

# Productivity and Energy Balance in Conversion of a *Quercus Cerris* L. Coppice Stand into High Forest in Central Italy

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## Abstract – Nacrtak

The work was carried out in Caprarola (Viterbo, Central Italy), in an aged *Quercus cerris* L. coppice positioned in hill zones, with 45% average slope. Harvesting was conducted according to the shortwood system (SWS). Felling and processing were done by chainsaw, while the bunching was performed with three different systems: in Plot 1 with mules, in Plot 2 with a tractor-mounted winch, in Plot 3 with polyethylene chutes. Logs were then forwarded to the roadside landing with a farm tractor, equipped with front and rear container bins. Finally, transportation from the landing to the company depot was performed with a truck and trailer unit. In order to speed up loading, a tractor equipped with a loader was used during this stage. On the basis of time consumption, product output and energy consumption, the authors estimated both the productivity and the energy balance obtained with each system. The best extraction productivity ( $PSH_0$ ) was achieved in Plot 2 (winching,  $0.8 \text{ t}_{d.w.} \text{ h}^{-1} \text{ worker}^{-1}$ ), while the lowest one was achieved in Plot 1 (mules,  $0.5 \text{ t}_{d.w.} \text{ h}^{-1} \text{ worker}^{-1}$ ). The energetic efficiency was high in all the plots (on average,  $97.6 \pm 0.3\%$ ). No correlation between time consumption and energy efficiency was observed. For Plot 3, high productivity, low time consumption and high system efficiency suggest that chutes are the most efficient bunching method from the energetic viewpoint. As the site was in a Nature Reserve and chutes are known to minimize damage to soil and seedlings, this system is to be recommended from both the energetic and environmental point of view, provided that wood can be extracted downhill.

*Key words:* forest operation, conversion of coppice to high forest, productivity, energy balance

## 1. Introduction – Uvod

Wood is still the dominant source of fuel in many developing countries (Matthews 2001). Until now, about 15% of world energy requirements have been provided by biomass. About 13% of biomass is used in developing countries, while 2% is used in developed countries (Baldini et al. 2007, Johansson and Lundqvist 1999). Among the many methods of potentially sustainable energy generation in the latter countries, biomass has received increasing attention (Matthews 2001). Between the biomass that may be used for energy production, wood shows the greatest potential from both the productive and the environmental point of view (Yoshioka et al. 2006).

However, the use of forest biomass must be supported by an energetic assessment, and must be

compatible with a sustainable forest management, also in terms of careful planning and organization of silviculture and logging operations (Baldini et al. 2007). In Italy, there is a lack of information on the energetic balance of forest biomass harvesting and delivery.

Historically, coppice represents an important source of firewood, suggesting that low-input coppice may be an efficient and sustainable biomass production system. According to the data offered by the Forest and Carbon Sink National Inventory (INFC 2005), in Italy there are 3,663,143 ha of coppice stands (41.8% of the Italian woodlands), most of which included in the category »coppice with standard« (28% of the Italian woodlands).

After the 1950s the management of coppices has been deeply affected by economic and social chan-

ges, which triggered off the progressive abandonment of coppice stands. The suspension of cutting produced the so-called »aged coppices« and brought about alternatives to the traditional form of coppice management, such as their conversion into high forests (Amorini et al. 1996). Conversion into high forest is obtained through repeated thinning of an aged coppice, in order to build a transitional high forest. At present, adult or aged coppices represent 89% of the whole Italian coppice surface, and transitional high forests occupy about 150,000 ha (INFC 2005).

A coppice in natural evolution shows a great structural variability, revealing dynamic changes toward typical structures of the high forest and a good ability to safeguard biodiversity and valorize the non-productive functions of forests. New silvicultural approaches support the natural development of aged coppice, with the purpose of increasing the stability and functionality of stands until reaching the appropriate age for seed regeneration (Manetti and Gugliotta 2006). As a result, coppice conversion is expected to further increase in popularity (Ciancio et al. 2002).

The most widespread extraction systems, both in coppice management and conversion, are by tractors with forestry winches (winching and skidding), tractors with forwarding bins and pack mules. Chutes are increasingly popular among public forest operators and represent an interesting technological development in similar contexts. In fact, chutes are popular with some small-scale operators – mostly public – but not so popular with the majority of private companies, which need to achieve higher productivity levels than those allowed by chutes.

The main aims of this study were to determine both the productivity of harvesting operations and the energetic balance (input/output) of different Shortwood Logging Systems (SWS) in conversion of coppice to high forest in central Italy. In order to estimate the energetic balance, we quantified: indirect inputs, i.e. the energetic value for production of machineries and tools; direct inputs, i.e. fuel and oil consumption of machineries, and energetic consumption of humans and animals during the work; output, i.e. energetic value of total wood extracted. These data were used to determine the energetic sustainability of three Shortwood System (SWS) bunching methods. SWS is the logging system commonly used in Italian coppice and conversion and may give several advantages: small landings, very low damage to residual stand during bunching/extraction (Spinelli et al. 2004), low investment level and energetic input (Hippoliti 1997, Bagnaresi et al. 1987). The final aim is to evaluate the best harvesting systems from an energetic point of view.

The term »energetic analysis« refers to the study of the energy implied in the production of a service or a product (IFIAS 1975). Such energy includes both the energy directly used during the production process (direct), and the energy stocked in the materials used for the production (indirect). The Gross Energy Requirements (GER) method is commonly used in energetic analysis (IFIAS 1975). The method underlines the importance of fossil energetic sources in the actual productive systems and focuses only on the fossil energy flow (direct and indirect). Although the GER method does not include the assessment of energetic human input, man work represents a relevant contribution in many production activities (IFIAS 1975, Biondi et al. 1989). A basic requirement for any bioenergy generation system is that the energy produced (output) must be greater than the inputs of non-renewable energy required to establish and operate the scheme (Matthews 2001).

