

Prediction of temperature drop accompanying a given pressure drop for natural gas wellstreams

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PROFESSIONAL PAPER

Accurate prediction of the temperature drop accompanying a given pressure drop for the natural gas production systems is necessary in the effective design of natural gas production facilities. Current rigorous compositional models depend on many variables and require information about fluid composition. In this paper, a simple-to-use method which is easier than current available models, is presented to predict accurately the appropriate temperature drop accompanying a given pressure drop in natural gas production systems based on the black-oil model to get a quick approximate solution for the temperature drop of a natural gas streams in gas production systems. Considering the results, the new developed correlation is recommended for rapid estimation of temperature drops in gas production systems for pressures up to 45 MPa and pressure drops up to 25 MPa. The obtained results illustrate that good agreement is observed between the reported data and the values calculated using the new developed method. The average absolute deviation between reported data and the proposed correlation is around 4.6%. The proposed method appears to be superior owing to its accuracy and clear numerical background, wherein the relevant coefficients can be retuned quickly for various data.

Key words: natural gas, liquid content, temperature drop, Black-Oil model, simulation

1. Introduction

Predicting accurate temperature profiles in gas-production systems can improve the design of production facilities. As an example, temperature profiles in systems have application in accurate two-phase flow pressure drop prediction, gas-lift designs, and etc. If composition of gas is available, engineers predict the temperature drop by using a computer simulation program based on a fully compositional equation of state (EOS) pVT formulation and flash calculation. The program will perform a flash calculation, internally balancing enthalpy. It will calculate the temperature downstream of the choke, which assures that the enthalpy of the mixture of gas and liquid upstream of the choke equals the enthalpy of the new mixture of more gas and less liquid downstream of the choke. Otherwise, the gas production system can be modeled with the use of a black-oil model, which is also a tool for modeling the gas reservoir exploitation and for calculating the resources.¹² Black-oil simulators represent a high percentage of all simulation applications and they can model immiscible flow under conditions such that fluid properties can be treated as functions of pressure.¹ Coats⁶ presented radial well simulations of a gas condensate that showed a modified black-oil pVT formulation giving the same results as a fully compositional equation of state (EOS) pVT formulation for natural depletion above and below dew point. Under certain conditions, he found that the modified black-oil model could reproduce the results of compositional simulation for cycling above the dew point.^{12,10}

Fevang et al.^{10,11} obtained results which mostly support the conclusions by Coats.⁶ However, they found differ-

ences in oil recoveries predicted by compositional and modified black oil (MBO) models when the reservoir is a very rich gas condensate and has increasing permeability downwards.¹² According to their final conclusions, a black oil simulator may be adequate where the effect of gravity is negligible, and for gas injection studies black oil model can only be used for lean to medium-rich gas condensate reservoirs undergoing cycling above dew point.¹² El-banbi and McCain^{7,8} suggested that modified black oil (MBO) approach could be used regardless of the complexity of the fluid. Their paper presented the results of a full field simulation study for a rich gas condensate reservoir. The modified black oil (MBO) model performance was compared with the performance of a compositional model in the presence of water influx and also a field wide history match study was conducted for above and below the dew point.^{7,8} Their paper presents an accurate match of average reservoir pressure and water production rates. They also mentioned contrary to the common belief, the modified black oil (MBO) approach proves to be sufficient for modelling gas condensate behaviour below the dew point and using the modified black oil (MBO) approach, instead of a fully compositional approach, may result in significant time saving especially in full-field simulation studies.⁷

El-Banbi et al.⁹ presented the set of correlations to generate modified black-oil pVT properties without the need for fluid samples or elaborate procedure for equation of states (EOS) calculations.

