

Development of a new index for methane drainageability of a coal seam using the fuzzy rock engineering system

The Mining-Geology-Petroleum Engineering Bulletin
UDC: 622:08
DOI: 10.17794/rgn.2019.4.4

Original scientific paper



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Abstract

Coal seam gas is one of the most significant energy resources in unconventional gas fields. The identification of influencing parameters and methane drainage assessment are, thus, a prime geotechnical focus for all potential methane drainage projects. In methane drainage operations of coal seams, many factors, such as natural factors and operational factors affect the drainage efficiency. In this paper, a new coal seam methane drainageability index (CMDI) is introduced for pre-drainage techniques in a working mine. In this approach, seventeen parameters are considered as the main factors affecting the methane drainage from coal seam, and the interaction matrix based on the fuzzy rock engineering system (FRES), which analyzes the interrelationship between the parameters affecting methane drainage activities, are used to study coal seam methane drainageability. Since the value of interaction in the RES method is not unique, the fuzzy system is used to minimize subjectivity of the weights which are computed in the RES method. The Tabas coal mine (Iran) was selected as a case study and the proposed index was used to rank the C₁ seam in this mine. It was observed that the methane drainageability index could suitably predict the potential of the methane drainage of coal seam. The newly proposed index can be used as a basis for decision-making when uncertainties about the evaluation of the parameters affect the methane drainage of a coal seam and reduce the risk of methane drainage projects.

Keywords

methane drainage, rock engineering system, fuzzy system, coal seam, unconventional gas, Tabas coal mine

1. Introduction

Coal seams may contain 60% to more than 95% methane that depend on the presence of other gases in the coal seam (Karacan et al., 2011; Darling, 2011; Wilson et al., 1995; Hamawand et al., 2013). Coalbed methane (CBM) also known as coal seam gas (CSG) is a natural gas that is stored (adsorbed) in coal seams. In the coal mine methane (CMM) method, gas is captured in working coal mines by underground or surface and underground methane drainage techniques to ensure the safety of a mine. In the enhanced coalbed methane (ECBM) method, the CO₂ is injected into the coal bed and the methane gas is released by some chemical reactions and then it is extracted by a drainage operation (Thakur, 2014; Gale & Freund., 2001; Wong et al., 2007; Karacan et al., 2011). CBM production behavior is complex and difficult to predict or analyze especially in the early stages of recovery. This is because gas production from CBM reservoirs is governed by a complex interaction of single phase gas diffusion through a matrix system and two-phase gas and water flow through a

cleat system that are coupled through a desorption process (Aminian et al., 2004). Coal mine methane can create a serious threat to mining safety and productivity due to its explosion risk. Methane drainage from a coal seam is used to improve the safety of coal mine extraction, reduce greenhouse gas emissions and improve mine economics by allowing a mine to produce coal with minimum methane levels (Warmuzinski, 2008; Karacan et al., 2011; Flores, 1998; Sereshki, 2005; Comfort et al., 1999).

Methane drainage methods involve the removal of methane prior to mining activity on a virgin coal seam and during extraction. The objective methane drainage caused increases the amount of gas removal from the underground mining districts and hence minimizes the gas flow into the mine airways (Diamond, 1994; Thakur, 2014). Based on the degree of gasification of a coal seam and discontinuities in overburdens, vertical boreholes, horizontal boreholes, gob gas ventholes and inclined boreholes can be used for methane drainage. The specifications of boreholes such as the number of boreholes, orientation, spacing, location and gasification time depend on the coal seam properties and other special conditions (Black, 2011; Diamond, 1994). Coal

Table 1: The interactions of parameters in methane drainage from a coal seam

Parameters	Effect on other parameters	References
increasing the ash content	<ul style="list-style-type: none"> the adsorption capacity of coal decreases the gas production decreases 	(Laxminarayana and Crosdale., 1999)
increasing coal rank	<ul style="list-style-type: none"> gas content increases moisture content decreases decreased permeability an increase in cleat frequency 	(Moore, 2012; Sivek et al., 2010; Balan and Gumrah., 2009; Ting, 1977)
increasing the degree of saturation	<ul style="list-style-type: none"> gas production decreases from highly under saturated zones with low permeability 	(Black, 2011)
increasing the depth	<ul style="list-style-type: none"> gas content increases decreases permeability moisture content decreases in most cases ash content increases 	(Paul and Chatterjee,2011; (Siveketal.,2010)
increasing the in-situ stress	<ul style="list-style-type: none"> permeability decrease Fracture systems close gas content increases 	(Moore, 2012; Liu et al., 2016)
increasing moisture content	<ul style="list-style-type: none"> gas content decreases 	(Levy et al., 1997)
increasing cleat spacing	<ul style="list-style-type: none"> permeability decreases 	(Laubach et al., 1998)

seam methane drainage is influenced by various factors which are divided into two categories: geological and operational factors. The success of drainage operations is dependent on these factors. Numerous studies have attempted to investigate the effect of various factors on methane drainage from a coal seam. Karacan analyzed methane emission data from U.S longwall mining using multiple regression analysis and a neural network. The principal component analysis (PCA) was used to determine the weight of each parameter on methane emissions. PCA test models showed that gas content and seam thickness have the highest effect on gas emission from a coal seam (Karacan, 2009 a,b). Karacan analyzed the total gas flow rates and methane percentages from gob gas ventholes using a multilayer-perceptron (MLP) type artificial neural network (ANN). Also the sensitivity analysis was performed to determine the most important variables that affect venthole productions (Karacan, 2009). Karacan developed an expert classification system for U.S longwall degasification system selection. This model can be used as a decision tool for degasification system selection using site- and mine-specific conditions (Karacan, 2009). Hemza et al. considered ten factors influenced on methane content of coal beds Czech Republic. Numerous analyses were performed to study the relationship between these factors and gas content (Hemza et al., 2009). Dougherty and Karacan discussed methane control and prediction (MCP) software which was developed by NIOSH. This software can determine the type of degasification system, predict the production performance of a gob gas venthole, predict ventilation emissions from longwall mines and predict the dynamic elastic properties of coal (Dougherty and Karacan, 2011). Black studied the relationship between gas production from underground in-seam drainage boreholes, coal seam properties and op-

erational factors. The results indicated that the degree of saturation and drainage time has a significant impact on gas production (Black, 2011). Dai et al. studied the effect of geological factors such as effective trapping thickness, moisture content and ash content on coal seam gas content. They used support vector machine (SVM) theory to set up a nonlinear prediction model for gas content prediction between coal seam gas content and main controlling factors (Dai et al, 2013). Zawadzki et al. estimated the methane content of a coal mine using multivariable geostatistic simulation. The desorption factor and coal strength index, both of which were used in cokriging and sequential Gaussian co-simulation (Zawadzki et al., 2013). Liu et al. studied the effect of various factors on CBM productivity using the analytic hierarchy process (AHP) method. The results indicated that the weight of geological factors, engineering factors and drainage factors are 50%, 25% and 25%, respectively (Liu et al., 2014). In all those methods, the researchers did not consider all the parameters and their interactions completely.