## 2. Materials and methods – *Materijal i metode*

### 2.1 Characteristics of sites and plots – *Značajke mjesta istraživanja*

The study was carried out in a private forest in Caprarola Municipality (Viterbo Province – Central Italy – 42°19'25,02"N, 12°14'34,91"E). The forest road network in the area is quite developed with an average density of 38 m/ha. The climate is mild, with humid summers. Annual precipitation averages approximately 800 mm, winter temperature averages 13°C and summer temperature averages 21°C. As the forest is included in the Nature Reserve of Lago di Vico, silviculture is subject to the following constraints: the mass of felled trees has to be lower than 20–25% of the total mass; felling of large diameter trees is not allowed (Formulario Natura 2000 – IT6010057).

Forest operations were carried out in an aged *Quercus cerris* L. coppice. There were also big trees of *Acer* spp. and *Carpinus* spp. but only *Q. cerris* trees were cut. The main characteristics of the test area are shown in Table 1.

### 2.2 Logging methods – *Metode pridobivanja drva*

Logging operations were carried out in the summer of 2004 on a total area of 12.30 ha (all area surveys were made by GPS – Trimble Juno ST). All operations were carried out by the same private forest Company. Three plots with the same orographic, microclimatic and dendrometric characteristics were selected with random criteria, where to apply three

**Table 1** Main characteristics of test site and of felled trees**Tablica 1.** Osnovne značajke staništa, sastojine i posječenih stabala

Site Stanište	Average ground slope <i>Prosječni nagib terena</i>	%	45
	Altitude a.s.l. <i>Nadmorska visina</i>	m	790
	Exposure - <i>Ekspozicija</i>		south <i>južna</i>
Stand Sastojina	Age - <i>Starost</i>	year godina	75
	Trees - <i>Broj stabala</i>	n/ha	750
	DBH - <i>Prsni promjer</i>	cm	32
	Average tree height <i>Srednja visina stabala</i>	m	18
	Growing stock <i>Drvna zaliha</i>	m <sup>3</sup> /ha	708
Felling Sječa	Felled trees <i>Posječena stabla</i>	n/ha	337
	Total felled volume <i>Ukupni posječeni obujam</i>	m <sup>3</sup> /ha	177
	Total felled mass <i>Ukupna posječena masa</i>	$t_{d.w.}/ha$	127.4
		$t_{33\%}/ha$ $t_{33\% \text{ vlage}}/ha$	166.4
	Wood density <i>Gustoća drva</i>	$t_{d.w.}/m^3$	0.72
		$t_{33\%}/m^3$ $t_{33\% \text{ vlage}}/m^3$	0.94

different bunching systems, one system per plot (Fig. 1). The sequence of steps was:

⇒ Felling and processing: in all plots, felling and processing were carried out by chainsaw (STIHL MS 390, 3.4 kW) and the same team of two workers.

⇒ Bunching:

⇒ Plot 1 (0.37 ha): bunching with two groups of 6 mules and one worker each. The workers loaded and unloaded the mules in each group. The firewood was stacked along a forest track.

⇒ Plot 2 (0.39 ha): bunching by winching. A Valtra Valmet 6050 tractor (75 kW) equipped with a Norse 450 winch with a pulling capacity of 50 kN, and a rope of 11 mm diameter and 100 m length was used. Winching operations were carried out by three workers. The firewood was stacked along a forest track. Unfortunately, in this plot

the private forest Company applied a sub-optimum practice. In fact winching short-wood is more efficient than winching full-length stems.

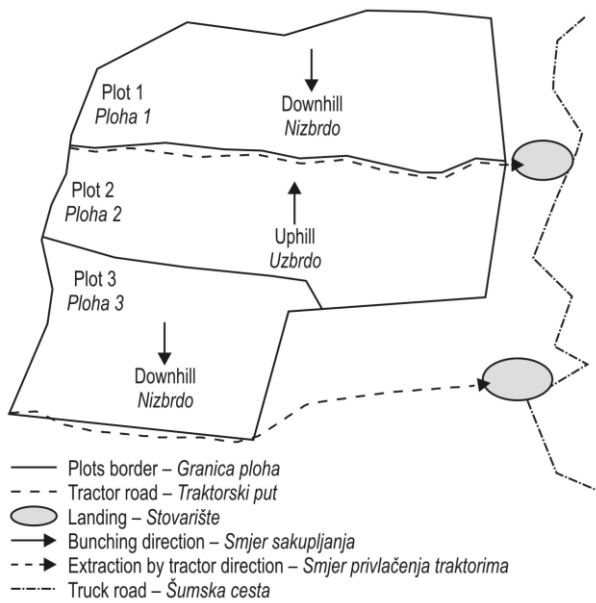
⇒ Plot 3 (0.24 ha): bunching with chute. The chute sections were 4 m long and made of medium density polyethylene. Each section weighted 35 kg. Sections were overlapped and secured with special steel hooks locked by an eccentric mechanism. In order to identify the optimal set-up route spacing and slope, a preliminary planning was made using a clinometer (Meridian MI 4007). The set-up route slope was 35–40%. A total of 9 chute lines were set up. In order to reduce the workload, the initial set-up was installed with the aid of a small portable KBF winch. Three workers operated the system (set-up, extraction, dismantle and relocation). The firewood was stacked along a forest track.

⇒ Extraction – In all plots, extraction of firewood from the forest track side to the landing was made by a tractor (a Valtra Valmet 6050 – 75 kW) equipped with forwarding bins on the front and rear sides (Piegai and Quilghini 1993) (Fig. 2). Both containers had a capacity of 2.8 steres each (1 stere = 1 m<sup>3</sup> stacked wood). Three workers operated the system: one driver and two loaders. Two landing sites were available (Fig. 1). Firewood from Plot 1 and Plot 2 was forwarded in one landing, while firewood from Plot 3 was forwarded to a second landing.

⇒ Transport – The transport from the landing to the company depot was performed with a truck (DAF CF 85.430, carrying capacity 16 t) and trailer (VIBERTI 7 LOMASS 22 R, carrying capacity 17 t) unit. In order to make easier the loading operation, a Valtra Valmet 6600 tractor equipped with a loader (Terrmacch T5100A) was used. Loading operations were carried out by the loader operator and two stackers.