Choking, or expansion of gas from a high pressure to a lower pressure, is generally required for control of gas well flow rates. Choking is achieved by the use of a choke or a control valve.¹ The pressure drop causes a decrease

in the gas temperature, thus hydrates can form at the choke or control valve. For a single component fluid, such as methane, a Mollier diagram can be used to calculate temperature drop directly. However, natural gas is not a single component and a Mollier diagram will probably not be available.¹

For black oil models and when composition of natural gas is not available, It is an essential to develop a simple correlation to predict accurately the appropriate temperature drop in natural gas production systems based on the black-oil model to get a quick approximate solution for the temperature drop of a natural gas streams. According to our knowledge, there is no correlation in the petroleum literature for the black-oil model to estimate temperature drop accompanying a given pressure drop for natural gas production streams. This paper describes a simple-to-use method for accurate prediction of temperature drop in the natural gas production systems for black-oil models.

2. Developing Simple Correlation

The required data to develop this correlation includes the reported from reference 8 (which are based on Gas Processors and Suppliers Association, Engineering Data Book, 9th edition, Tulsa, OK, 1972) for the temperature drop accompanying a given pressure drop at various initial (up stream) pressures and for wide range of gas well streams liquid content.¹ In this work a simple correlation is developed to estimate the appropriate temperature drop in natural gas production wells based on the black-oil model as a function of gas initial pressure, gas pressure drop and gas liquid contents. The following methodology has been applied to develop this correlation:

Firstly, the appropriate temperature drop in natural gas production systems are correlated as a function of

Coefficient	Pressure drop less than 13800 kPa	Pressure drop more than 13 800 kPa
A_1	1.040 719 991 7	9.362 950 815 33
B_1	$5.863 426 642 58 \times 10^{-1}$	$-6.939 607 862 509 \times 10^{-1}$
C_1	$-6.342 086 209 79 \times 10^{-2}$	$-2.382 350 807 \times 10^{-3}$
D_1	$2.814 825 604 12 \times 10^{-3}$	$1.707 747 521 64 \times 10^{-3}$
A_2	$2.430 764 529 804 \times 10^{-3}$	$-1.0182 981 741 4$
B_2	$3.069 694 101 171 \times 10^{-2}$	$1.677 279 709 66 \times 10^{-1}$
C_2	$-2.701 623 402 13 \times 10^{-3}$	$-6.403 523 610 97 \times 10^{-3}$
D_2	$2.322 543 561 003 \times 10^{-5}$	$-1.349 784 156 13 \times 10^{-5}$
A_3	$-4.474 832 714 94 \times 10^{-3}$	$3.407 062 549 01 \times 10^{-2}$
B_3	$-1.218 162 552 3 \times 10^{-3}$	$-6.307 680 717 04 \times 10^{-3}$
C_3	$1.731 754 226 62 \times 10^{-4}$	$2.974 089 458 302 \times 10^{-4}$
D_3	$-4.277 312 720 08 \times 10^{-6}$	$-2.195 720 171 01 \times 10^{-6}$
A_4	$1.155 971 384 07 \times 10^{-4}$	$-3.50 210 682 437 8 \times 10^{-4}$
B_4	$-8.871 530 681 92 \times 10^{-6}$	$5.983 899 386 423 \times 10^{-5}$
C_4	$-1.032 600 663 99 \times 10^{-7}$	$-2.950 536 870 498 \times 10^{-6}$
D_4	$-7.938 290 866 22 \times 10^{-9}$	$2.757 769 149 12 \times 10^{-9}$

Table 2. Tuned coefficients for equation (6)

Coefficient	Value
α	-5.555 968 253 968
β	$4.943 879 595 915 \times 10^{-2}$
γ	$8.171 231 318 052 \times 10^{-8}$
θ	$-2.610 407 344 111 \times 10^{-10}$

initial (upstream) pressure of gas stream for different pressure drops. Then, the calculated coefficients for these polynomials are correlated as a function of pressure drop. The derived polynomials are applied to calculate new coefficients for equation (1) to predict the appropriate temperature drop in natural gas production systems. Table 1 shows the tuned coefficients for equations (2) to (5).