There is an important point in methane drainage from a coal seam and its affecting parameters on each other. For example, increasing the value of one parameter causes an increase or decrease in the value of other parameters. Therefore, it is necessary to consider all parameter interactions completely. The interactions of some parameters in methane drainage are shown in Table 1.

Predicting the capability of a coal seam for methane drainage is an important issue in methane drainage systems. Therefore, the development of a new index that can classify the coal seam capability drainage by considering the interactions of influencing parameters is important. In such systems, the interactions of all influencing parameters (geological and operational) must be considered simultaneously.

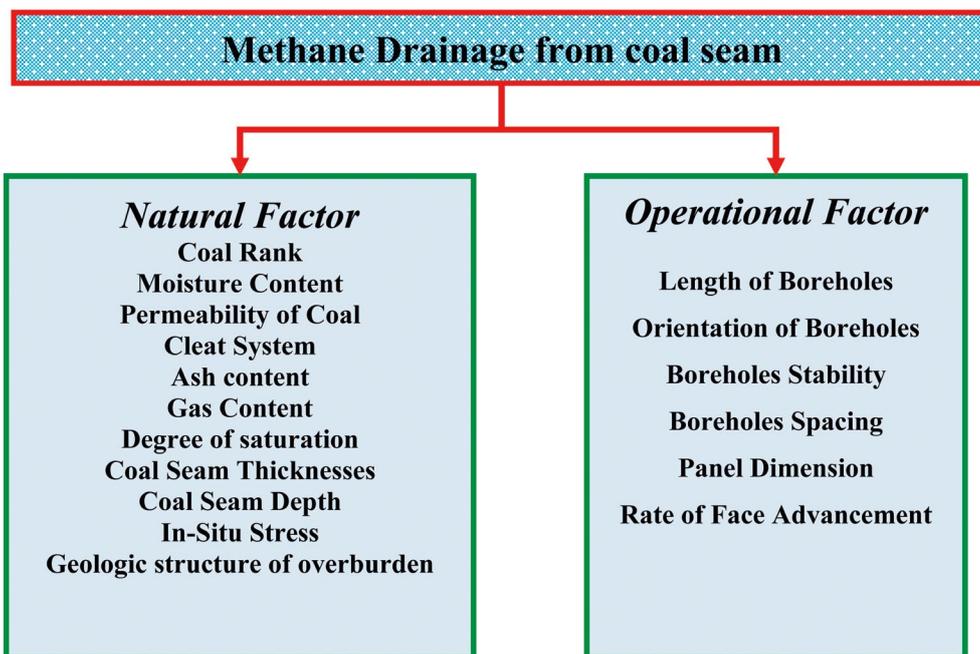
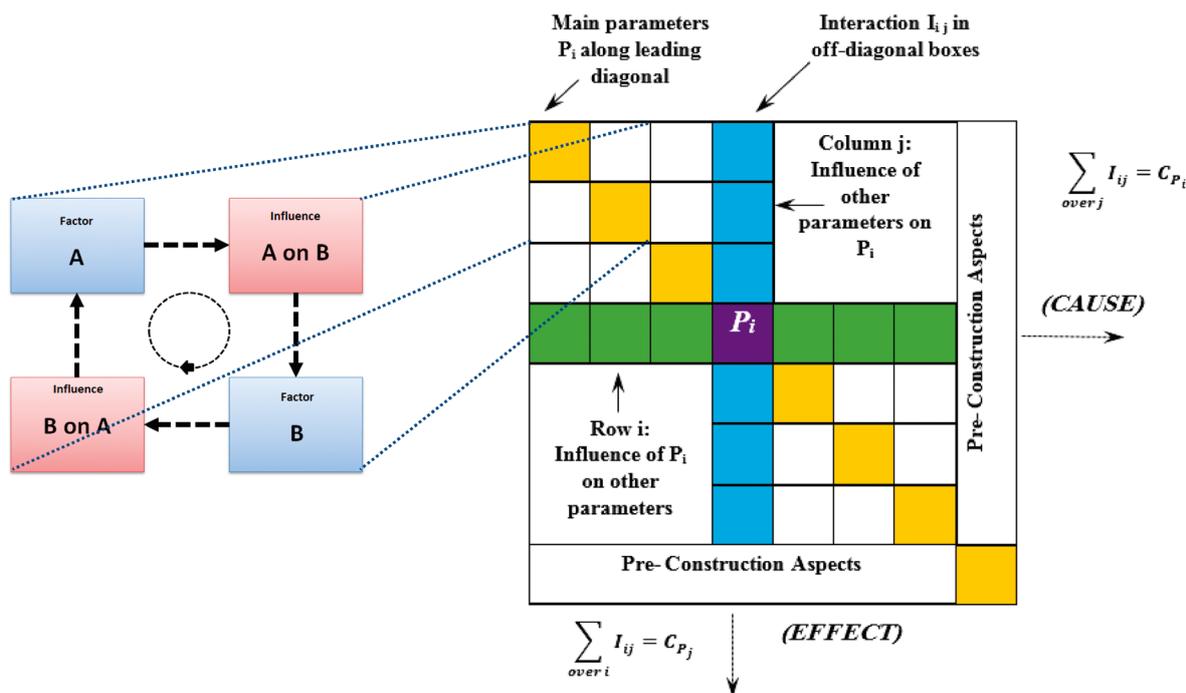


Figure 1: The main factors affecting methane drainage from a coalbed (Black, 2011; Moore, 2012; Liu et al., 2016; Karacan, 2009 a,b)



a: The principle of the interaction matrix with two factors

b: a general view details of the coding of interaction matrix

Figure 2: Summation of coding values in the row and column through each parameter to establish the cause and effect coordinates (Hudson, 1992)

The rock engineering system (RES) approach can be used for the analysis of coupled mechanisms in rock engineering problems (Hudson, 1992). In this approach, the main factors are listed along the main diagonal elements of a matrix, also called the interaction matrix, and the interrelations between pairs of factors are identified in off-diagonal elements. Many researchers have studied

this method in various fields of rock mechanics and mining engineering such as Shang et al. (2000), Zhang et al. (2004), Rozos et al. (2008), Andrieux and Hadjigeorgiou (2008), Younessi and Rasouli (2010), Zare Naghadehi et al. (2013), Saeidi et al. (2013), Huang et al. (2013), Rafiee et al. (2015 a, b) and Rafiee et al. (2016).