### 2.3 Measurement and calculation of productivity – *Mjerenje i proračun učinkovitosti*

The main dendrometric parameters (diameter at breast height – DBH and tree height) were measured in 2 sample plots per each study plot (total surface 9600 m<sup>2</sup>). A Kruskal Wallis test (Sprent and Smeeton 2001) was applied to each dendrometric parameter and did not show any significant differences among the test areas. A non parametric test was selected because data showed low homogeneity of variance. A tree calibre (Silvanus type 1208, accuracy 0.5 cm)



**Fig. 1** Working site, plot schemes, landing, bunching and extraction directions

**Slika 1.** Radilište, plohe, stovarište, smjerovi skupljanja i privlačenja

was used for measuring the DBH of all the trees as well as the diameter of firewood logs at half length. The diameter and length of 300 randomly selected firewood pieces was measured at the two landings (150 by landing). For the calculation of moisture and wood density, 30 stem sections (3-cm thick) were collected at each landing. 60 wood samples were immediately weighed with a portable scale (Orma model BC16D) and transferred to the laboratory for moisture and wood density determination, using the thermo-gravimetric method (UNI ISO 3130 – 1985,



**Fig. 2** Valtra Valmet 6050 tractor (75 kW) forestry version, equipped with open-ended containers mounted on both front and rear sides

**Slika 2.** Traktor Valtra Valmet 6050 (75 kW), šumska izvedba, opremljen otvorenim spremnicima na prednjem i stražnjem kraju

UNI 9091 – 1987, CEN/TS 14774-2 – 2004; UNI ISO 3131 – 1985, CEN/TS 15103 – 2005). Statistical analysis (Kruskal Wallis) did not detect any significant differences (wood density  $f.w.$ : KW 7.087,  $p$ -value 0.131; wood density  $d.w.$ : KW 5.972,  $p$ -value 0.201) between the two landings.

Slopes were measured by means of a clinometer. A laser gauge (Stanley TLM 300 TRU LASER) was used to measure the bunching and extraction distances. A spring-loaded self-reeling tape (Walktax-r) was used to measure workers' and mules' walking distances. A CR10C CAMPBELL data-logger was used for the tractor engine data (power, engine load factor and using time). The transport distances by lorry were measured with the lorry odometer.

Working times were recorded for every single phase (except transport by lorry and trailer) by a chronometric table Minerva, equipped with three centesimal chronometers (Anon. 1988, Harstela 1991, Berti et al. 1989). In order to calculate outputs in different plots, effective time and delays in the work routine up to 15 min (unavoidable time UT and avoidable time AT) (Anon. 1988, Harstela 1991) were recorded.

Based on work times, volume and mass, the productivity per worker for different operations was calculated as follows: average gross productivity ( $PHS_{15}$ ) calculated on the basis of time consumption, inclusive of all delays up to the maximum event duration of 15 minutes; average net productivity ( $PHS_0$ ), calculated with the exclusion of delays. Productivity was also expressed in terms of both dry matter and fresh matter (measured in laboratory, 33% average moisture level).

## 2.4 Calculation of energy balance – Proračun energetske bilance

### 2.4.1 Machineries and tools – Strojevi i oruđe

According to the Gross Energy Requirements (GER) method (IFIAS 1975), the equation to calculate the energetic consumption of machineries and tools was:

⇒ Direct input (machinery only):

$$C_u = P \times F_c \times C_s \times T_u$$

where:

$C_u$  – unit consumption of fuel ( $\text{kg t}_{d.w.}^{-1}$ ).

$P$  – nominal engine power (kW);

$F_c$  – engine load factor (from 0 to 1);

$C_s$  – engine specific fuel consumption ( $\text{kg kW}^{-1} \text{h}^{-1}$ );

$T_u$  – time of use for output unit (dry mass) ( $\text{h t}_{d.w.}^{-1}$ );

In order to convert the unit consumption ( $\text{kg t}_{\text{d.w.}}^{-1}$ ) to direct input ( $\text{MJ t}_{\text{d.w.}}^{-1}$ ), the energetic values ( $\text{MJ kg}^{-1}$ ) showed in Table 2 were applied. Lubricant consumption was assumed as 3 kg per 100 kg of diesel and as 1/3 kg per 1 kg of chainsaw mixed fuel (Biondi *et al.* 1989).

**Table 2** Energetic input of fuel and lubricant (Biondi *et al.* 1989; Volpi 1992)

**Tablica 2.** *Energijska vrijednost goriva i maziva (Biondi i dr. 1989, Volpi 1992)*

Fuel Gorivo	Energetic value <i>Energijska vrijednost</i>
	MJ/kg
Diesel - Dizelsko	51.5
Mixed fuel (two-stroke) - Mješavina (2-taktni)	55.3
Lubricant - Mazivo	83.7

⇒ Indirect input (machinery and tools):

The indirect input  $I_{\text{ind.}}$  ( $\text{MJ t}_{\text{s.s.}}^{-1}$ ) of machineries and tools was determined by the average energetic values  $E_{\text{cm}}$  ( $\text{MJ kg}^{-1}$ ) of raw materials (Table 3) in relation to: their quantitative presence  $pm\%$ , total machinery mass  $m$  (kg), total service life of the machine  $t_1$  ( $\text{h t}_{\text{s.s.}}^{-1}$ ), and use of the machine in these forest operations  $ut$  (h) (Volpi 1992).

$$I_{\text{ind}} = \{[(\sum_n^1 EV_i) m] / ut\} t_1 \quad EV_i = E_{\text{cm}} pm\%$$

#### 2.4.2 People and animals – Ljudi i životinje

On the basis of literature data, we developed a preliminary approach to estimate the energetic consumption of human work. Mean energetic consumption of forest workers was calculated by applying the value of  $0.0502 \text{ MJ min}^{-1} \text{ worker}^{-1}$  (Rodio *et al.* 2002) as human physiological requirement. Similar values were suggested by Hippoliti (1997) and

**Table 3** Average energetic value of raw materials used in the construction of machinery and implements (Biondi *et al.* 1989; Volpi 1992)

**Tablica 3.** *Energijska vrijednost sirovina korištenih u konstrukciji strojeva i oruđa (Biondi i dr. 1989, Volpi 1992)*

Raw material Sirovina	Energetic value <i>Energijska vrijednost</i>
	MJ/kg
Iron matter (steel) - Metal (čelik)	67.5
No iron matter (copper and zinc) <i>Nemetali (bakar, cink)</i>	90.0
Alloy - Legure	360.0

Christie (2008), i.e.  $0.036\text{--}0.045 \text{ MJ min}^{-1} \text{ worker}^{-1}$  and  $0.028\text{--}0.030 \text{ MJ min}^{-1} \text{ worker}^{-1}$ , respectively.