In brief, the following steps are repeated to tune the correlation's coefficients.

1. Correlate the appropriate temperature drop in natural gas production systems as a function of initial pressure (p_i) for a given pressure drop (Δp).
2. Repeat step 1 for other pressure drops (Δp).
3. Correlate corresponding polynomial coefficients, which are obtained in previous steps versus pressure drop, $a = f(\Delta p)$, $b = f(\Delta p)$, $c = f(\Delta p)$, $d = f(\Delta p)$ [see equations (2)-(5)].

Equations (1) to (5) represent the new developed correlation in which four coefficients are used to correlate the temperature drop as a function of initial (upstream) pressure in MPa and the given pressure drop in MPa, where the relevant tuned coefficients have been reported in table 1, these tuned coefficients help to predict the temperature drop accompanying a given pressure drop for the natural gas well-stream for pressures up to 45 MPa and pressure drops up to 25 MPa. Those tuned coefficients can be retuned quickly if more data are available in the future according to the above-mentioned procedure.

$$\ln(\Delta T_i) = a + b_p + c_p^2 + d_p^3 \quad (1)$$

where:

$$a = A_1 + B_1 (\Delta p) + C_1 (\Delta p) + D_1 (\Delta p)^3 \quad (2)$$

$$b = A_2 + B_2 (\Delta p) + C_2 (\Delta p) + D_2 (\Delta p)^3 \quad (3)$$

$$c = A_3 + B_3 (\Delta p) + C_3 (\Delta p) + D_3 (\Delta p)^3 \quad (4)$$

$$d = A_4 + B_4 (\Delta p) + C_4 (\Delta p) + D_4 (\Delta p)^3 \quad (5)$$

This method is based on a liquid content of 112.3 m³/million m³. For each increment of 56 m³/million m³, there is a correction of 2.77 °C in temperature drop. For example, if there is no liquid, the final temperature is 5.54 °C cooler (the temperature drop is 5.54 °C more) than indicated by equation (1). Equation (6) is applied to correct temperature drop based on the liquid content of the gas (L , m³/ million m³), where the final gas tempera-

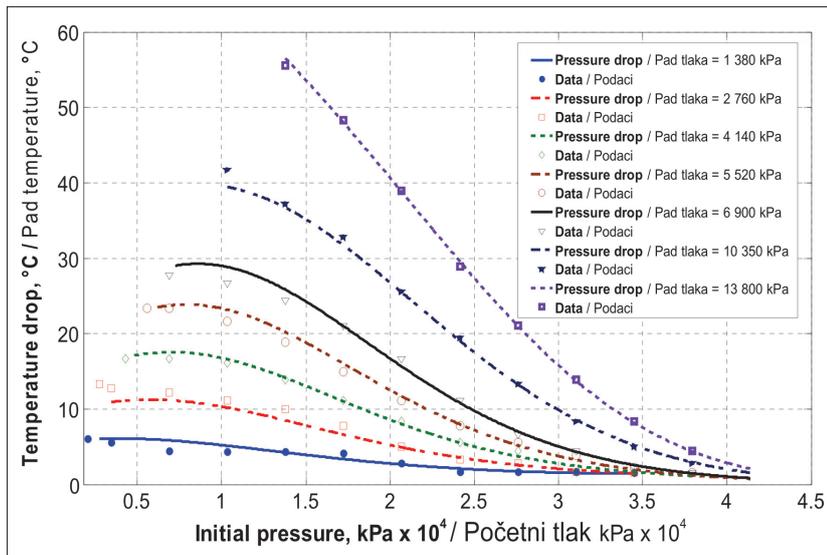


Fig. 1. Predicting temperature drop accompanying a given pressure drop for natural gas well-stream using the proposed method and comparison with reported data at liquid content of 112.3 cubic meters per million standard cubic meters.¹