Table 2: Proposed range of affecting parameters on the coal seam methane drainage classification

Parameters	Rating				
	1	2	3	4	5
Coal Rank	Lignite	Sub-bituminous	Bituminous	Semi-anthracite	Anthracite
Moisture Content (%)	>3	2-3	1-2	0.5-1	<0.5
Permeability of Coal (md)	<0.1	0.1-1	1-9	10-50	>50
Cleat System (spacing (cm))	>20	8-20	3-8	1-3	<1
Ash content (%)	>60	40-60	20-40	10-20	<10
Gas Content (m ³ /t)	<5	5-10	10-15	15-20	>20
Degree of saturation (%)	0-20	20-40	40-60	60-80	80-100
Coal Seam Thicknesses (m)	<1	1-2.5	2.5-3.5	3.5-5	>5
Coal Seam Depth (m)	>1000 <100	100-400	800-1000	600-800	400-600
In-Situ Stress (MPa)	>30	20-30	10-20	5-10	<5
Geologic structure of overburden	Very low gas content and very high permeability of surrounding rocks, Very low strength of hangingwall and footwall, High permeable faults with low gas and low distance to each other	Low gas content and high permeability of surrounding rocks, Low strength of hangingwall and footwall, moderate permeable faults with low gas and unsuitable distance to each other	Moderate gas content and permeability of surrounding rocks, Moderate strength of hangingwall and footwall, impermeable faults with low gas	High gas content and low permeability of surrounding rocks, Moderate strength of hangingwall and footwall, impermeable faults with moderate gas	Very high gas content and very low permeability of surrounding rocks, High strength of hangingwall and footwall, impermeable faults with high gas and suitable distance to each other
Length of Boreholes (m)	<100	100-200	200-400	400-600	600-1100
Orientation of Boreholes to the principal horizontal stress) (Degree)	70-90	40-70	15-40	3-15	0-3
Boreholes and Wellbore Stability	instable	Very low stability	Low stability	Moderate stability	High Stability
Boreholes Spacing (m)	>60	30-60	15-30	5-15	<5
Panel Dimension (Width and Length) (m)	W<150 or L<600	W=150-200 or L=600-1000	W=200-250 or L=1000-1500	W=250-300 or L=1500-2000	W>300 or L=2000-3500
Cut Depth (cm)	<70	70-80	80-90	90-100	>100

The aim of this research is to propose a new index for assessing the drainageability of a coal seam using the fuzzy rock engineering system. Therefore, by using the FRES method first, the parameters with the highest effect on the methane drainage are found and then a new index is presented to predict the coal seam methane drainage potential for pre-drainage techniques.

2. Factors influencing methane drainage

In the first step, the parameters that influence the methane drainage have been identified. According to lit-

erature and various studies, the most important factors influencing methane drainage from a coal seam can be categorized into two types: natural factors and operational factors. These parameters are shown in **Figure 1**.

3. Rock engineering system

The concept of the rock engineering system (RES) approach was first introduced by Hudson for solving complex engineering problems. This approach can be used for the analysis of coupled mechanisms in rock engineering problems (**Hudson, 1992**). The RES uses a

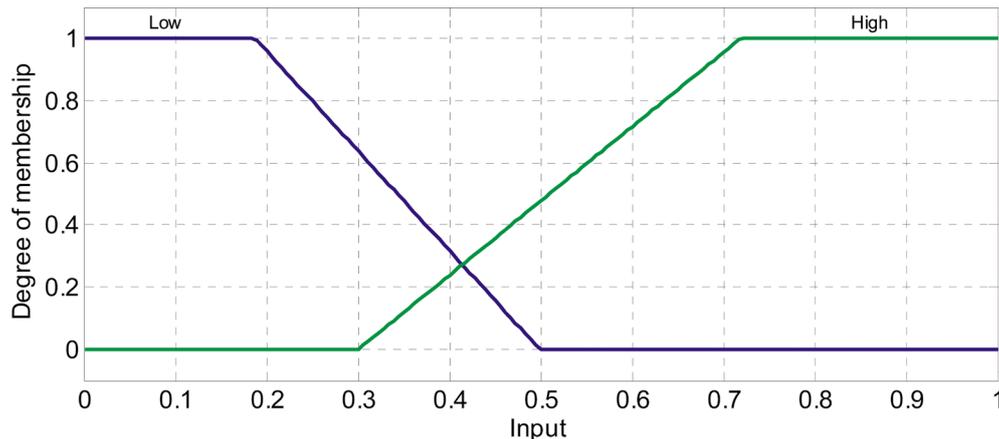


Figure 3: Fuzzy set for each fuzzy system input

top-down analytic model to treat the rock mass, the boundary conditions, and the engineering activities as a complete, interactive, and dynamic system. The key element in the RES method is the interaction matrix. The interaction matrix is a basic technique for characterizing the important parameters and the interaction mechanisms in a rock engineering system. In the interaction matrix, all parameters influencing the system are arranged along the leading diagonal of the matrix, called the diagonal terms. Otherwise, the influence of each individual parameter on any other parameters is included at the corresponding off-diagonal position of the matrix. The off-diagonal terms are assigned numerical values which describe the influence degree of one parameter on the other parameters. Assigning these values are usually referred to as “coding the matrix”. Several coding methods have been developed for this purpose, with the most common being the ‘expert semi-quantitative’ (ESQ) coding method (Hudson, 1992). ESQ coding has been used in nearly all previous works. In this method, one unique code is assigned to each interaction, thereby expressing the influence of a parameter on another in the matrix. Typically, coding values vary between 0 and 4 with 0 indicating no interaction, 1 indicating a weak interaction, 2 indicating a medium interaction, 3 indicating a strong interaction and 4 indicating a critical interaction. An interaction matrix is illustrated in Figure 2. After coding the interaction matrix by inserting the appropriate values for each off-diagonal cell of the matrix, the influence of each parameter on the system is named “cause” (C_i) and the effect of the system on each parameter is named “effect” (E_i) (see Figure 2).

The C-E diagram is created by (C_i, E_i) coordinate values plotted in cause and effect space. From this diagram “less interactive” and “more interactive” parameters are determined (Hudson, 1992).

4. Coal seam methane drainageability index (CMDI)

As mentioned in section 2, many parameters affect coal seam methane drainage. In this study, seventeen pa-

rameters are considered as the main factors affecting the methane drainage from a coal seam and the importance and physical ranges of parameters, also the corresponding ratings, are listed in Table 1. It is notable that the values of the parameters are divided into five classes and each class ranges from 1 to 5. The ranges of parameters in Table 2 were proposed based on the judgments of experienced experts in field methane drainage and also the results obtained from literature review.