We evaluated also the energy consumption of animal work (in our case the mules) by using the Forage Unit method (Ronchi 1988), summarized in the following equation (Table 4):

$$E_t = F_g \text{ uf } E_m / 0.55$$

where:

$E_t$  – total energy ( $\text{MJ d}^{-1}$ ),

$F_g$  – daily amount of feed per mule ( $\text{kg d}^{-1}$ ), i.e. 3 kg hay, 2.5 kg straw and 4 kg oats (Ronchi 1988),

$uf$  – forage unit ( $\text{kg}^{-1}$ ), a conversion factor to express equivalent energetic value of barley,

$E_m$  – nutritive value of 1  $uf$ , corresponding to 11.4 MJ, which is the amount of energy actually available for work at a metabolic conversion rate of 55%.

**Table 4** Calculation of a mule daily energetic consumption

**Tablica 4.** *Izračun dnevne potrošnje energije mule*

Feed Hrana	Daily amount <i>Dnevna količina</i>	Forage unit <i>Hranjivi odnos</i>	Raw energy <i>Hranjiva vrijednost</i>	Total energy <i>Ukupna energija</i>
	$F_g$	$uf$	$E_g$	$E_t$
	kg/day (kg/dan)	$\text{kg}^{-1}$	MJ	MJ/day (MJ/dan)
Hay <i>Sijeno</i>	3	0.42	20.72	26.11
Straw <i>Slama</i>	2.5	0.15	20.72	7.77
Oats - <i>Zob</i>	4	0.82	20.72	67.96

#### 2.4.3 Energy output – Energijski dobitak

In order to calculate the energetic value of wood, the energy released by its combustion must be determined (Volpi 1992). The Higher Heating Value (HHV) was determined (CEN/TS 14918) on 20 random samples, one sample per tree, by means of an adiabatic calorimeter (Parr, model 6200) (Canagaratna and Witt 1988). A Kruskal Wallis test, suggests very limited variability (KW 5.763,  $p$ -value 0.218). The average HHV of *Q. cerris* wood was  $20.62 \text{ MJ kg}_{\text{d.w.}}^{-1}$ .

**Table 5** Characteristics, time consumption and productivity of different harvesting phases**Tablica 5.** Značajke, utrošak vremena i učinak različitih faza pridobivanja drva

