

**NONLINEARITY OF THE PIEZORESISTIVE EFFECT OF p-TYPE SILICON
DIFFUSED LAYERS WITH HIGH SURFACE CONCENTRACION**

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ABSTRACT

In this work we present results of measurement of piezoresistivity coefficients of <100> oriented silicon with high boron dopant concentrations. An nonlinear approximative expression has been derivated, that can treat piezoresistance effect quantitavely .

The results of this work where used to discuss the nonlinearity of integrated piezoresistive bridge pressure sensors, in which the piezoresistors where obtained by diffusion of boron into silicon diaphragm.

1. INTRODUCTION

The change of electrical resistivity as a function of mechanical stress (piezoresistive effect) is in general case given by equation:

$$[\Delta\rho/\rho] = \sum \Pi_{ijk1} \sigma_{k1} \quad (1)$$

in which $\Delta\rho/\rho$ is a relative change of resistivity, σ_{k1} stress tensor and Π piezoresistive coefficient. Silicon has cubic lattice of diamond type, and therefore the number of indepent variables is reduced from 81 to 3. If the piezoresitors are placed along crystallogaphic axes, which is usual for semiconductor devices where this effect is used, the expression for resistivity change becomes:

$$\Delta R/R = \Pi_l \sigma_l + \Pi_t \sigma_t$$

Π_l denotes piezoresistive coefficient of longitudinal resistor, formed along $\langle 110 \rangle$, where electrical current and mechanical stress have the same direction. Π_t is piezoresistive coefficient of transversal resistor, also formed along $\langle 110 \rangle$, where the direction of current and mechanical stress are perpendicular one to each other. Piezoresistive coefficients may be regarded as linear only in the first approximation, and for small stress value. Ref. /1/ and /2/ report investigation for nonlinearity of piezoresistive effect of diffused resistor with dopant concentration range $1 \times 10^{24} \text{ m}^{-3}$ to $1.5 \times 10^{25} \text{ m}^{-3}$. We did not find data in literature about concentrations of approx. $2 \times 10^{26} \text{ m}^{-3}$ although they have high practical importance.

2. EXPERIMENTAL

It is well known that $\langle 100 \rangle$ oriented silicon is widely used for pressure sensors and accelerometers. The mentioned orientation enables us to etch sample accurately along $\langle 111 \rangle$ plane using orientation-dependent etching techniques and thus to form diaphragms or cantilevers. Samples with following parameters were used in measurements: silicon orientation $\langle 100 \rangle$, n-type, resistivity 5 ohm-cm, with diffused resistor with surface concentration of approx. $2 \times 10^{26} \text{ m}^{-3}$. The surface concentration of resistor was determined via known data for piezoresistance temperature coefficient /4/. The resistor were formed in open-tube boron diffusion from Boron+ source. Diffused layers was 700 um in length and 15 um in width, placed parallel along $\langle 110 \rangle$ axes. Eight samples were cantilever-cutted, with various length and width. Mechanical stress along clamped cantilever with force applied at the end is given by expression /3/:

$$\sigma_x = (F L)/z \{ [1 - (1/15) u^2] - L_0 / L \} \quad (3)$$

where

$$u \approx (12 F L^2)/Y b \quad z \approx b L^2/3$$

and L is cantilever length; L_0 is the distance between resistor and the attachment place; Y is Young's elasticity module, b is the width and h the thickness of the

canteliver. Mechanical load was delivered using known weight attached on the end of the canteliver. The extension is denoted with +, and the compression with -. It was necessary to hold the specimen in a dark place and at constant temperature. A temperature variation less than 0.1 °C during measurement, would cause a significant error.