4.1. Definition of the coal seam methane drainageability index (CMDI) using the fuzzy rock engineering system

As previously mentioned in the ESQ coding method, one value is deterministically assigned to each interaction. Therefore, in order to consider the uncertainties of the influence of one parameter on the others, the “Fuzzy ESQ” (FESQ) coding approach was used.

The first step is to form the interaction matrix between effective parameters on coal seam methane drainageability. Then, questionnaires were prepared and ten experts were asked to determine the value of the interaction between each pair of parameters.

In order to defuzzify the interaction matrix, for each element of the matrix, the number of each state of interaction based on the experts’ decisions is considered. The states of interaction are named as n_A (number of no interaction), n_B (number of weak interactions), n_C (number of medium interactions), n_E (number of strong interactions) and n_F (number of critical interactions). These values are firstly normalized and then used as the input of the fuzzy system. For each fuzzy system input, two fuzzy sets “Low” and “High” are considered which are shown in Figure 3. For example, if n_F is “Low” this means that most of the experts stated there is no critical interaction, and the probability of mode F (critical interaction) is lower (Rafiee et al. 2015).

When the normalized value for each element in the interaction matrix is less than 0.4, the MF (membership function) value of “Low” set is greater and the MF value

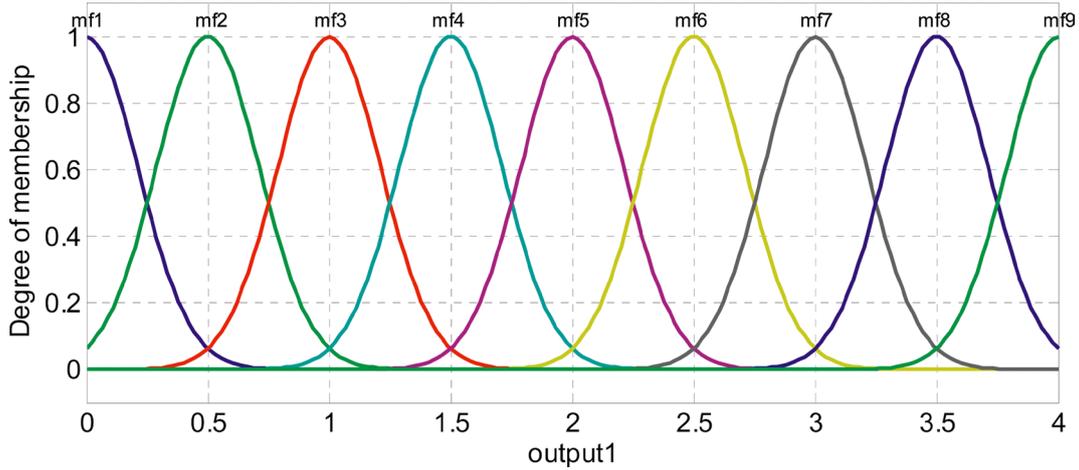


Figure 4: Output of fuzzy system

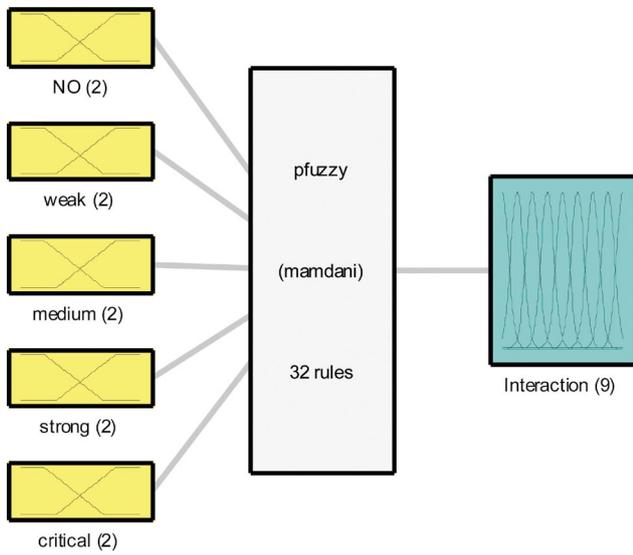


Figure 5: Fuzzy system with 5 inputs, 32 rules and 1 output

of “High” set is lower and vice versa. It is noteworthy, the choice of the “Low” and “High” membership function for each input of fuzzy system have been appointed based on the experts’ judgment (Rafiee et al. 2015). To increase the precision of the intermediate state of the output, the m_1 to m_9 fuzzy sets are defined between 0 and 4 for output of the fuzzy system. The output of fuzzy system form is shown in Figure 4. According to five inputs and considering two modes for each input, 2^5 rules could be defined. In Figure 5, a fuzzy system with 5 inputs, one output and 32 rules is shown.

Considering the fuzzy system, the RES interaction matrix can be coded. Afterward, by using the value of parameters and their corresponding ‘weights’, the methane drainageability index for a coal seam can be calculated.

Hudson proposed a method for determining a weight for each parameter. For this purpose, in the first step, the cause (C_i) and effect (E_i) values for each parameter in the system is calculated by Equation 1 and 2 (Hudson, 1992).

$$C_i = \sum_n I_{mn} \text{ (with } m \equiv i) \tag{1}$$

$$E_i = \sum_m I_{mn} \text{ (with } n \equiv i) \tag{2}$$

Where:

I_{mn} – interaction matrix element

C_i – sum of the raw values

E_i – sum of the column values for each parameter

Then, the weight of each parameter is determined using following Equation 3 (Hudson, 1992).

$$w_i (\%) = \left(\frac{\frac{1}{MP_i} \times (C_i + E_i)}{\sum_j (C_j + E_j)} \right) \times 100 \tag{3}$$

Where:

MP_i – The rating value assigned to the different category of the parameter i .

Therefore, the weight for parameter i , which is shown by w_i , is calculated by its ‘parameter interaction intensity’ ($C_i + E_i$) divided by the sum of interaction intensities of all parameters in the system (Hudson, 1992). After the weights for all parameters (w_i) were calculated, the coalbed methane drainageability index (CMDI) is calculated by Equation 4.

$$CMDI = \sum_i w_i \times P_i \tag{4}$$

Where:

w_i – weights of parameters

P_i – assigned values to each input parameter considered for coal seam methane drainageability.

In the following section, the proposed coal seam methane drainageability index (CMDI) is calculated for the Tabas coal mine and is used to assess the coal seam methane drainageability.