Sl. 1. Predviđeni pad temperature koji prati odgovarajući pad tlaka za plinske bušotine, korištenjem predložene metode i usporedba s podacima iz izvještaja kod sadržaja kapljevine od 112,3 m³/milijun m³.¹

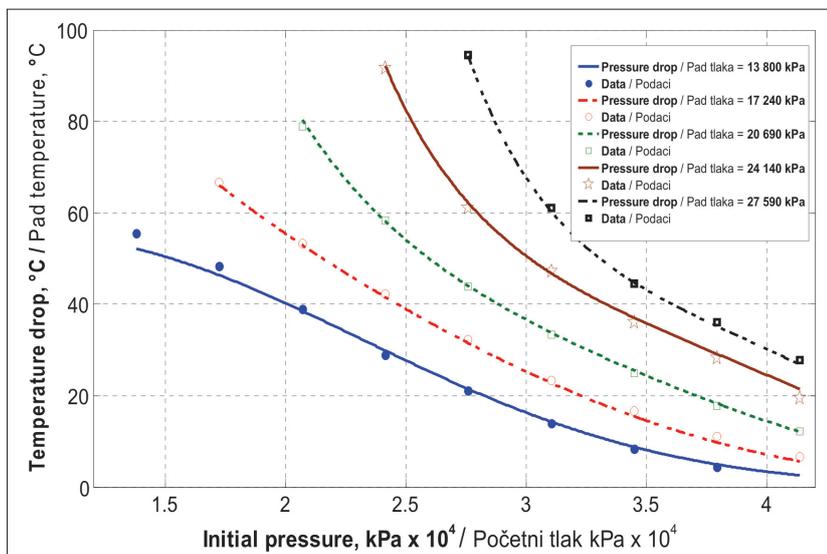


Fig. 2. Predicting temperature drop accompanying a given pressure drop for natural gas well-stream using the proposed method and comparison with reported data at liquid content of 112.3 cubic meters per million standard cubic meters.¹

Sl. 2. Predviđeni pad temperature koji prati odgovarajući pad tlaka za plinske bušotine, korištenjem predložene metode i usporedba s podacima iz izvještaja kod sadržaja kapljevine od 112,3 m³/milijun m³.¹

The obtained results illustrate that good agreement is observed between the reported data and the values calculated using the new developed method. In addition, we have selected exponential function to develop the correlation, because these functions are smooth and well-behaved (i.e. smooth and non-oscillatory) equations which should allow for more accurate predictions.²⁻⁵

3. Results

Figures 1 and 2 show the results of the proposed method comparing with the reported data¹ at various initial pressures and pressure drops and at liquid content of 112.3 cubic meters per million standard cubic meters where these figures show excellent agreement between proposed method and reported data.¹ Figure 3 illustrates the correction factor for natural gas temperature drop as a function of gas liquid content. Figures 4 and 5 show the performance of proposed correlation to predict temperature drop as a function of pressure and pressure drop at low and high pressure drops respectively for liquid contents of 112.3 cubic meters per million standard cubic meter of natural gas. These figures show the excellent performance of proposed correlation. However, the greater the amount of liquid in the gas the lower the temperature drops, thus leading to higher the calculated final temperature. Table 3 shows the accuracy of proposed correlation in terms of average absolute deviation percent with some typical reported data. It shows the proposed correlation has an average absolute deviation percent about 4.6 percent, which is very small deviation from reported data. Sample calculations shown here clearly demonstrate the simplicity of the proposed method and the benefits associated with such estimations.

Example:

A natural gas stream flows at 10 MPa and it will have a pressure drop around 4.14 MPa. Calculate the temperature drop for this gas if liquid content is 240 cubic meters per million standard cubic meters.