Felling and processing – Sječa i izrada													
Surface <i>Površina</i>	Workers <i>Radnici</i>	Chainsaw <i>Matorna pila</i>	Trees <i>Stabla</i>	Chainsaw time <i>Vrijeme rada motorne pile</i>	Fuel consumption <i>Potrošnja goriva</i>	Lubricant consumption <i>Potrošnja maziva</i>	Total gross time <i>Ukupno utrošeno vrijeme</i>	Unavoidable times <i>Opravljeni prekid</i>	Avoidable times <i>Neopravljeni prekid</i>	Log volume <i>Obujam trupaca</i>	Log mass <i>Masa trupaca</i>	Gross productivity <i>Učinak u ukupnom vremenu</i> PSH <sub>15</sub>	Net productivity <i>Učinak u efektivnom vremenu</i> PSH <sub>0</sub>
ha	No.	No.	No.	h	L	L	h	h	h	m <sup>3</sup>	t <sub>33%</sub> t <sub>33% vlage</sub>	t <sub>d.w.</sub> t <sub>suhe tvari</sub>	t <sub>d.w.</sub> h <sup>-1</sup> worker <sup>-1</sup> t <sub>suhe tvari</sub> h <sup>-1</sup> radnik
1.00	2	1	337	30.0	29.3	15.5	61.3	17.2	8.6	177	166.4	127.4	1.1   1.8
Bunching with mules (Plot 1) – Skupljanje mulama (ploha 1)													
Journeys <i>Turnusi</i>	Workers <i>Radnici</i>	Mules <i>Mule</i>	Logs <i>Trupci</i>	Av. logs per journey <i>Prosječni broj trupaca u tovaru</i>	Average mass per journey <i>Pros. masa tovara</i>	Av. extraction distance <i>Srednja udaljenost skupljanja</i>	Total gross time <i>Ukupno utrošeno vrijeme</i>	Unavoidable times <i>Opravljeni prekid</i>	Avoidable times <i>Neopravljeni prekid</i>	Log volume <i>Obujam trupaca</i>	Log mass <i>Masa trupaca</i>	Gross productivity <i>Učinak u ukupnom vremenu</i> PSH <sub>15</sub>	Net productivity <i>Učinak u efektivnom vremenu</i> PSH <sub>0</sub>
No.	No.	No.	No.	No.mule <sup>-1</sup>	t <sub>33%</sub>	m	h	h	h	m <sup>3</sup>	t <sub>33%</sub> t <sub>33% vlage</sub>	t <sub>d.w.</sub> t <sub>suhe tvari</sub>	t <sub>d.w.</sub> h <sup>-1</sup> worker <sup>-1</sup> t <sub>suhe tvari</sub> h <sup>-1</sup> radnik
24	2	12	3361	12	0.2	200.0	49.3	1.5	0.0	65	61.1	46.8	0.5   0.5
Bunching with tractor (Plot 2) – Skupljanje traktorom (ploha 2)													
Total winching <i>Broj privitavanja</i>	Workers <i>Radnici</i>	Tractor time <i>Vrijeme rada traktora</i>	Logs <i>Trupci</i>	Av. logs per journey <i>Prosječni broj trupaca u tovaru</i>	Fuel consumption <i>Potrošnja goriva</i>	Av. extraction distance <i>Srednja udaljenost skupljanja</i>	Total gross time <i>Ukupno utrošeno vrijeme</i>	Unavoidable times <i>Opravljeni prekid</i>	Avoidable times <i>Neopravljeni prekid</i>	Log volume <i>Obujam trupaca</i>	Log mass <i>Masa trupaca</i>	Gross productivity <i>Učinak u ukupnom vremenu</i> PSH <sub>15</sub>	Net productivity <i>Učinak u efektivnom vremenu</i> PSH <sub>0</sub>
No.	No.	h	No.	No.	L	m	h	h	h	m <sup>3</sup>	t <sub>33%</sub> t <sub>33% vlage</sub>	t <sub>d.w.</sub> t <sub>suhe tvari</sub>	t <sub>d.w.</sub> h <sup>-1</sup> worker <sup>-1</sup> t <sub>suhe tvari</sub> h <sup>-1</sup> radnik
143	3	10.4	3568	25	30	42.0	22.7	1.7	0.7	69	64.9	49.7	0.7   0.8
Bunching with chutes (Plot 3) – Skupljanje točlima (ploha 3)													
Chute lines <i>Točila</i>	Workers <i>Radnici</i>	Av. chute per line <i>Broj dijelova točila</i>	Logs <i>Trupci</i>	Winch time <i>Vrijeme privitavanja</i>	Fuel consumption <i>Potrošnja goriva</i>	Av. chute line length <i>Srednja duljina točila</i>	Total gross time <i>Ukupno utrošeno vrijeme</i>	Unavoidable times <i>Opravljeni prekid</i>	Avoidable times <i>Neopravljeni prekid</i>	Log volume <i>Obujam trupaca</i>	Log mass <i>Masa trupaca</i>	Gross productivity <i>Učinak u ukupnom vremenu</i> PSH <sub>15</sub>	Net productivity <i>Učinak u efektivnom vremenu</i> PSH <sub>0</sub>
No.	No.	No.	No.	h	L	m	h	h	h	m <sup>3</sup>	t <sub>33%</sub> t <sub>33% vlage</sub>	t <sub>d.w.</sub> t <sub>suhe tvari</sub>	t <sub>d.w.</sub> h <sup>-1</sup> worker <sup>-1</sup> t <sub>suhe tvari</sub> h <sup>-1</sup> radnik
9	3	22	2224	4.2	4	86	20.4	3.9	1.4	43	40.4	31.0	0.5   0.7
Extraction by tractor – Privlačenje traktorom													
Journeys <i>Turnusi</i>	Workers <i>Radnici</i>	Tractor time <i>Vrijeme rada traktora</i>	Logs <i>Trupci</i>	Av. logs per journey <i>Prosječni broj trupaca u tovaru</i>	Fuel consumption <i>Potrošnja goriva</i>	Av. extraction distance <i>Srednja udaljenost privlačenja</i>	Total gross time <i>Ukupno utrošeno vrijeme</i>	Unavoidable times <i>Opravljeni prekid</i>	Avoidable times <i>Neopravljeni prekid</i>	Log volume <i>Obujam trupaca</i>	Log mass <i>Masa trupaca</i>	Gross productivity <i>Učinak u ukupnom vremenu</i> PSH <sub>15</sub>	Net productivity <i>Učinak u efektivnom vremenu</i> PSH <sub>0</sub>
No.	No.	h	No.	No.	L	m	h	h	h	m <sup>3</sup>	t <sub>33%</sub> t <sub>33% vlage</sub>	t <sub>d.w.</sub> t <sub>suhe tvari</sub>	t <sub>d.w.</sub> h <sup>-1</sup> worker <sup>-1</sup> t <sub>suhe tvari</sub> h <sup>-1</sup> radnik
33	3	34	9155	277	11.8	570.0	20.4	0.0	0.0	177	166.4	127.4	2.1   2.1
Loading on truck and trailer – Utovar na kamionski skup													
Loads <i>Tovari</i>	Workers <i>Radnici</i>	Tractor time <i>Vrijeme rada traktora</i>	Logs <i>Trupci</i>	Av. logs per load <i>Prosječni broj trupaca u tovaru</i>	Fuel consumption <i>Potrošnja goriva</i>	Av. mass per load <i>Prosječna masa tovara</i>	Total gross time <i>Ukupno utrošeno vrijeme</i>	Unavoidable times <i>Opravljeni prekid</i>	Avoidable times <i>Neopravljeni prekid</i>	Log volume <i>Obujam trupaca</i>	Log mass <i>Masa trupaca</i>	Gross productivity <i>Učinak u ukupnom vremenu</i> PSH <sub>15</sub>	Net productivity <i>Učinak u efektivnom vremenu</i> PSH <sub>0</sub>
No.	No.	h	No.	No.	L	t <sub>33%</sub> t <sub>33% vlage</sub>	h	h	h	m <sup>3</sup>	t <sub>33%</sub> t <sub>33% vlage</sub>	t <sub>d.w.</sub> t <sub>suhe tvari</sub>	t <sub>d.w.</sub> h <sup>-1</sup> worker <sup>-1</sup> t <sub>suhe tvari</sub> h <sup>-1</sup> radnik
6	3	15.0	9155	1526	43	27.0	18.5	0.7	0.2	177	166.4	127.4	2.3   2.4

## 4. Results and discussion – Rezultati s diskusijom

### 4.1 Productivity – Učinkovitost

Productivity ( $PSH_{15}$  and  $PSH_0$ ) of each working phase was good (Table 5), as compared to literature data of manual logging operations in central Italian *Q. cerris* coppices (Calafatello et al. 2005, Fabiano et al. 2002, Piegai 2005, Piegai 2008). Technical problems in the use of the tractor and winch increased the time consumption for bunching, in particular during log hooking and winching, whereas bunching by mules or by chutes proceeded smoothly.

The best bunching productivity was recorded in Plot 2 (winching,  $0.8 t_{d.w.} h^{-1} worker^{-1}$ ), while the lowest one was recorded in Plot 1 (mules,  $0.5 t_{d.w.} h^{-1} worker^{-1}$ ) with Plot 3 showed intermediate results (chutes,  $0.7 t_{d.w.} h^{-1} worker^{-1}$ ). The best  $PSH_{15}$  was still in Plot 2 ( $0.7 t_{d.w.} h^{-1} worker^{-1}$ ), while Plot 1 and Plot 3 showed the same  $PSH_{15}$  ( $0.5 t_{d.w.} h^{-1} worker^{-1}$ ), because of longer unavoidable delay times (UT) in Plot 3 (Table 5). Then the tractor and winch performed best, despite the technical problems.