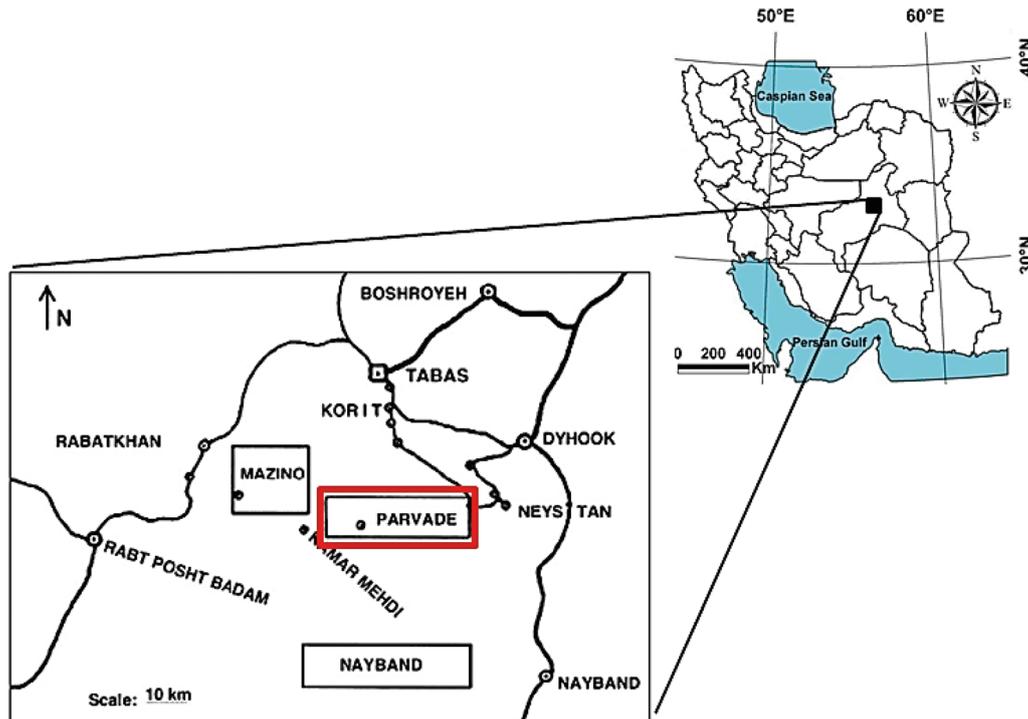


Figure 6: Location map showing the Tabas coal mine (Najafi et al., 2014)

4.2. Case study: Tabas coal mine

The Tabas coalfield is one of the most important coalfields in Central Iran. The area is located in the central desert of Iran, very far from any inhabited areas. The Tabas coalfield consists of the Mazino, Parvadeh and Nayband coal deposits. Coal-bearing strata in the Parvadeh deposit are within the Triassic formations. The rank of the Parvadeh deposit is anthracite and all of the coal seams are formed within the complicated monoclines and synclinal folds. The geology of the area is within a syncline which has been deepened to the east, and has been cut by several faults. Parvadeh coal deposit consists of five coal seams (C_1 , C_2 , D, B_1 and B_2). It has three minable seams (C_1 , B_1 and B_2). The coal seam gas content in the Parvadeh coal deposit increased to a depth of 300 m with a value of 19 m^3 per ton and then it will be constant. In this deposit, the gas content of the surrounding rocks of the coal seam is $3\text{-}5 \text{ m}^3$ per ton at a depth of 500 m (Anon, 2005).

The Tabas coal mine is located in the Tabas coal region approximately 85 km south of Tabas in the South Khorasan province, Iran (see Figure 6). The C_1 seam which is located in the Tabas coal mine is mined by a mechanized longwall retreat mining method. The thickness and dip of the C_1 seam vary from 1.5 to 3 meters (approximately 2.2 m) and from 5 to 26 degrees, respectively. Intermittently low strength sandstone and siltstone layers form in the hangingwall of the coal seam. The distance between the C_1 seam and C_2 is approximately 12.9 m. The footwall consists of siltstone and mudstone seams (see Figure 7). The orientation of the

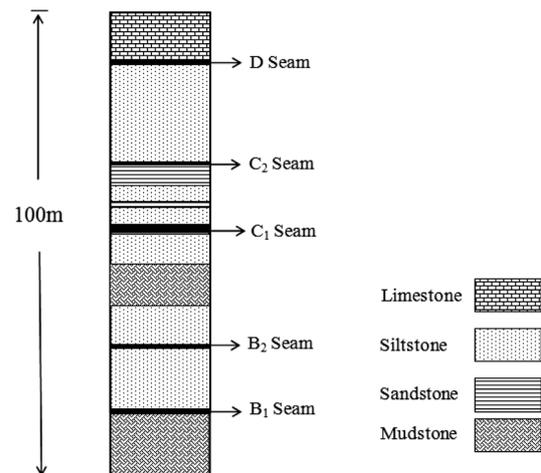


Figure 7: Generalized stratigraphic column at the Tabas coal mine (Anon, 2005)

major cleat set in respect to the C_1 coal seam direction is almost vertical. The direction of one of the sub set of cleats in relation to the C_1 seam direction is approximately parallel but with a plan plunge difference of 35 degrees relating to the horizon. The direction of the other is entirely parallel in relation to the C_1 coal seam direction (Shahriar et al., 2009).

In this mine, a three-entry system was used for serving a 220 m long longwall face. There are two rows of chain pillars between two adjacent panels. Considering the dip of the coal seam, the first set of chain pillars is 200 m deep and the last one located along the lowest panel is approximately 700 m deep. The entries to the panels are 2.8 m high and 4.6 m wide. According to Fig-

Table 3: The value of influencing parameters in the Tabas coal mine for methane drainage classification

Parameters	Value	
P1	Coal Rank	Anthracite
P2	Moisture content (%)	0.36
P3	Permeability of Coal (md)	0.34
P4	Cleat system (spacing (cm))	1.6
P5	Ash content (%)	32
P6	Gas content (m3/t)	20
P7	Degree of saturation (%)	51
P8	Coal seam thicknesses (m)	2.8
P9	Coal seam depth (m)	450
P10	In-situ stress (MPa)	11.5
P11	Geologic structure of overburden	High gas content of surrounding rock
P12	Length of boreholes (m)	50-150
P13	Orientation of boreholes toward the horizon (Degrees)	20
P14	Borehole stability	Moderately Stable
P15	Borehole spacing (m)	20
P16	Panel dimension (Width) (m)	220
P17	Cut depth (cm)	80

ure 7, the B₁ and B₂ coal seams are located above and below the C₁ coal seam and predicted after coal extraction the amount of gas entered to the mine working panel. Considering the high value of C₁ gas content, a horizontal methane drainage wellbore was designed for this mine and its implementation was planned for a depth greater than 300 m (Anon, 2005).