Solution:

Because pressure drop is less than 13.8 MPa, we use the coefficients in the first column of table 1 and we will have:

$$a = 2.5809 \text{ [from equation (2)]}$$

$$b = 0.0610 \text{ [from equation (3)]}$$

ture drop (ΔT) can be determined using Equation (7). Table 2 gives the tuned coefficients used in Equation (6).

$$\Delta T_{\text{correction}} = \alpha + \beta L + \gamma L^2 + \theta L^3 \tag{6}$$

$$\Delta T = \Delta T_i + \Delta T_{\text{correction}} \tag{7}$$

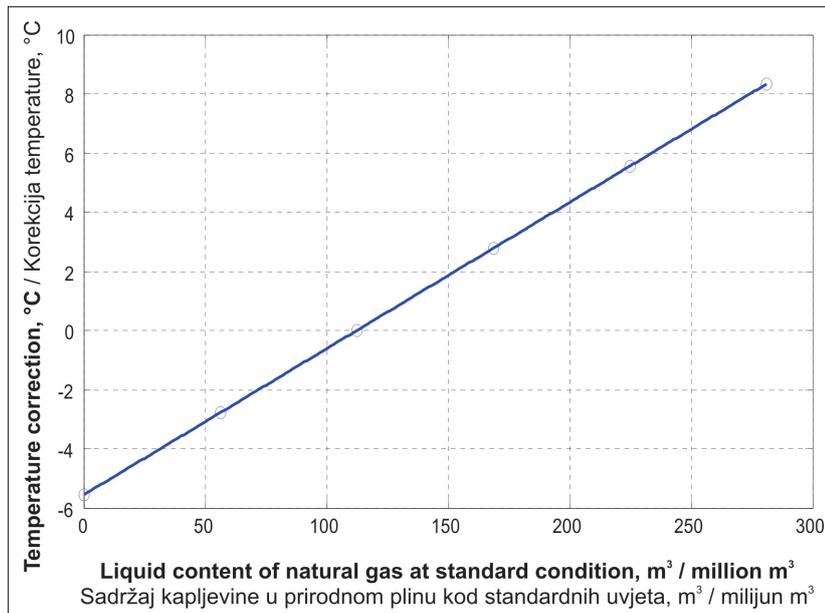


Fig. 3. Temperature drop correction factor as a function of liquid content of natural gases

Sl. 3. Faktor korekcije pada temperature kao funkcija sadržaja kapljevine prirodnog plina

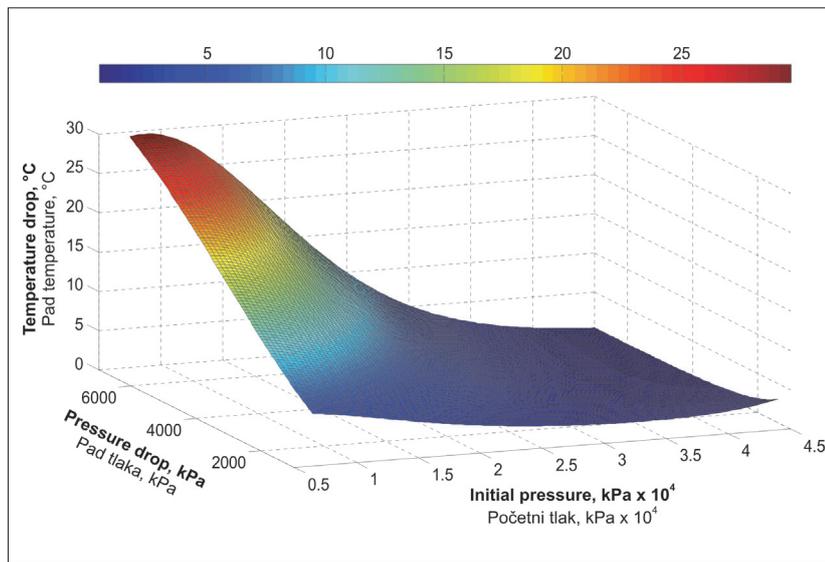


Fig. 4. Correlation performance for prediction of temperature drop as a function of initial pressure and pressure drop at liquid content of 112.3 cubic meters per million standard cubic meters (low pressure drop range). Color bar shows the temperature drop.