Because of the high concentration of wood on the site and the optimal chute slope (30–35%, Hippoliti 1997), chute productivity was higher than the average values reported in the literature ( $PSH_{15}$   $0.22–0.34 t_{f.w.} h^{-1} worker^{-1}$ , Calafatello et al. 2005). Due to the use of appropriate tractors and the availability of a good trail network, forwarding productivity was also higher than previously reported for similar work conditions ( $2.1 t_{d.w.} h^{-1} worker^{-1}$  vs.  $1.2–1.8 t_{f.w.} h^{-1} worker^{-1}$  in Piegai 2005, Piegai 2008). A preliminary assessment of transport productivity by truck and trailer showed that the truck needed 5 full trips of 60 km each at an average speed of 60 km/h to transport  $166.4 t_{33\%}$  of firewood.

### 4.2 Energetic balance – Energijska bilanca

The lowest energy efficiency was recorded in Plot 1 (mules, with a total input of  $71 GJ ha^{-1}$  or  $0.56 GJ t_{d.w.}^{-1}$ ); the results for Plot 2 were only marginally better (winch,  $-2.6\%$  or  $0.54 GJ t_{d.w.}^{-1}$  compared to Plot 1); the highest energy efficiency was calculated in Plot 3 (chutes,  $-22.7\%$  or  $0.43 GJ t_{d.w.}^{-1}$ ) (Table 6 and Fig. 3). Direct inputs were 34% higher in Plot 2 (winch) than in Plot 1 and Plot 3 (on average,  $45 GJ ha^{-1}$  or  $0.36 GJ t_{d.w.}^{-1}$ ). The most mechanized system (Plot 2, winch) had a 19% lower human input and a 16% higher indirect input than the system based on mules and chutes (on average,  $1.22 GJ ha^{-1}$  humans or  $0.01 GJ t_{d.w.}^{-1}$  and  $6.22 GJ ha^{-1}$  indirect input or  $0.05 GJ t_{d.w.}^{-1}$ ).

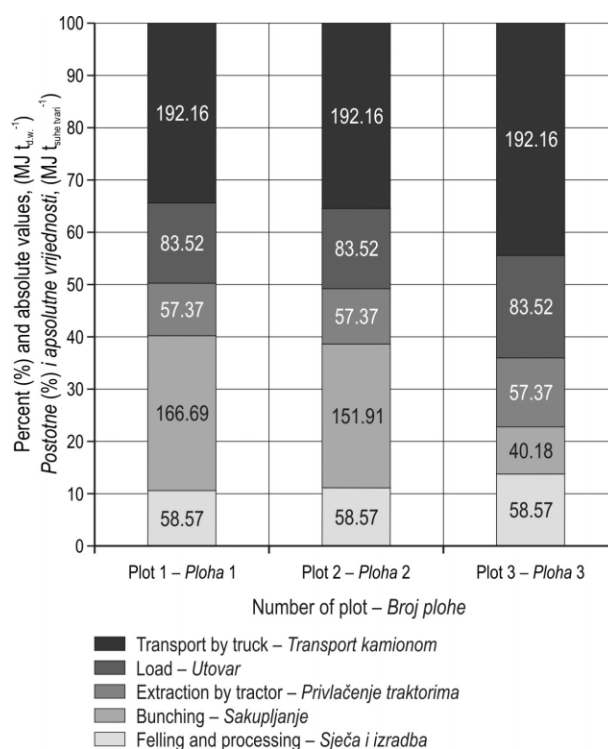
**Table 6** Energetic value of outputs and inputs (all working phases, transport included)

**Tablica 6.** Energijska vrijednost dobitka i utroška

Plot Ploha	Output Dobitak	Input – Utrošak				
		Machines & Tool Strojevi i alati		Human Ljudi	Mules Mule	Total Ukupno
		Direct Izravni	Indirect Neizravni			
$GJ ha^{-1}$						
1	2627.24	43.46	5.93	1.24	20.50	71.13
2	2627.24	61.01	7.25	0.99	0.00	69.25
3	2627.24	47.31	6.51	1.20	0.00	55.01

Concerning the role of single work phases (Fig. 3), the energetic input of truck transport contributed the most in all treatments (from 33% to 43% – average  $192.16 MJ t_{d.w.}^{-1}$ ), followed by extraction in Plot 1 and Plot 2 (from 28% to 30% or average  $159 MJ t_{d.w.}^{-1}$ ).

The input/output ratio was 28% higher in Plot 3 than in Plot 1 and Plot 2 (Table 7). Due to the large amount of biomass harvested, the input/output ratio was on average even three times higher than that reported in literature for chip harvesting (8.6–11.7, Baldini et al. 2007). Our ratios were, however,



**Fig. 3** Contribution of single work phases to the total energy inputs

**Slika 3.** Udio pojedinih radnih faza u ukupnom energijskom utrošku

**Table 7** Energy efficiency, time consumption and productivity (PSH<sub>15</sub> e PSH<sub>0</sub>) in three plots**Tablica 7.** Energjska učinkovitost, utrošak vremena i učinak

Plot Ploha	Input/output Dobitak/Utrošak	System efficiency Korisnost sustava	Time consumption Utrošak vremena	Gross productivity Učinak u ukupnom vremenu PSH <sub>15</sub>	Net productivity Učinak u efektivnom vremenu PSH <sub>0</sub>
		%	min t <sub>d.w.</sub> <sup>-1</sup> worker <sup>-1</sup> min t <sub>suhe tvari</sub> <sup>-1</sup> radnik <sup>-1</sup>	t <sub>d.w.</sub> <sup>-1</sup> worker <sup>-1</sup> t <sub>suhe tvari</sub> <sup>-1</sup> h <sup>-1</sup> radnik <sup>-1</sup>	t <sub>d.w.</sub> <sup>-1</sup> worker <sup>-1</sup> t <sub>suhe tvari</sub> <sup>-1</sup> h <sup>-1</sup> radnik <sup>-1</sup>
1	36.94	97.3	213.12	0.26	0.29
2	37.94	97.4	168.93	0.32	0.37
3	47.76	97.9	205.16	0.27	0.34

slightly higher than the literature data for the forestry sector (25–50, Scholz et al. 1998). Higher values (100–180, Bagnaresi et al. 1987) were also reported in some studies, which however did not include transport by lorry from landing to the company depot. If we remove transport from our calculation, our ratios will climb to 80–180.