This paper concerns the panel at a depth of 300 m. The information of the Tabas coal mine for methane drainage classification is shown in Table 3.

4.3. Determination CMD index for the Tabas coal mine

For the determination of the coal seam methane drainageability index in the Tabas coal mine with the FRES method, the first step is the creation of an interaction matrix. For this purpose, by applying the arbitrations of specialists to the fuzzy system and using fuzzy rules on their views, the fuzzy interaction matrix was created and is shown in Table 4.

The second step consists of plotting a cause-effect diagram in order to identify dominant or subordinate parameters, and also interactive parameters. The parameter interaction intensity of each parameter is calculated according to Figure 8.

The C-E diagram of the affecting parameters on coal seam methane drainageability is plotted in Figure 9. The spots below the C=E line are called dominant and the spots above the C=E line are called subordinate. Conforming to this figure, along the C=E, the C+E value increases.

It can be seen that gas content (P₆) is mostly a subordinate parameter (affected by the system). The more interactive parameter is the permeability of coal (P₃) and the less interactive parameter is ash content (P₅). The most dominate parameter is coal seam depth (P₉).

The interaction intensity histogram (E+C) for each parameter is shown in Figure 10. This histogram displays that small changes in the parameters P₃ (Permeability of Coal), P₆ (Gas Content) and P₁₀ (In-situ stress)

Table 4: The fuzzy interaction matrix for coal seam methane drainageability

P1	1.88973489	2.99999919	1.24654	1.50562	2.7534603	1.50562	0.159211	0.159738	0.159211	0.159738	0.159738	0.159738	0.182461	0.159738	0.159211	0.464948
0.159738	P2	1.26872294	0.505321	0.159211	2.9999992	3.238063	0.157082	0.159211	0.159211	0.505321	0.159211	0.159211	0.464948	0.159211	0.159211	0.159211
0.159738	1.05496666	P3	1.20591	0.464948	2.999999	2	0.159211	0.159738	0.159738	0.464948	0.464948	1.22246	1.22246	1.889735	0.464948	1.20591
0.464948	1.05496666	3.84078917	P4	0.464948	2.6003345	1.889735	0.159211	0.159211	1.054967	1.054967	1.054967	1.5	2	2.999999	0.159738	1.268723
1.746853	0.15921061	0.76190955	0.159211	P5	0.7619096	1.20591	0.157082	0.157082	0.157082	0.157082	0.157082	0.159211	0.464948	0.159211	0.159211	0.464948
0.464948	1.21346428	0.76190955	0.464948	0.159211	P6	1.979523	0.159211	0.464948	0.505321	0.159738	1.054967	1.054967	0.159738	1.5	0.182461	0.464948
0.159211	2.49437974	1.20591029	0.159211	0.159211	3.8175391	P7	0.157082	0.159211	0.159211	0.159211	1.054967	0.182461	0.159211	1.268723	0.159211	0.159738
0.159211	0.15708173	0.46494846	0.464948	0.464948	1.9747828	1.000001	P8	0.157082	0.464948	0.464948	1.213464	0.464948	1.268723	1.889735	1.889735	2.25816
2.080636	0.18246091	2.999999	2.75346	0.505321	2.999999	1.50562	0.157082	P9	2.246538	1.268723	1.979523	1.889735	2	1.50562	1.889735	1.399595
1.24654	0.15921061	2.62609916	2.999999	0.157082	1.2059103	1.24654	0.159211	1.054967	P10	1.379981	1.213464	2.49438	3.817539	2	1.268723	2.999999
0.182461	0.46494846	1.05496666	2.258227	0.182461	2.999999	2	0.159211	0.159738	2.999999	P11	2	2	2.794035	2.999999	1.746853	2.49438
0.159211	0.15708173	1.74685313	0.464948	0.157082	0.1592106	0.464948	0.159211	0.159211	0.464948	0.159211	P12	1.889735	1.24654	2.600335	1.213464	1.054967
0.159211	0.15708173	1.68424763	0.159738	0.157082	0.1592106	0.159738	0.159211	0.157082	0.464948	0.159211	2.999999	P13	1.493939	1.979523	0.464948	0.182461
0.159211	0.15708173	0.50532077	0.159738	0.159211	0.159738	0.159211	0.159211	0.159211	0.159738	0.159211	2.258227	2.25816	P14	1.000001	1.22246	1.20591
0.159211	0.15921061	1.88973489	0.464948	0.159211	0.4649485	0.159738	0.159211	0.157082	0.464948	0.159211	1.974783	2.75346	1.000001	P15	0.182461	0.464948
0.159211	0.15708173	0.76190955	0.464948	0.157082	0.1592106	0.505321	0.159211	0.159211	0.464948	0.159738	0.464948	1.000001	1.20591	1.24654	P16	2.25816
0.159211	0.15708173	0.46494846	0.76191	0.159211	0.159738	0.464948	0.157082	0.157082	0.182461	0.159211	0.182461	0.505321	1.000001	1.000001	0.159738	P17

P1: Coal Rank, P2: Moisture content, P3: Permeability of Coal, P4: Cleat system, P5: Ash content, P6: Gas content, P7: Degree of saturation, P8: Coal Seam thicknesses, P9: Coal seam depth, P10: In-situ stress, P11: Geologic structure of overburden, P12: Length of boreholes, P13: Orientation of boreholes to the principal horizontal stress), P14: Boreholes stability, P15: Boreholes spacing, P16: Panel dimension, P17: Cut depth

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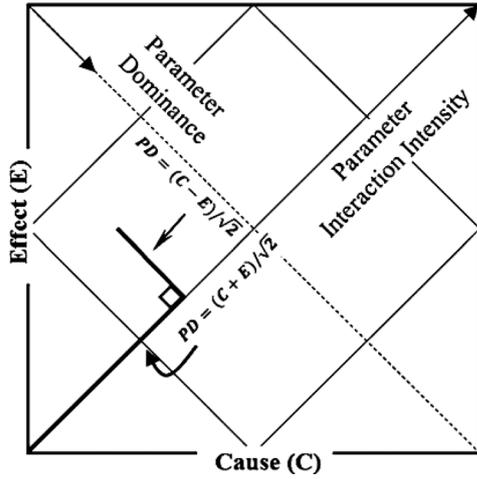


Figure 8: Equal parameter interaction intensity and dominance (Hudson, 1992)