Sl. 4. Rezultat korelacije u predviđanju pada temperature kao funkcije početnog tlaka i pada tlaka kod sadržaja kapljevine od 112,3 m³ na milijun m³ prirodnog plina (opseg pada niskog tlaka). Crta u boji pokazuje pad temperature.

$$c = -0.0069 \text{ [from equation (4)]}$$

$$d = 0.000076536 \text{ [from equation (5)]}$$

$$\Delta T_i = 13.22 \text{ °C [from equation (1)]}$$

Now, we correct temperature drop by equations (6) and (7) for liquid content of 240 cubic meters per million standard cubic meters:

From equation (6):

$$\Delta T_{\text{correction}} = 6.31 \text{ °C}$$

From equation (7):

$$\Delta T = \Delta T_i + \Delta T_{\text{correction}} = 13.22 + 6.31 = 19.53 \text{ °C}$$

This is classic example showing how the information evolving out of this correlation can be used to predict the temperature drop accompanying a given pressure drop for the natural gas production systems.

4. Conclusions

In the present work, a simple-to-use correlation is developed to predict natural gas temperature drops at a given pressure drop in gas production systems. The new proposed correlation is based on the black-oil model, which is simpler than current available models that involve a large number of parameters and require more complicated and longer computations. Considering the results, the new developed correlation is recommended for rapid estimation of wellbore temperature drops in gas production systems for pressures up to 45 MPa and pressure drops up to 25 MPa. This Simple-to-use approach can be of immense practical value for the gas reservoir and production engineers to have a quick check on wellbore temperature drops in gas production systems at various conditions. In particular, personnel dealing with regulatory bodies of natural gas production would find the proposed approach to be user friendly involving no complex expressions with transparent calculations. The correlation proposed in the present work is simple and unique expression which is non-existent in the literature. This is expected to benefit and making design decisions which could lead to informed decisions on the temperature drop in black-oil model.

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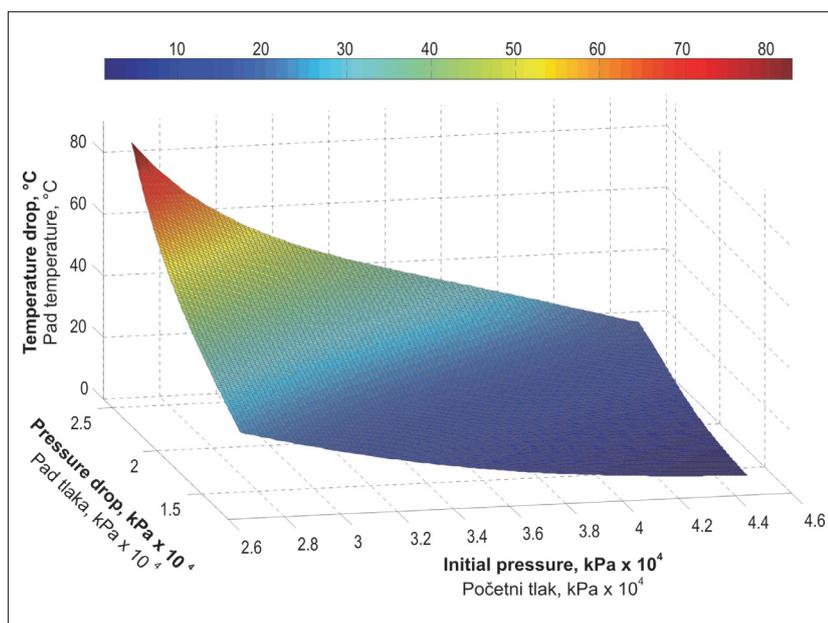


Fig. 5. Correlation performance for prediction of temperature drop as a function of initial pressure and pressure drop at liquid content of 112.3 cubic meters per million standard cubic meters (high pressure drop range). Color bar shows the temperature drop

