumulative exergy destruction of the analyzed steam turbine  
Slika 7. Kumulativni eksrgerijski gubitak analizirane parne turbine

The exergy efficiency of the analyzed steam turbine and both of its parts have the same trend as energy efficiency - Fig. 5 and Fig. 8. LP turbine part has significantly higher exergy efficiency (73.03%) in comparison with the HP turbine part (62.32%), while the whole turbine exergy efficiency is equal to 65.58%, Fig. 8. LP turbine part has lower exergy than energy efficiency, while the

exergy efficiencies of HP turbine part and the whole turbine are higher in comparison with energy efficiencies, Fig. 5 and Fig. 8.

Specific exergy destruction (specific exergy loss) of the whole turbine and each turbine part is calculated by using Eq. 34 - Eq. 36 and is obtained by dividing of exergy loss (exergy destruction) with real developed power. Specific exergy destruction of HP turbine part is much higher in comparison with the LP turbine part (60.47% vs. 36.93%), while the whole turbine has specific exergy destruction equal to 52.49%, Fig. 8. LP turbine part has higher exergy than energy specific loss, while HP turbine part and the whole turbine have much lower specific exergy losses when compared to specific energy losses, Fig. 5 and Fig. 8.

Exergy flow streams of steam and power throughout the analyzed turbine, according to operating parameters from Table 1 as well as by using general equations (Eq. 5 - Eq. 9) and Eq. 28 - Eq. 36 are presented in Fig. 9. Taking into account the parameters of the ambient (pressure and temperature) generates additional steam exergy loss (when compared to energy flow streams) which for the whole turbine is 556.48 kW. In the cumulative exergy destruction of the whole turbine are included mentioned steam exergy loss (steam exergy destruction) and mechanical losses.

The influence of the ambient temperature change on steam turbine exergy efficiencies and exergy losses is usually low [49, 50]. Still, it can be concluded that an increase in the ambient temperature reduces turbine exergy efficiency and increases turbine exergy destruction [8]. For the same mechanical efficiency of each turbine part and the whole turbine, mechanical losses will remain the same as presented in Fig. 3 (b) and in Fig. 9, regardless of the ambient temperature.

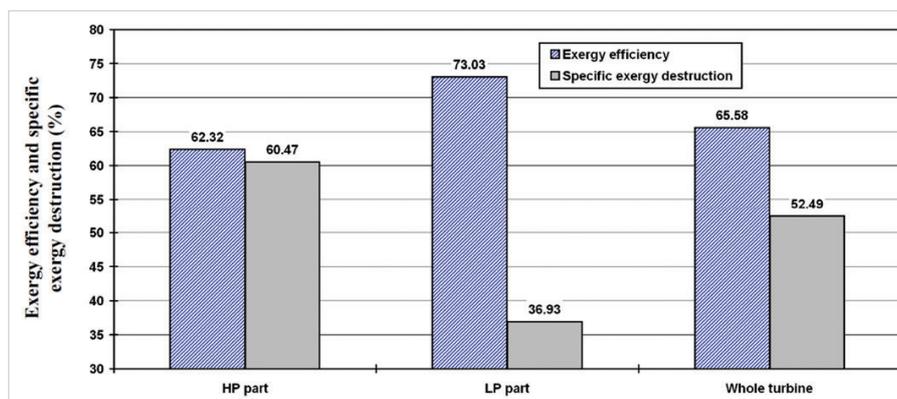


Figure 8 Exergy efficiency and specific exergy loss of the analyzed steam turbine and its parts  
Slika 8. Učinkovitost i specifični gubitak eksrgerije analizirane parne turbine i njezinih dijelova

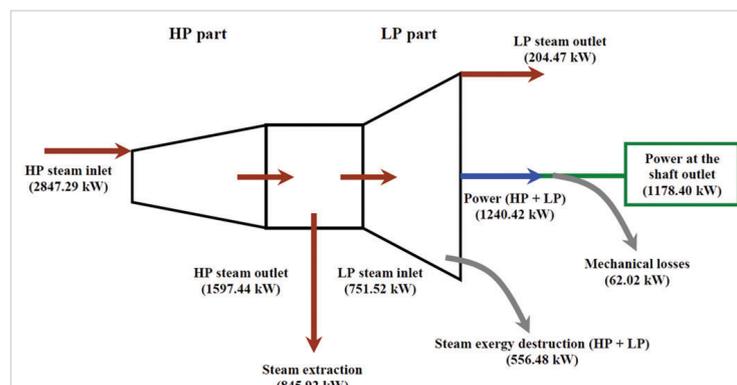


Figure 9 Exergy flow streams (steam and power) throughout the analyzed steam turbine  
Slika 9. Struje protoka eksrgerije (para i snaga) kroz analiziranu parnu turbinu

## 6. CONCLUSIONS / Zaključci

This paper focuses on the thermodynamic (energy and exergy) analysis of low-power steam turbine with one extraction for marine applications. According to the producer data, losses and efficiencies of the whole turbine and both turbine parts (HP and LP part) are calculated. Energy and exergy flow streams are also presented throughout the analyzed turbine along with mechanical losses as an integral part of the analysis.

The major conclusions obtained from the presented analysis are:

- HP turbine part, in comparison with the LP turbine part, produces higher power (ideal and real), but also has higher mechanical, energy and exergy losses.
- Regardless of the fact that LP turbine part operates in much heavier conditions in comparison with the HP turbine part (with wet steam, which has a high volume flow), LP turbine part has significantly higher energy and exergy efficiencies and lower specific energy and exergy losses (destructions).
- In the turbine energy analysis, the only losses are mechanical losses (if the steam which passes through front and rear turbine gland seal is neglected). In the turbine exergy analysis additional loss occurs (steam exergy destruction).
- The whole observed turbine has energy and exergy efficiencies equal to 62.84% and 65.58%, while energy and exergy turbine losses are 696.74 kW and 618.50 kW, what are expected efficiencies and losses for low-power steam turbine.
- Analyzed turbine at the shaft outlet produces real power equal to 1178.40 kW, which can be used for any power consumer drive.
- Presented steam turbine, along with produced power, delivered a notable amount of heat (by steam extraction) to any heat consumer or more of them.

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Nazivlje

Abbreviations:

HP	High Pressure
LNG	Liquefied Natural Gas
LP	Low Pressure
WT	Whole Turbine

Latin Symbols:

$\dot{E}$	the total energy/exergy of a flow, kW
$h$	specific enthalpy, kJ/kg
$\dot{m}$	mass flow rate, t/h or kg/s
$p$	pressure, bar or kPa
$P$	power, kW
$\dot{Q}$	energy heat transfer, kW
$s$	specific entropy, kJ/kg·K
$T$	temperature, K or °C
$\dot{X}_{\text{heat}}$	exergy heat transfer, kW

Greek symbols: / Grčki simboli

$\varepsilon$	specific exergy, kJ/kg
$\eta$	efficiency, %

Subscripts:

0	the ambient state
en	energy
ex	exergy
in	inlet (input)
is	isentropic (ideal expansion)
mech	mechanical
out	outlet (output)
re	real (polytropic expansion)

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