Table 5: The weighted coefficient

Parameters	C + E	W _i (%)
P1 Coal rank	21.60	0.884
P2 Moisture content	20.35	0.832
P3 Permeability of coal	40.34	1.650
P4 Cleat system (spacing)	36.42	1.490
P5 Ash content	12.16	0.497
P6 Gas content	37.13	1.518
P7 Degree of saturation	31.10	1.272
P8 Coal seam thicknesses	17.29	0.707
P9 Coal seam depth	31.10	1.272
P10 In-situ stress	36.30	1.485
P11 Geologic structure of overburden	33.23	1.359
P12 Length of boreholes	30.65	1.254
P13 Orientation of boreholes to the principal horizontal stress	30.39	1.243
P14 Boreholes stability	30.52	1.248
P15 Boreholes spacing	35.13	1.437
P16 Panel dimension (Width)	20.97	0.857
P17 Cut depth	24.34	0.995

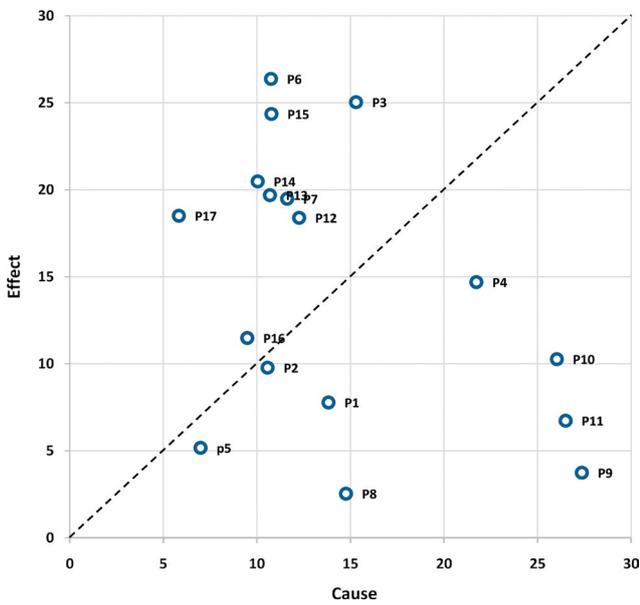


Figure 9: Cause-effect diagram

have a great effect in the system treatment. These parameters have a maximum value of C+E in the system.

Base on the weight value (see Table 5) of each parameter, the coal seam methane drainageability index (CMDI) is calculated. The coal seam methane drainageability index is an expression of the inherent potential methane drainage of the coal seam, where the maximum value of the index is 100 and refers to very good conditions for pre-drainage techniques in a working mine. The classification of methane drainageability status for a coal seam is shown in Figure 11. CMDI ranges between 0 and 100; CMDI <20 indicates very bad conditions for

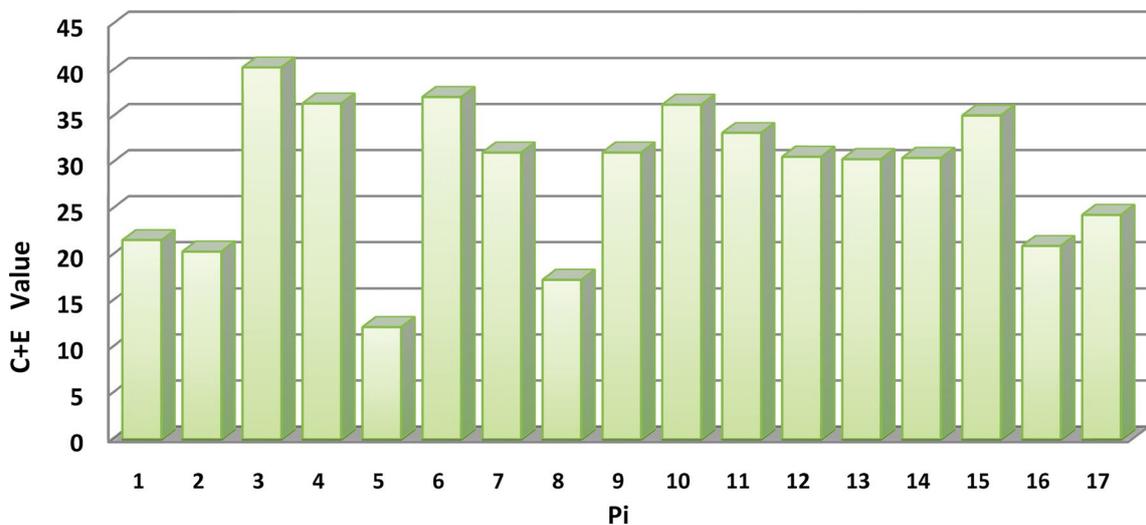


Figure 10: Histogram of interactive intensity of parameters

methane drainage, $20 < \text{CMDI} < 40$ corresponds to bad condition for methane drainage, $40 < \text{CMDI} < 60$ corresponds to moderate conditions for methane drainage, 60

$< \text{CMDI} < 80$ corresponds to good conditions for methane drainage and $80 < \text{CMDI} < 100$ corresponds to very good conditions for methane drainage. It should be noted that by increasing the CMDI, the potential of methane drainage from a working mine increases. Therefore, it is recommended that for CMDI values between 60 and 80, horizontal boreholes and gob gas ventholes be implemented and for CMDI values between 80 and 100, vertical boreholes and gob gas ventholes be implemented. In this study, the CMDI value for the Tabas coal mine is 67.4. This value indicates the methane drainage method could be implanted in this mine. In summary, the flow sheet for determining the coal seam methane drainageability by FRES is presented in Figure 12.

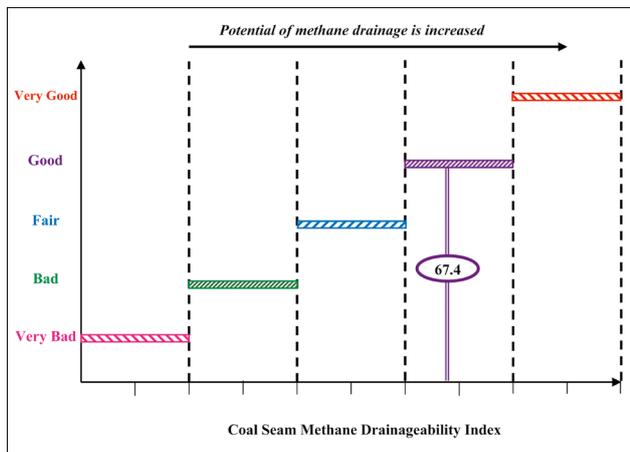


Figure 11: The classification of coalbed methane status

5. Conclusion

In this study, a new approach, namely, coal seam methane drainageability index (CMDI) is developed for