The percentage energy efficiency (Table 7) (Energy efficiency = ((output – input)/output)\*100) was high in all the plots (97.6±0.3%). No correlation between time consumption and energy efficiency was observed: the operation with the highest energy efficiency (Plot 3) showed intermediate specific time consumption, whereas the operation with the lowest specific time consumption (Plot 2) showed an intermediate level in energy efficiency.

Plot 3 offered an intermediate high productivity and specific time consumption and high energy system efficiency, suggesting that HDPE chutes are the most efficient system from the energy viewpoint. In addition, the site was in a Nature Reserve and chutes are known to minimize damage to soil and seedlings (Eroglu et al. 2007, Hippoliti 1997): therefore, this system is to be recommended from both the energy and environmental point of view, provided that bunching is performed downhill.

#### 4. Conclusions – Zaključci

An energy analysis of productivity in logging operations carried out with three different bunching methods (mules, winch and chutes) in a *Q. cerris* coppice in central Italy showed input/output ratios of 37–48. These values are in the range already reported by previous studies on the subject, but the large variation of literature data (4–180 in Baldini et al. 2007, Scholz et al. 1998, Bagnaresi et al. 1987) suggests that more investigations are needed to further refine the estimates.

From an energy point of view, the best harvesting system is that where bunching is performed with log chutes, which also offer good productivity and significant environmental protection. As high mechanization in Shortwood System (SWS) operations in coppice can be difficult, the chute system is therefore recommended for use in the conversion of coppice stands into high forest systems. At the same time, more research is needed to develop efficient Full Tree Systems operations in coppice, in order to remove residues from the forest floor, in fire prone environment, such as Mediterranean countries. In fact, in coppice stands branches and tops can represent 10–30% of the total mass (Baldini et al. 2008), and their release into the stand improves dead fuel accumulation and increases the risk of the occurrence of wildfires, which represent a serious hazard for woodland, infrastructure and people (Marchi et al. 2007).

As the highest energy contribution to inputs was given by transport, the development of local markets should be encouraged. Adequate training of workers and planners is also needed for a sustainable use of forest biomass as renewable resource, which can provide increased energy output and a favourable carbon balance.

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## Sažetak

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### Učinkovitost i energijska bilanca pri konverziji šikara hrasta cera u viši uzgojni oblik

Šikare pokrivaju 41,8 % šumskoga zemljišta (3 663 143 ha) u Italiji. One su značajan izvor ogrjevnoga drva te se stoga njima može učinkovito i potrajno gospodariti radi proizvodnje šumske biomase. Sa stanovišta uzgajanja šuma potiče se konverzija sastojina u viši uzgojni oblik da bi se povećala stabilnost i funkcionalnost šumskih sastojina te postigla njihova prirodna obnova. Konverzija se šikara u viši uzgojni oblik provodi ponoovljenim procedama, što daje znatnu količinu ogrjevnoga drva. Pri tome se ogrjevno drvo prikraja u kratke sortimente.

Pri privlačenju drva kod radova na konverziji šikara ili pri potrajnom gospodarenju šikarama najčešće se koriste traktori opremljeni šumskim vitlima ili traktori opremljeni utovarnim spremnicima te sprege mula. Točila kao zanimljivo tehnološko rješenje privlačenja i skupljanja drva također dobro prihvaćaju privatni poduzetnici.

Cilj je rada odrediti učinkovitost radova pridobivanja drva i energijsku bilancu različitih sustava pridobivanja drva pri konverziji šikara u viši uzgojni oblik. Krajnji je cilj istraživanja procijeniti najbolji sustav pridobivanja s energijskoga stajališta. Osnovni je zahtjev da je pridobivena energija, koju predstavlja količina privučenoga i transportiranoga ogrjevnoga drva, veća od ukupno utrošene energije u sustavu pridobivanja drva. Ukupno utrošena energija uključuje izravno utrošenu energiju strojeva, ljudi i životinja, ali i energiju utrošenu u proizvodnju materijala, oruđa i strojeva koji se koriste u sustavu pridobivanja drva.

Istraživanje je provedeno u privatnoj šumi pri konverziji šikare hrasta cera u viši uzgojni oblik. Šumska je površina smještena u zaštićenom području te je sječa obavljena prema ovim propisima: ukupni posječeni drveni obujam ne smije biti veći od 20 do 25 % ukupne drvne zalihe, sječa stabala većih prsnih promjera nije dopuštena (Formulario Natira 2000 – IT6010057). Osnovne značajke staništa i sastojine te podaci o posječenom drvnom obujmu prikazani su u tablici 1. Stabla su posječena motornim pilama.

Površina je šumske sastojine podijeljena u 3 ispitne plohe na kojima su primijenjene različite metode skupljanja drva (slika 1). Statističkim testiranjem podataka izmjere prsnih promjera i visine primjernih stabala nisu uočene razlike između postavljenih ploha. Na prvoj su plohi drvo skupile dvije skupine od 6 mula i jednoga radnika po skupini. Ogrjevno je drvo slagano pored traktorskoga puta. Na drugoj plohi tri su radnika skupljala ogrjevno drvo pomoću traktora Valtra Valmet opremljenoga šumskim vitlom Norse 450, nazivne vučne sile od 50 kN, uz primjenu užeta promjera 11 mm i duljine od 100 m. Na trećoj plohi ogrjevno se drvo skupljalo točilima. Pojedinačni dijelovi točila bili su duljine 4 m, mase 35 kg, izrađeni od polietilena. Njihovim spajanjem i učvršćivanjem izrađeno je 9 točila uz pomoć prijenosnoga KBF vitla. Radi optimalnoga prostornoga rasporeda

točila i postavljanja dopuštenoga nagiba (35 – 40 %) prethodno su označeni pravci uz izmjeru terena padomjerom. Tri su radnika sudjelovala u skupljanju drva točilima.