3. RESULTS

The measured values of piezoresistive coefficient Π_{44} , which were found to be $27 - 30 \cdot 10^{-5} \text{MPa}^{-1}$, agree well with the results given in /4/. It confirms, together with the measured temperature coefficient of piezoresistor of 0.14 %/ °C, that resistor dopant concentration of $2 \times 10^{26} \text{ m}^{-3}$ was successfully achieved. The resistivity of longitudinal and transversal resistor versus mechanical stress is shown in Fig 1. This dependance can be approximated with high degree of accuracy, if the second order polynomial is used:

$$(\Delta R/R)_{l,t} = C_{11,t} \sigma + C_{21,t} \sigma^2 \quad (4)$$

The coefficients of polynomial are:

$$\begin{aligned} C_{11} &= 2.78 \cdot 10^{-4} \text{MPa}^{-1} & C_{21} &= 6.57 \cdot 10^{-8} \text{MPa}^{-2} \\ C_{1t} &= -1.48 \cdot 10^{-4} \text{MPa}^{-1} & C_{2t} &= 8.76 \cdot 10^{-8} \text{MPa}^{-2} \end{aligned}$$

and is extracted by method of least squares.

Nonlinearity of piezoresistive coefficients was calculated in the usual way, according to the expression:

$$NL(\sigma) = \frac{R(\sigma) - [R(\sigma_m) - R(\sigma_0)] L/L_m + R(0)}{R(\sigma_m) - R_0} \quad (5)$$

where $R(\sigma)$ is the resistance value under stress σ and σ_m is maximum stress. Its meaning is illustrated by Fig. 2.

4. CONCLUSION

Nonlinearity characteristics of piezoresistive coefficient of diffused p-type resistor on <100> silicon with high surface concentration were analyzed, using a

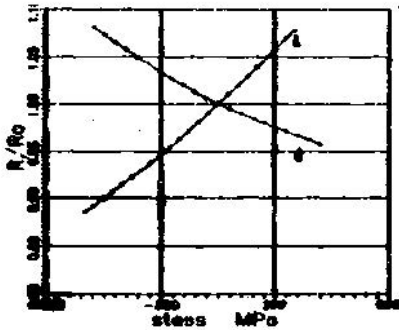


Fig 1 Relative change of resistivity vs. mechanical stress

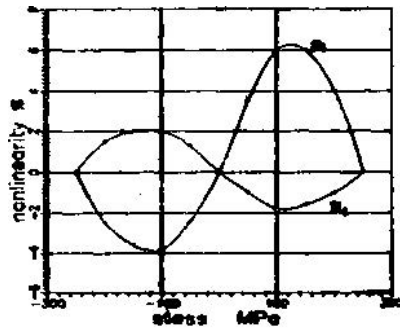


Fig. 2. Nonlinearity change vs. mechanical stress

canteliver-cuted samples. Following conclusions have been reached;

- piezoresistive coefficient can be approximated with order polinomial with sufficient accuracy.
- transversal resistor nonlinearity is higher than longitudinal one.
- nonlinearities of transversal piezoresistor for stress strain have opposite signs and approximateliy the same intensity. It is therefore possible to compensate these nonlinearities with piezoresistors connected in a Wheatstone's bridge.

References:

1. Suzuki K., Ishihara T., Hirata M., Tanigava H.: NONLINEAR ANALYSIS OF A C-MOS INTEGRATED SILICON PRESSURE SENSOR, IEEE TRANS.ELECTRONDEVICE, ED 34, No 6, 1987
2. Yamada K., Nishihara M., Shimada S., Tanabe M., Shimadze M., MatsuokaV.: NONLINEARITY OF p-TYPE SILLICON DIFFUSED LAYERS, IEEE TRANS. ELECTRON DEVICE, ED - 29 No 1, 1982
3. Timoshenko S., TEORIJA ELASTICNOSTI, GRADJEVINSKA KNJIGA, BEOGRAD, 1962
4. Tufte O., Selzer E. L.,: PIEZORESISTIVE PROPERTIES OF SILICON DIFFUSED LAYERS, J. APPL. PHYS. VOL 34 NO 2, 1963