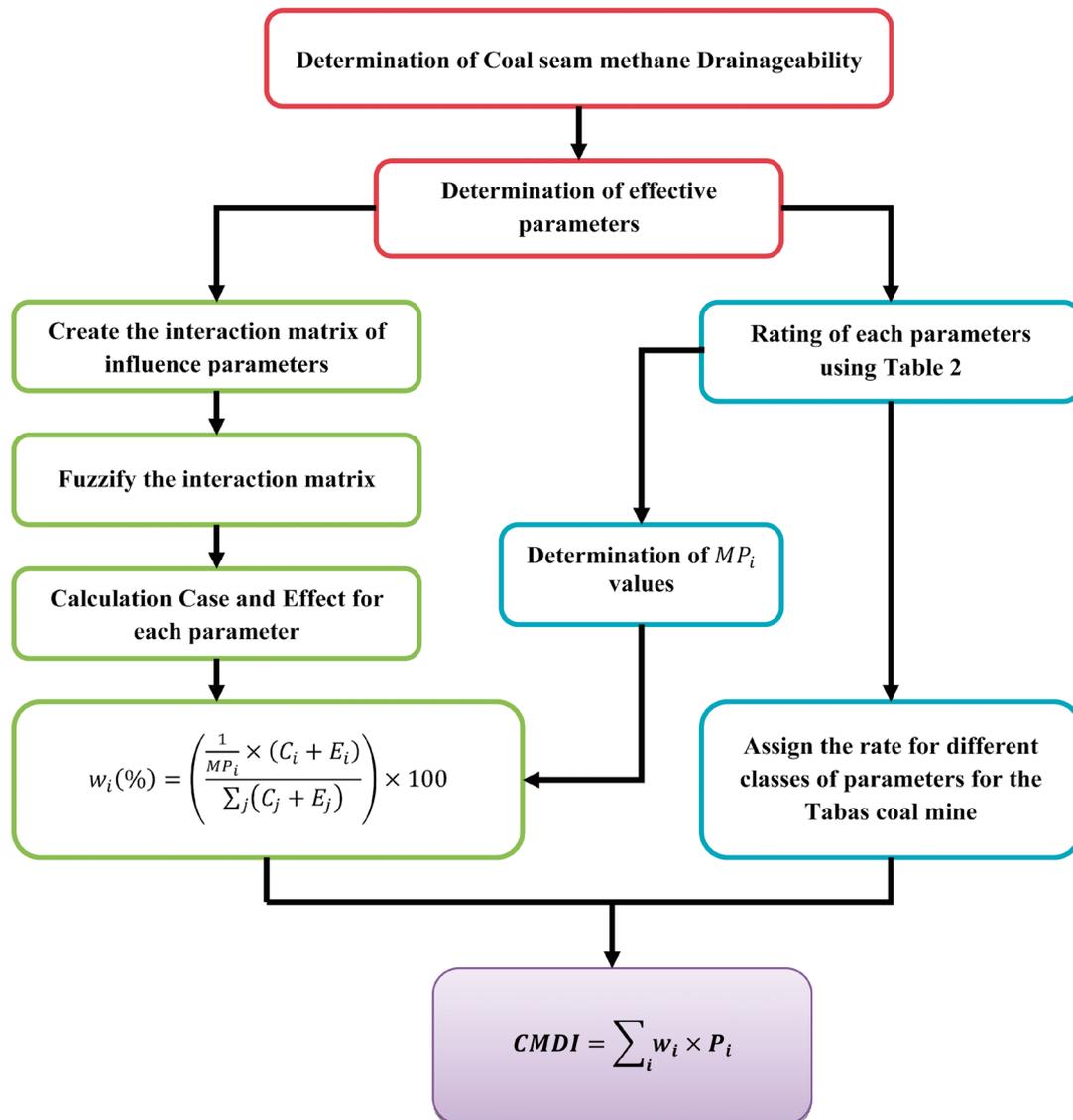


Figure 12: Flowchart in prediction CMDI using FRES

the classification of coal seam methane drainageability. In this study, after initial studies, the most important parameters (17 parameters) affecting methane drainage were selected. In the CMDI approach, the classification of a coal seam is based on the fuzzy rock engineering system. Accordingly, the first step is creating an interaction matrix by applying the fuzzy system to judgments of experts and using fuzzy rules on their views. Then a cause–effect diagram is plotted using the values of cause and effect parameters. By calculating the coefficient values of each parameter and performing a summation of the multiplication of them to assigned values for each input parameter, the coal seam methane drainageability index is calculated. According to this new approach, the following conclusions have been made:

- The effect of each parameter on methane drainage from the coal seam in a working mine is evaluated. The results obtained from a cause–effect diagram show that the permeability of coal (P_3) is the most interactive parameter. In other words, a small change in this parameter causes a large change in the system. The most dominant parameter is coal seam depth (P_9) and the most subordinate parameter is gas content (P_6).
- The application of this new approach at the Tabas coal mine for the classification C_1 coal seam showed that the C_1 coal seam is located in a good zone for methane drainage.

The presented index based on the fuzzy RES is a suitable method which provides a reliable result for the prediction coal seam methane drainageability. However, such a proposed index usually requires future research for incorporating other parameters which may be critical for methane drainage from a coal seam. It should be noted that the present index is suitable for pre-drainage in a working mine, and is not necessarily appropriate for post-drainage techniques.

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SAŽETAK

Razvoj novoga indeksa propusnosti metana u slojevima ugljena uporabom inženjerskoga sustava temeljenoga na neizravnoj logici

Ugljeni plin jedan je od najvažnijih izvora energije iz nekonvencionalnih plinskih ležišta. Prepoznavanje varijabli koji utječu na propusnost metana važno je za sve buduće projekte iskorištavanja takvih ležišta. Kod crpenja takvih metanskih ležišta efikasnost je određena prirodnim i operacijskim čimbenicima. Prikazan je novi metanski indeks crpenja (MIC, engl. skr. CMDI) kao vrijednost za uporabu u rudarskim zahvatima. Razmatrano je 17 glavnih parametara koji utječu na crpenje metana iz ugljena, svrstanih u matricu kreiranu na temeljima neizravne logike stijenskoga sustava. Zatim je analiziran odnos parametara koji utječu na crpenje. Budući da odnosi u neizravnim logičkim modelima nisu jedinstveni, takav sustav pažljivo je prilagođen kako bi minimizirao subjektivnost u određivanju težinskih faktora pojedinačnih parametara. Primjer uporabe modela prikazan je za rudnik ugljena Tabas u Iranu. Na uzorcima iz sloja C₁ toga prostora primijenjen je izračun indeksa crpenja. Rezultati su pokazali kako takav indeks može vrlo uspješno predvidjeti moguću proizvodnju metana te biti uporabljen kao varijabla za donošenje odluka i smanjenje rizika negativnih događaja u takvim projektima.

Ključne riječi:

crpenje metana, stijenski inženjerski sustav, sustavi neizravne logike, nekonvencionalni plin, rudnik ugljena Tabas

Authors contribution

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