Za privlačenje ogrjevnoga drva do stovarišta je korišten traktor Valtra Valmet 6050 (75 kW) opremljen spremnicima, kapaciteta od 1 m<sup>3</sup> prostornoga drva, na prednjem i stražnjem kraju (slika 2). Dva su radnika radila na utovaru ogrjevnoga drva u spremnike, a jedan je radnik upravljao traktorom. Ogrjevno se drvo s ploha 1 i 2 privlačilo na prvo stovarište, a s plohe 3 na drugo stovarište.

Drvo se dalje prevozilo kamionskim skupom (kamion DAF CF 85.430 nosivosti 16 t i prikolica VIBERTI 7 LOMASS 22 R nosivosti 17 t). Uz dva radnika na utovaru se također koristio traktor Valtra Valmet 6600 s utovarnim hvatalom Terrmach T5100A.

Duljina i srednji promjer ogrjevnoga drva izmjereni su na stovarištu. Za određivanje gustoće i mokrine drva sa 60 komada ogrjevnoga drva otpiljen je kolut 3 cm debljine. Uzorci su odmah vagani na terenu prijenosnom vagom, a zatim analizirani u laboratoriju termogravimetrijskom metodom. Laserskim su mjeračem izmjerene udaljenosti skupljanja i privlačenja, a mjernom trakom udaljenosti hoda ljudi i mula. Prijedeđeni je put kamionskoga skupa očitani s brojala prijeđenih kilometara. CR10C CAMPBELL data-logger je korišten za prikupljanje podataka o radu traktora.

Snimljena su utrošena vremena po radnim operacijama te vremena opravdanih i neopravdanih prekida rada. Na temelju utrošenih vremena, obujma i mase ogrjevnoga drva izračunat je učinak po radniku za istraživane sustave pridobivanja drva. Pri tome je učinak izražen u ukupnom vremenu rada (uključujući dopuštene prekide u najdužem trajanju od 15 min) te u efektivnom vremenu rada (bez prekida). Dodatno je učinak također izražen s obzirom na masu svoježe tovari, suhe tovari i mase tovari uz 33 % vlage u drvu.

Energijska je bilanca izrađena prema GER (Gross Energy Requirements) metodi (IFIAS 1975). Izračun je utrošene energije u sustavima pridobivanja drva podijeljen na izravni i neizravni utrošak strojeva i oruđa te utrošak energije ljudi i životinja.

Jedinična je potrošnja goriva (kg/t<sub>suhe tovari</sub>) izračunata kao umnožak nazivne snage motora, faktora opterećenja motora, specifične potrošnje goriva i norme vremena za svako sredstvo rada. Potrošnja je maziva određena temeljem pretpostavljene vrijednosti od 3 kg maziva na 100 kg dizelskoga goriva, odnosno 1/3 kg na 1 kg smjese goriva motorne pile. Energijske vrijednosti prikazane u tablici 2 korištene su za određivanje utrošene energije (MJ/t<sub>suhe tovari</sub>).

Neizravni utrošak energije strojeva i oruđa izračunat je na osnovi prosječnih energijskih vrijednosti sirovina (tablica 3), kvantitativnoga udjela pojedine sirovine, mase strojeva, vremena održavanja stroja i vremena primjene stroja.

Utrošak je energije radnika izračunat na osnovi fiziološke potrebe čovjeka od 0,0502 MJ/min (Rodio i dr. 2002). Metoda hranjivoga odnosa (Ronchi 1988) primijenjena je za izračun utroška energije mula. Izračun se zasniva na potrebnoj dnevnoj količini sijena, slame i zobi za jednu mulu, hranjivu odnosu (faktor koji izražava ekvivalent energijske vrijednosti ječma) i hranjivoj vrijednosti namirnica (tablica 4).

Dobivena energija predstavlja energiju koja nastaje izgaranjem privučenoga i prevezenoga drva. Određena je gornja ogrjevna moć drva kalorimetrom na 20 uzoraka te je ustanovljena srednja vrijednost od 20,62 MJ/kg<sub>suhe tovari</sub>.

Najveća je učinkovitost pri skupljanju drva zabilježena pri primjeni traktora s vitlom. Zatim slijedi učinak pri skupljanju točilima, a najmanji se učinak postiže pri skupljanju drva mulama (tablica 5).

Najveći je utrošak energije (71 GJ/ha) ostvaren na plohi 1 gdje se drvo skupljalo mulama (tablica 6). Izravni utrošak strojeva i oruđa najveći je pri skupljanju drva traktorom s vitlom. Taj sustav pridobivanja drva ima oko 19 % manji utrošak ljudske energije i oko 16 % veći neizravni utrošak energije od sustava s upotrebom točila i mula. Najveći je udio kamionskoga prijevoza u ukupno utrošenoj energiji (slika 3).

Najveći je odnos dobitka/utroška energije (47,76) ostvaren na plohi 3 primjenom sustava pridobivanja drva koji uključuje skupljanje točilima (tablica 7). Energijska je korisnost svih sustava vrlo velika – od 97,3 % kod sustava koji primjenjuje skupljanje mulama do 97,9 % kod sustava s primjenom točila. Učinak sustava pridobivanja drva s primjenom točila od 0,32 t<sub>suhe tovari</sub> h<sup>-1</sup> radnik<sup>-1</sup> u ukupnom vremenu, odnosno 0,37 t<sub>suhe tovari</sub> h<sup>-1</sup> radnik<sup>-1</sup> u efektivnom vremenu, nalazi se u sredini vrijednosti učinaka promatranih sustava.

Sustav se pridobivanja drva s primjenom točila odlikuje povoljnim mogućim učinkom te najvećim odnosom dobitka/utroška energije. Primjena točila znatno utječe na smanjenje oštećenja šumskoga tla i pomlatka te se

preporučuje za izvođenje radova skupljanja drva u zaštićenim područjima, kao što je bilo mjesto istraživanja. Pri tome treba napomenuti da je primjena točila moguća jedino pri skupljanju drva niz nagib.

Iz svega navedenoga donosi se zaključak o ekonomskoj i okolišnoj povoljnosti primjene točila u sustavu pridobivanja drva.

*Ključne riječi: šumski radovi, konverzija šikara u viši uzgojni oblik, učinkovitost, energijska bilanca*

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