Sl. 5. Rezultat korelacije u predviđanju pada temperature kao funkcije početnog tlaka i pada tlaka kod sadržaja kapljevine od 112,3 m³ na milijun m³ prirodnog plina (opseg pada visokog tlaka). Crta u boji pokazuje pad temperature

Table 3. Accuracy of proposed method				
Upstream pressure, MPa	Pressure drop, MPa	Reported temperature drop, °C ¹	Calculated temperature drop, °C	Absolute deviation percent
3.448 3	1.379 3	5.555 6	6.097	8.87
27.586	2.758 6	2.777 8	2.583	7.54
20.69	4.137 9	8.333 3	8.005	3.94
10.345	5.517 2	21.666 7	23.165 5	6.91
24.138	13.793	28.888 8	29.586	2.41
27.586 2	17.241 38	32.222 2	31.508	2.21
41.379	20.689	12.222 2	12.082 4	1.14
41.379	27.586	27.777 7	26.817 2	3.45
Average absolute deviation percent				4.6

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Nomenclature:

- Δp_i initial pressure in MPa
- Δp pressure drop in MPa
- ΔT temperature drop, °C at various liquid contents
- ΔT temperature drop for liquid content of 112.3 m³ / million m³, °C
- $\Delta T_{correction}$ Correction for temperature drop in other liquid contents of gas, °C
- L Liquid content of gas, m³/million m³



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i Index for initial pressure (upstream pressure)

References

1. Arnold, K. and Stewart, M. Surface Production Operations (2nd Edition) Volume 2 - Design of Gas-Handling Systems and Facilities. Chapter 4. Elsevier, 1999.
2. Bahadori, A. and Vuthaluru H. B. (2009) International Journal of Pressure Vessels and Piping, 86 (2009) 550-554.
3. Bahadori, A. and al., Chemical Engineering & Technology 31 (12)(2008) 1743-1747.
4. Bahadori, A. et al., International Journal of Greenhouse Gas Control 3 (4) (2009) 474-480
5. Civan, F., Chemical Engineering Progress 104 (7) (2008) 46-52.
6. Coats, K. H., Journal of Petroleum Technology, 5, 1870., 1985.
7. El-Banbi, A. H. and McCain, W.D” Producing Rich-Gas-Condensate Reservoirs—Case History and Comparison Between Compositional and Modified Black-Oil Approaches” Paper SPE 58988 presented at the 2000 SPE International Petroleum Conference and Exhibition in Mexico, Villahermosa, Mexico, 1-3 February 2000.
8. El-Banbi, A. H. and McCain, W.D., “Investigation of Well Productivity in Gas-Condensate Reservoirs” Paper SPE 59773 presented at the 2000 SPE/CERI Gas Technology Symposium, Calgary, Alberta, Canada, 3-5 April, 2000.
9. A.H. El-Banbi, K.A. Fattah and M.H. Sayyouh, “New Modified Black-Oil Correlations for Gas Condensate and Volatile Oil Fluids” SPE Annual Technical Conference and Exhibition, San Antonio, Texas, USA. 24-27 September 2006.
10. Fevang, O. and Whitson C. H.: “Modeling Gas Condensate Deliverability” Paper SPE 30714 presented at the SPE Annual Technical Conference and Exhibition, Dallas, Texas, 22-25 October, 1995.
11. Fevang, O., Singh, K., and Whitson C. H.: “Guidelines for Choosing Compositional and Black-oil Models for Volatile Oil and Gas Condensate Reservoirs” Paper SPE 63087, presented at the 2000 International Conference and Exhibition Dallas, Texas, USA, 1-4-October, 2000.
12. Izgec, B., and Barruffet, M.A., “Performance Analysis of Compositional and Modified Black-Oil Models for a Rich Gas Condensate Reservoir”, Society of Petroleum Engineers, SPE 93374, Offshore Europe, 6-9 September, Aberdeen, Scotland, 2005.